

***Project 46: Influence of Microstructure on the Oxidation
Behaviors of Refractory Complex Concentrated
Alloys (RCCAs)***

***Semi-annual Fall Meeting
April 2022***

- Student: Noah Welch (ISU)
- Faculty: Dr. Peter C. Collins (ISU)
- Industrial Mentors: Dr. Todd Butler (AFRL)

Project 46: Influence of Microstructure on the Oxidation Behaviors of Refractory Complex Concentrated Alloys (RCCAs)



- Student: Noah Welch (ISU)
- Advisor(s): Peter Collins (ISU), Maria Quintana (ISU)

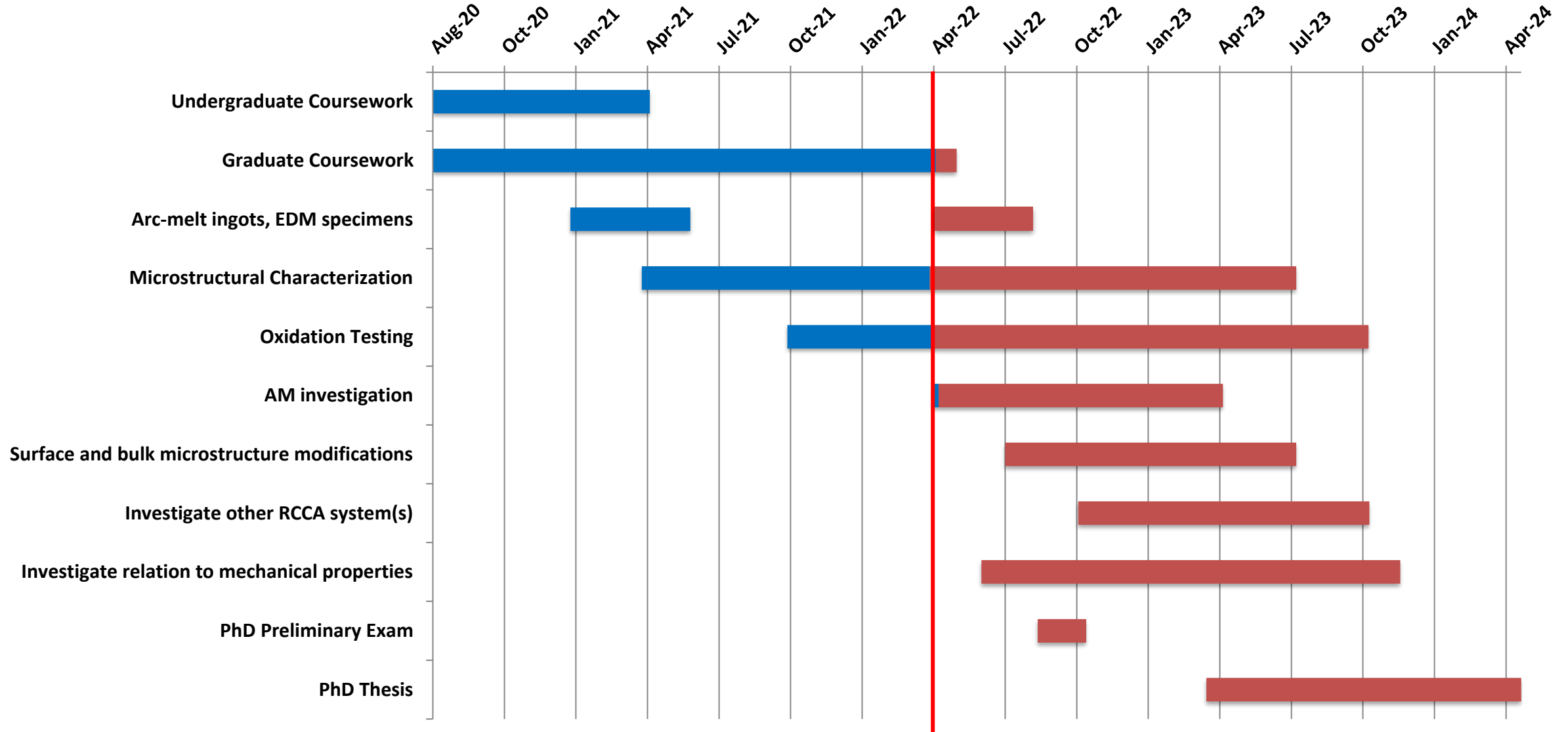
Project Duration
PhD: Fall 2020 to Spring 2024

- **Problem:** The oxidation mechanisms in RCCAs and the influence of microstructure on oxide formation are poorly understood.
- **Objective:** Investigate microstructural influence on the oxidation properties of RCCAs, specifically TaTiCr system.
- **Benefit:** RCCAs show great promise for future use in advanced, high-temperature structural applications.

- Recent Progress**
- Completed TGA Oxidation tests of Ta-Ti-Cr alloys in HIP condition
 - EDS, SEM, and XRD analysis of oxide structures and investigation of oxidation mechanisms in each alloy
 - Promising alloy identified, investigating nearby composition ranges using AM for future oxidation testing
 - Draft manuscript on oxidation behavior being sent to CANFSA IAB

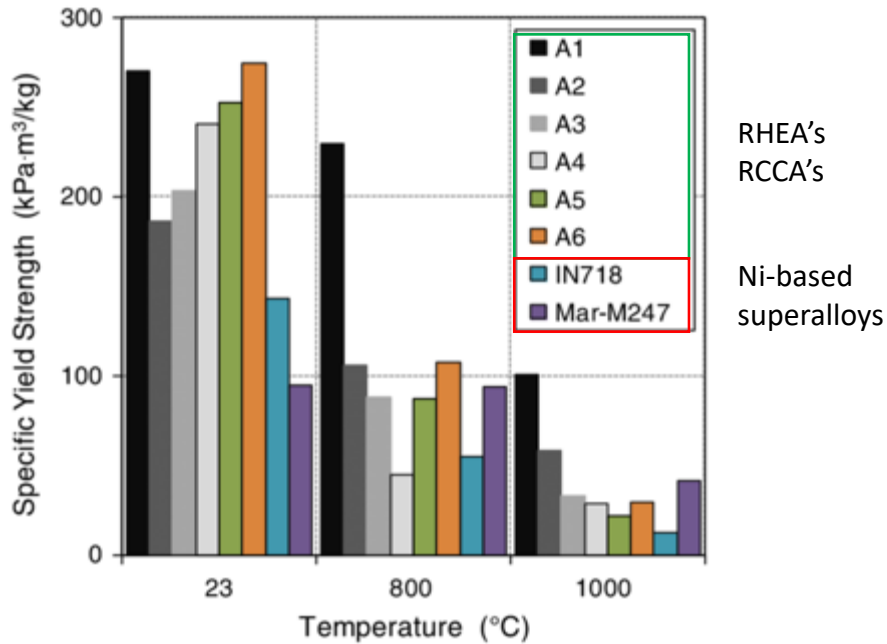
Metrics		
Description	% Complete	Status
1. Literature review	80%	●
2. Cast specimens at desired compositions for oxidation tests, characterize microstructure.	50%	●
3. Test oxidation performance with TGA and investigate oxidation mechanisms in various processing conditions	50%	●
4. Measure mechanical properties	0%	●
5. Investigate expansibility to other RCCA systems	0%	●

Progress



Center Proprietary – Terms of CANFSA Membership Agreement Apply

Industrial Relevance



Comparison of refractory high entropy alloys (RHEA) and RCCA specific yield strength to two Ni-based superalloys

Implications:

- Displace Ni-based superalloys as prominent advanced structural alloys
 - Improved oxidation performance and mechanical properties
- Framework for future alloy development

Applications:

- High temperature, structural components and advanced propulsion components

Benefits:

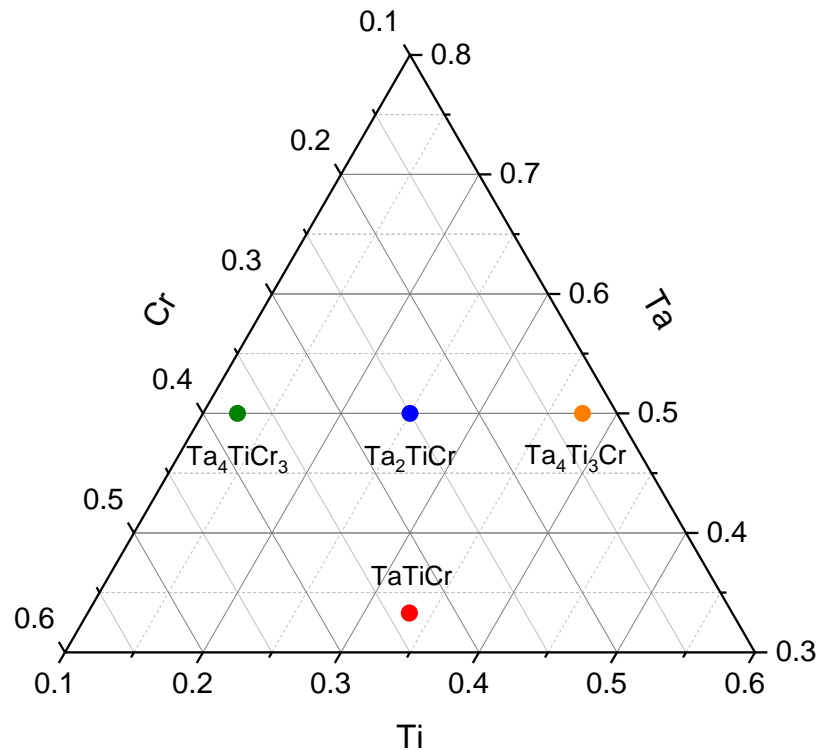
- Higher operating temperatures
- Better oxidation performance
- Improved high-temperature processes

Outline



- Ta-Ti-Cr system
- HIP Microstructure
- Oxidation Tests
- Post-oxidation Microstructure
- Conclusions
- Future Work

Ta-Ti-Cr System

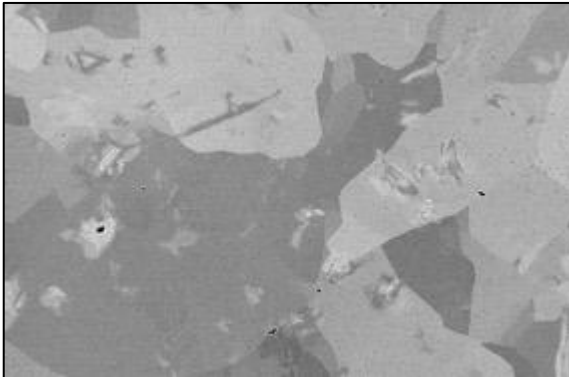


- Characterize four alloys in system
 - TaTiCr ($\text{Ta}_{33.3}\text{Ti}_{33.3}\text{Cr}_{33.3}$)
 - $\text{Ta}_4\text{Ti}_3\text{Cr}$ ($\text{Ta}_{50}\text{Ti}_{37.5}\text{Cr}_{12.5}$)
 - Ta_2TiCr ($\text{Ta}_{50}\text{Ti}_{25}\text{Cr}_{25}$)
 - Ta_4TiCr_3 ($\text{Ta}_{50}\text{Ti}_{12.5}\text{Cr}_{37.5}$)
- Predicted to form (Ta,Ti)-rich bcc solid solution and Cr_2 -(Ta,Ti) Laves precipitates
- Initial investigation to determine promising candidates with good oxidation properties

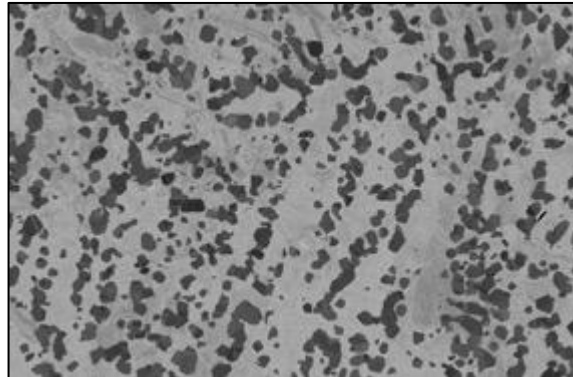
Microstructure

Microstructure - HIP

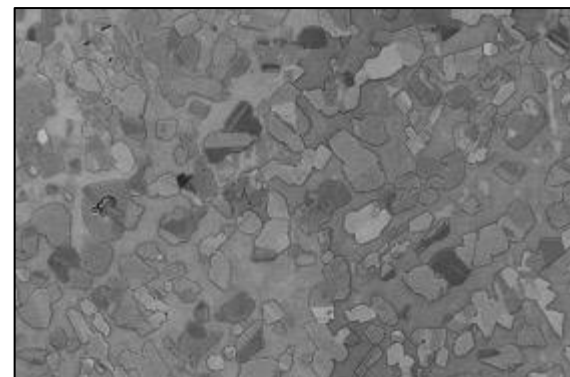
Ta₄Ti₃Cr



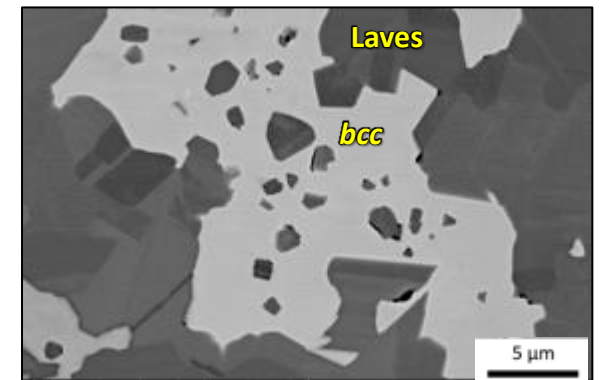
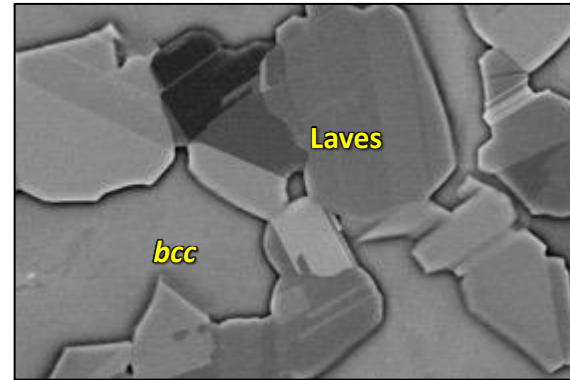
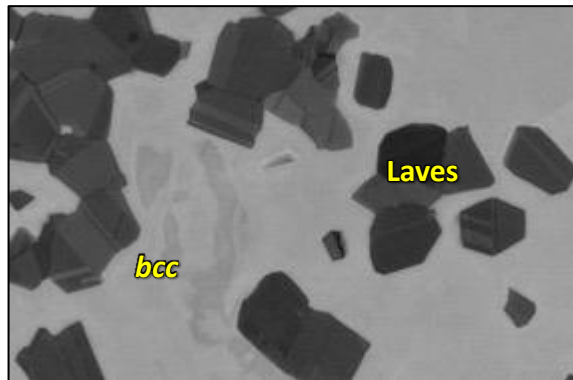
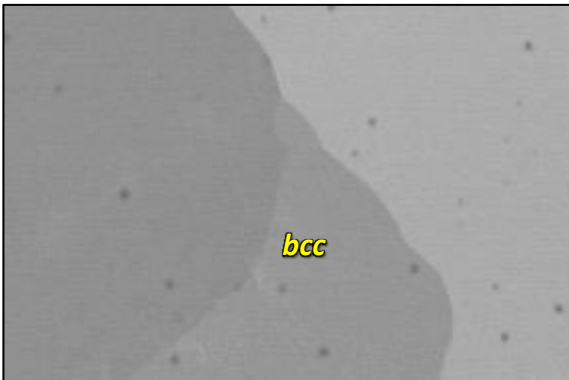
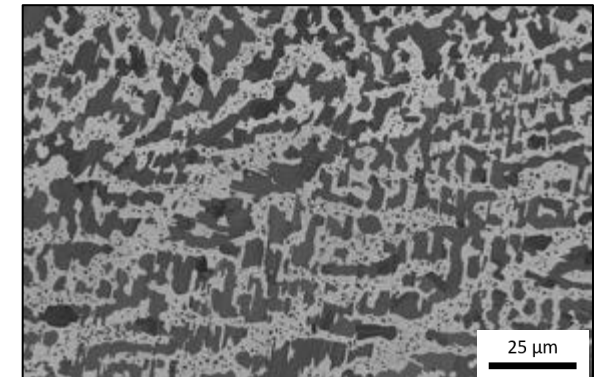
Ta₂TiCr



TaTiCr



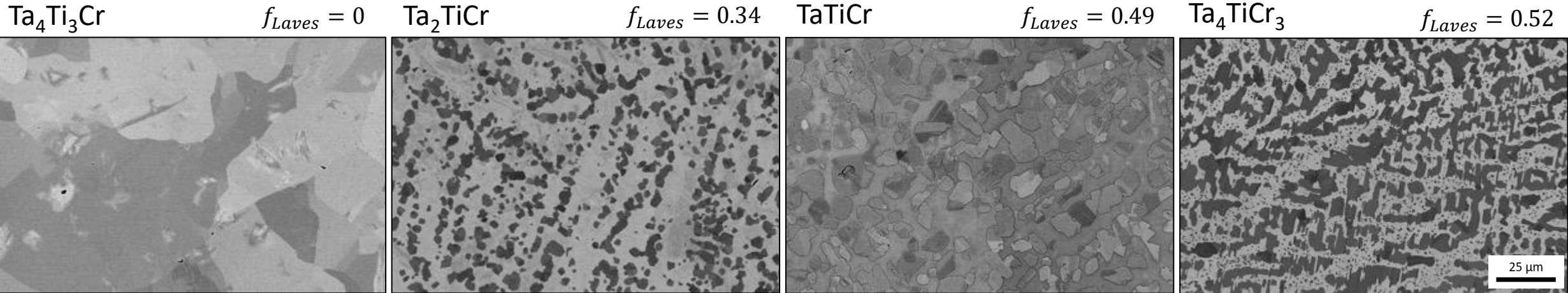
Ta₄TiCr₃



All specimens HIPed for 3 hrs, 30 ksi (207 MPa), 1400 °C

Microstructure - HIP

Increasing Laves fraction, increasing alloy Cr content →

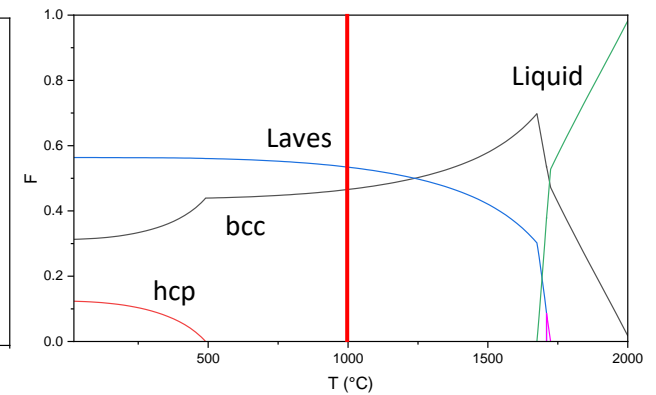
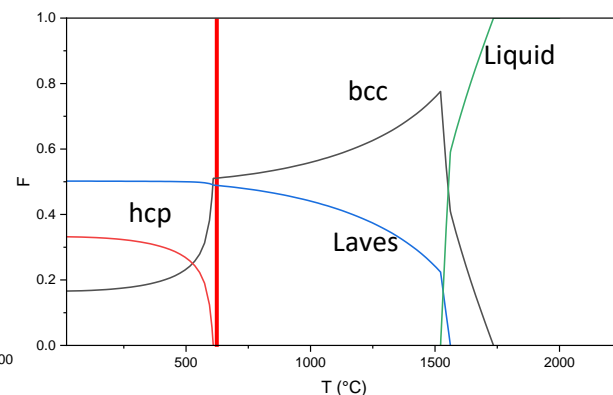
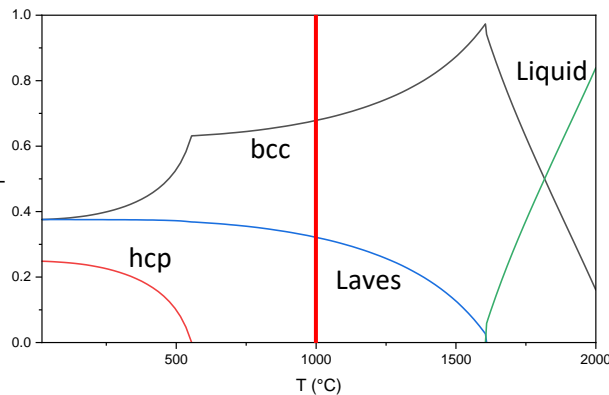
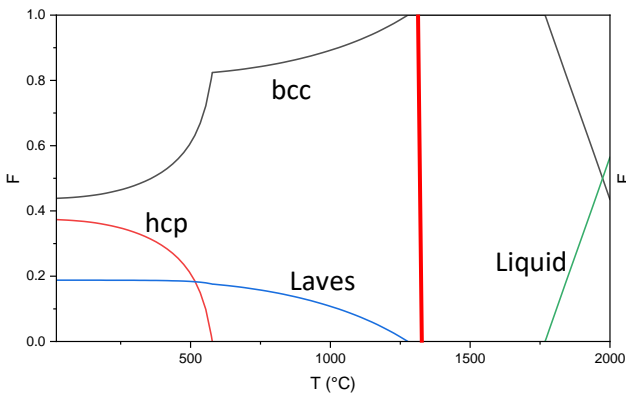


Hardness: 36.9 HRC, Density: 11.79 g/cm³

Hardness: 53.2 HRC, Density: 11.95 g/cm³

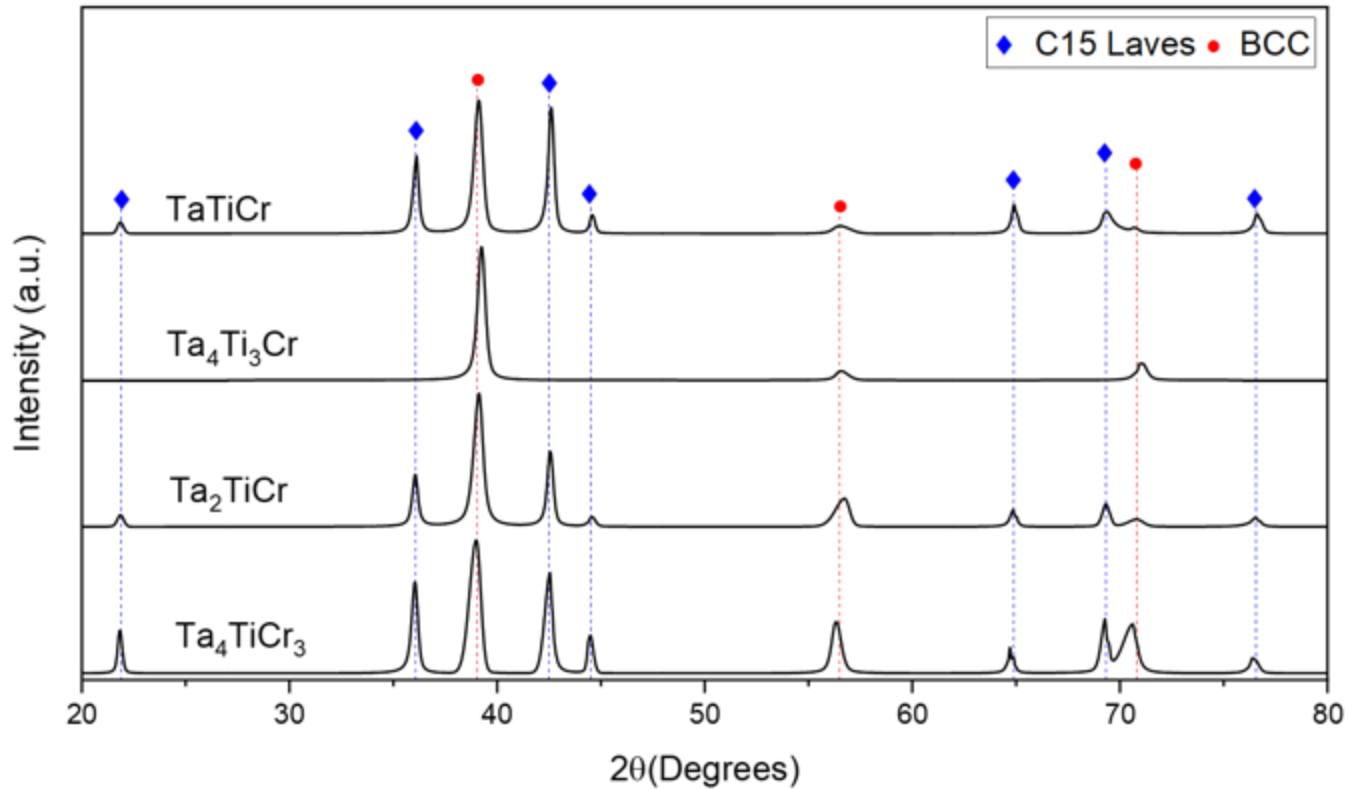
Hardness: 53.5 HRC, Density: 8.40 g/cm³

Hardness: 60.2 HRC, Density: 12.69 g/cm³



Sluggish kinetics are responsible for quasi-quenched state after cooling from 1400 °C. (Cooling rate 15 °C /min)

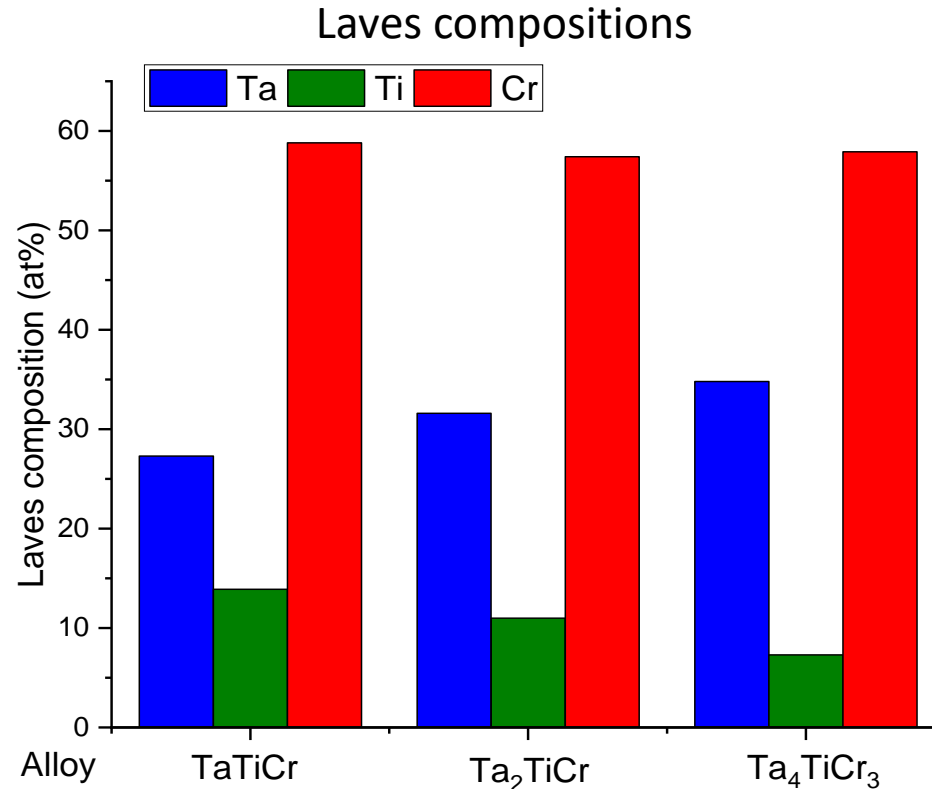
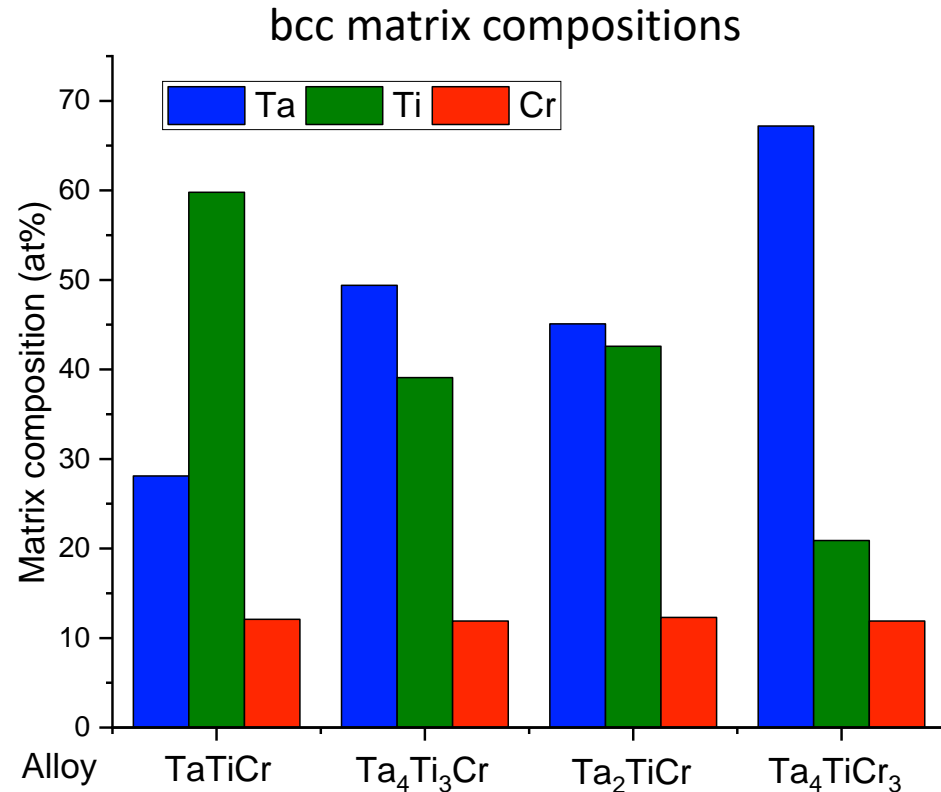
XRD Phase Verification



	TaTiCr	Ta ₄ Ti ₃ Cr	Ta ₂ TiCr	Ta ₄ TiCr ₃
C15 Laves	7.024	-	7.036	7.047
bcc	3.243	3.247	3.254	3.264

Lattice parameters of phases (Å)

Phase Compositions



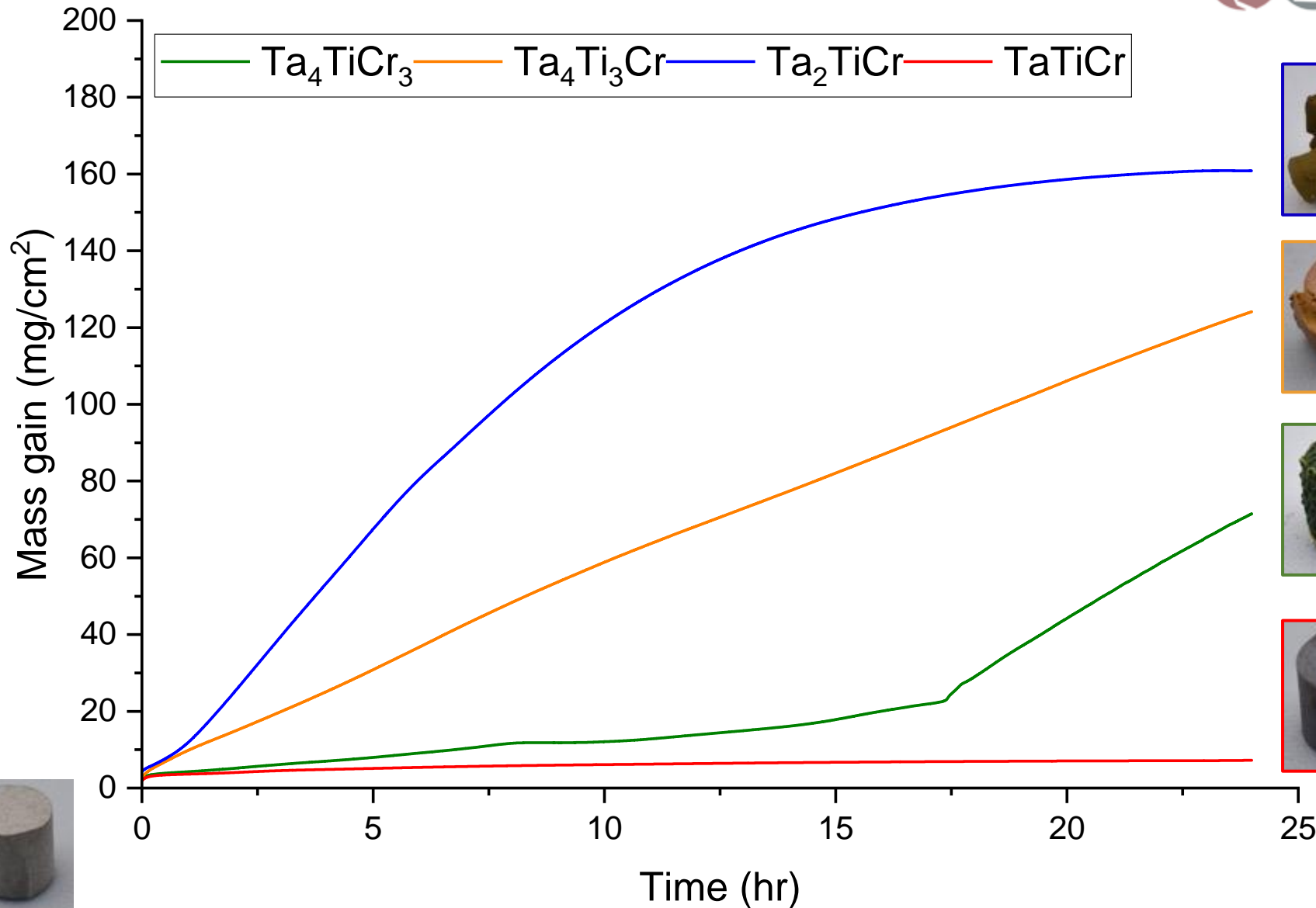
Alloy composition has a large influence on matrix composition and smaller effect on Laves composition

- Cr content in bcc matrix and Laves remains nearly constant across the four alloys
- Ta/Ti vary widely in matrix w.r.t. alloy composition (30-40%), not as much in Laves (5-6%)

*Hence, why TaTiCr matrix is so much darker in BSE images than other alloys (less Z-contrast between bcc and Laves)

Oxidation Tests

TGA Oxidation Tests – 1200°C



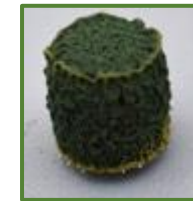
Ta₂TiCr

160.9 g/cm²



Ta₄Ti₃Cr

124.1 g/cm²



Ta₄TiCr₃

71.5 g/cm²



TaTiCr

7.2 g/cm²



Oxidation Kinetics



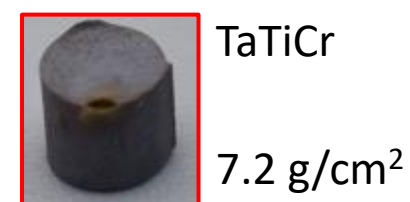
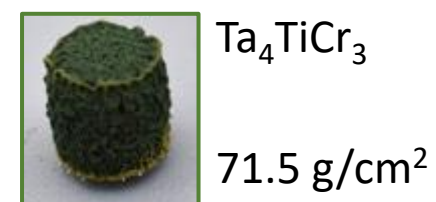
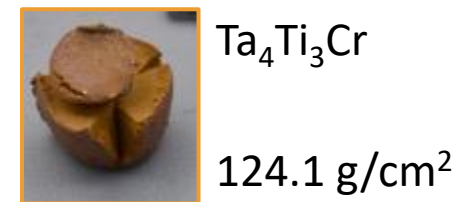
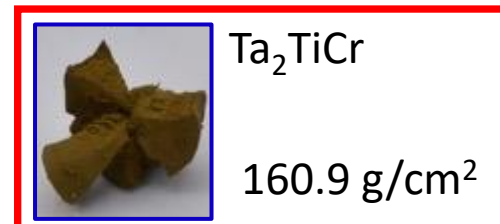
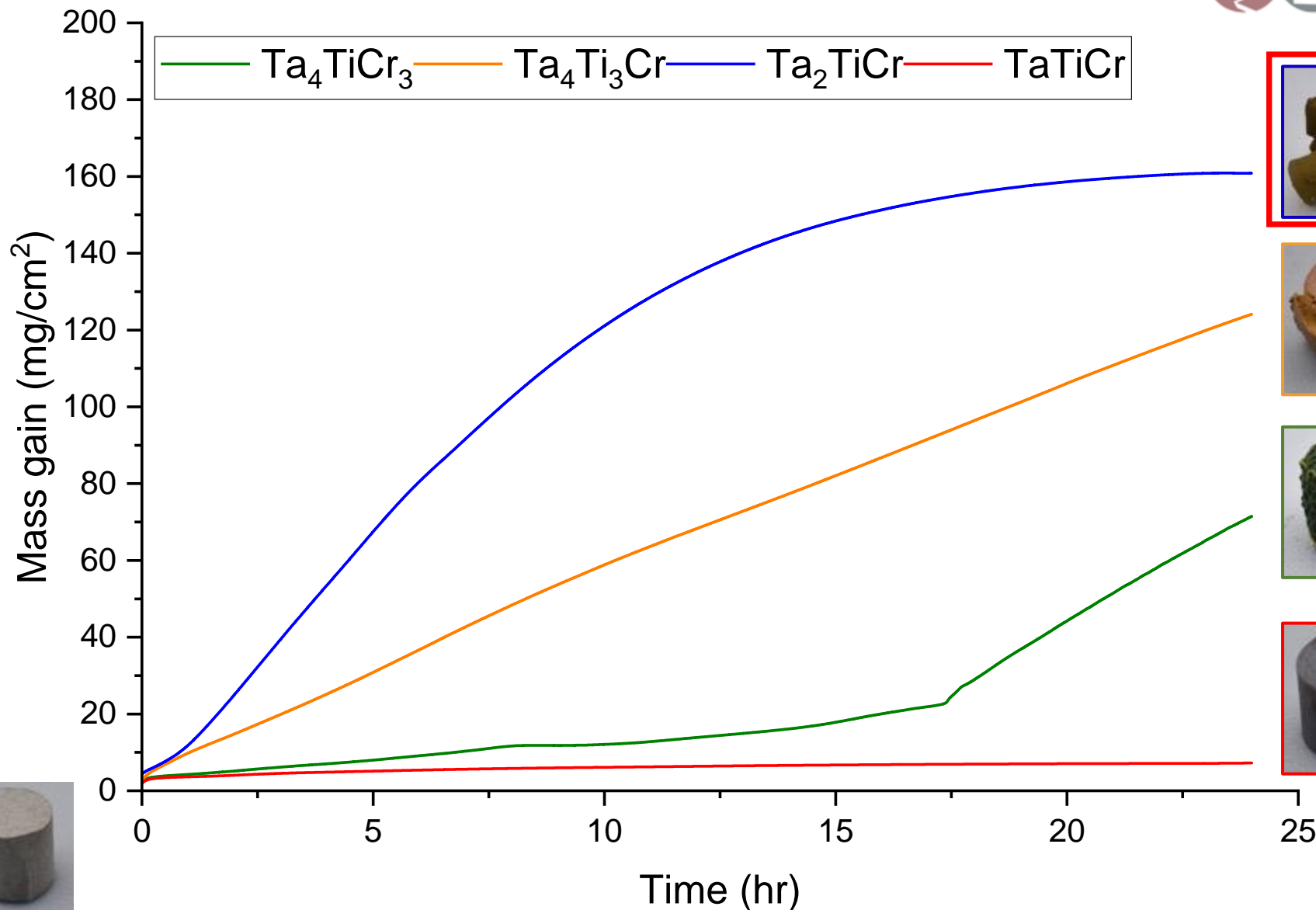
$$\Delta m = kt^n$$

- Δm = mass gain
- k = reaction rate constant
- n = time exponent
 - $n > 1$, breakaway oxidation
 - $n = 1$, linear, interface-controlled
 - $n = 0.5$, parabolic, diffusion-controlled
 - $n < 0.5$, diffusion-controlled + volatilization effects

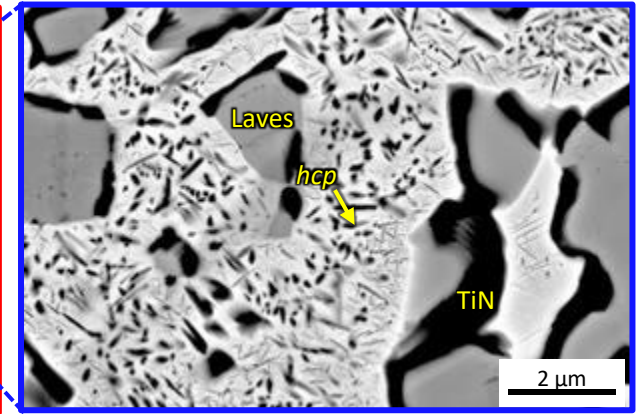
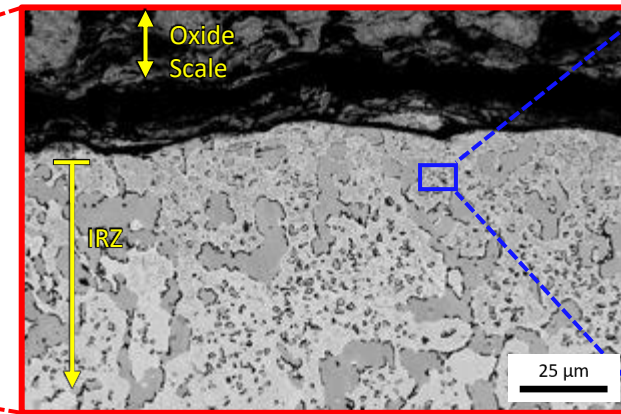
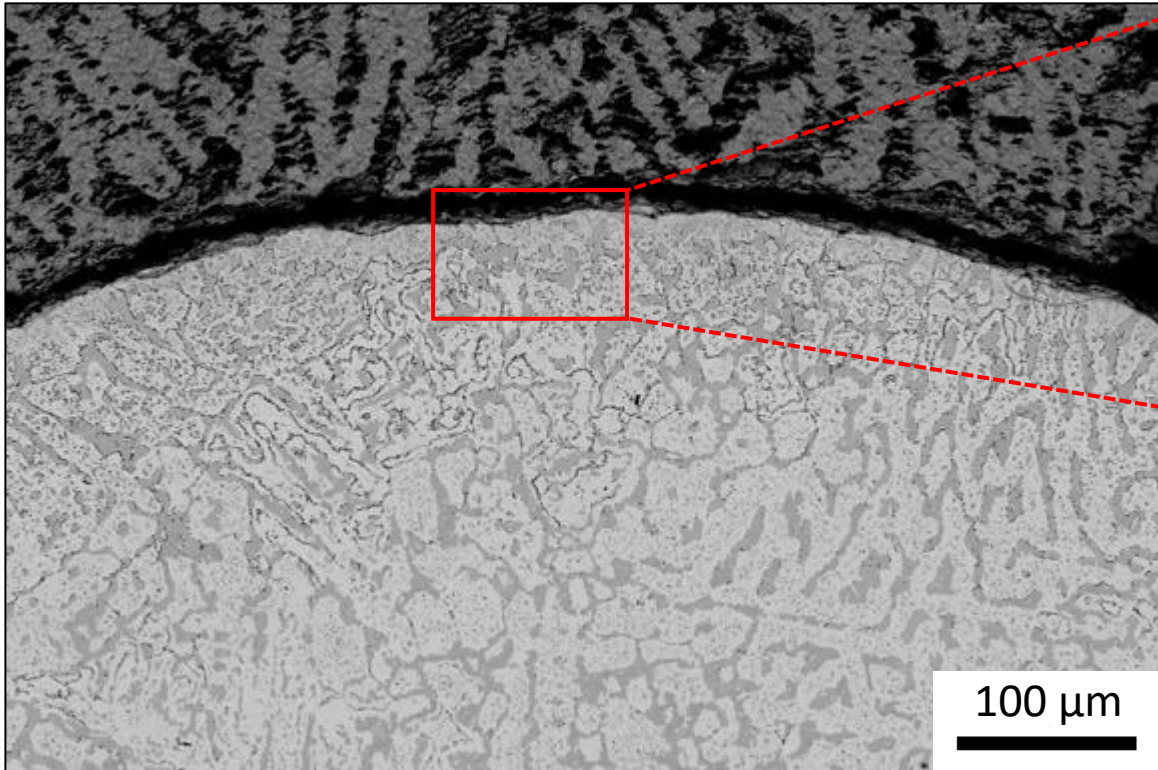
Alloy	Mass gain after 24 hrs (mg/cm ²)	k (mg/cm ² -h ^{n})	n	Duration
TaTiCr	7.2	3.58	0.23	0-24 hrs
		3.55	0.51	0-6 hrs
Ta₄TiCr₃	71.5	0.84	1.17	6-16 hrs
		0.01	3.19	16-24 hrs
Ta₄Ti₃Cr	124.1	7.88	0.85	0-24 hrs
Ta₂TiCr	160.9	12.06	1.03	0-24 hrs

Post-oxidation Microstructure

TGA Oxidation Tests – 1200°C



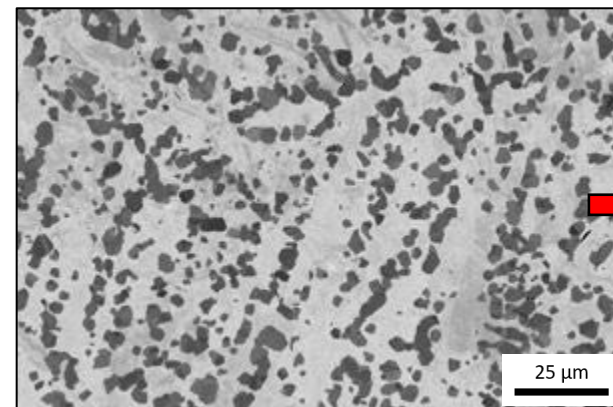
Post-oxidation microstructure - Ta₂TiCr (1200°C, 13 hrs)



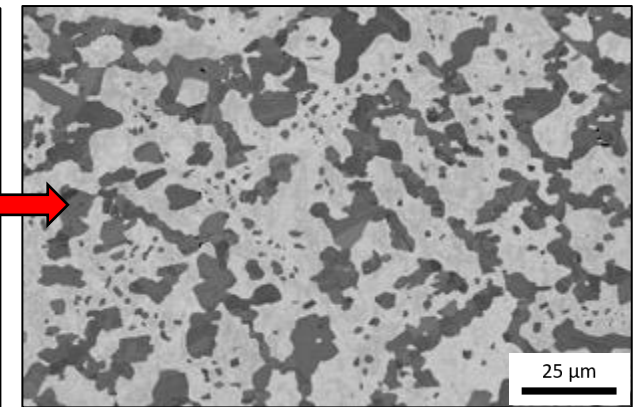
External scale: 1.15 mm
Internal reacted zone (IRZ): 150 μm

- Thick, separated oxide scale after 13 hrs
- Fine TiN and hcp precipitates along phase boundaries and in matrix.

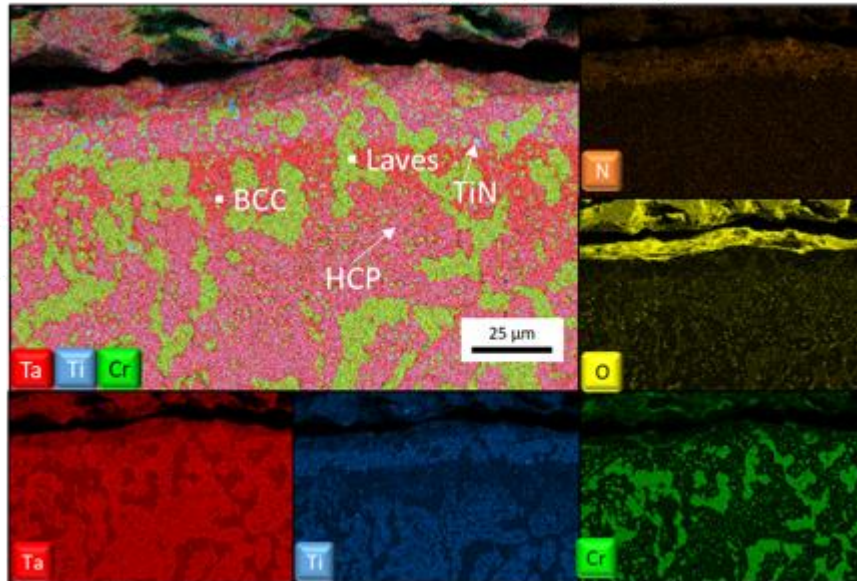
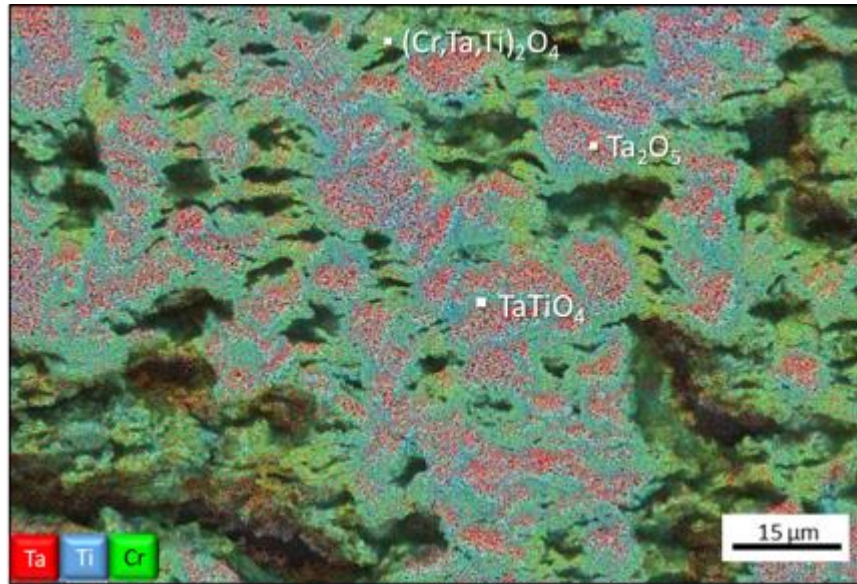
Bulk before oxidation



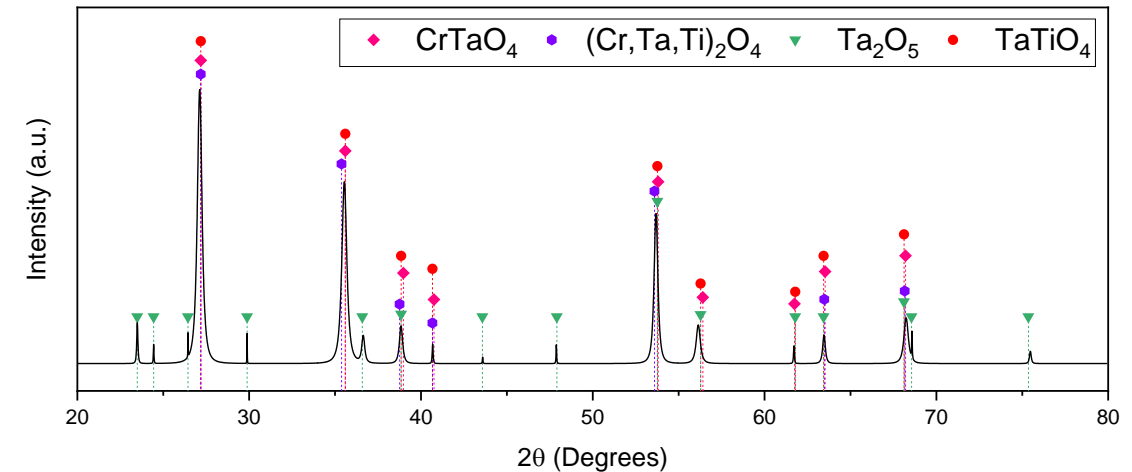
After 13 hrs at 1200°C



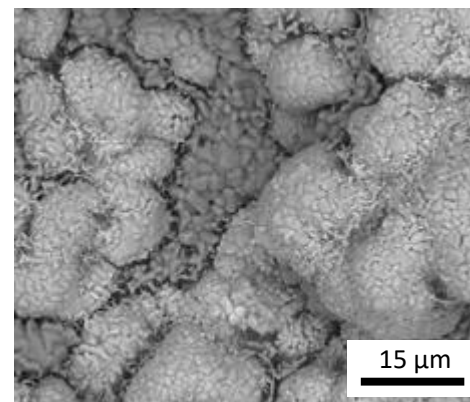
Oxide Products – Ta₂TiCr (1200°C, 13 hrs)



Powder XRD from oxide scale

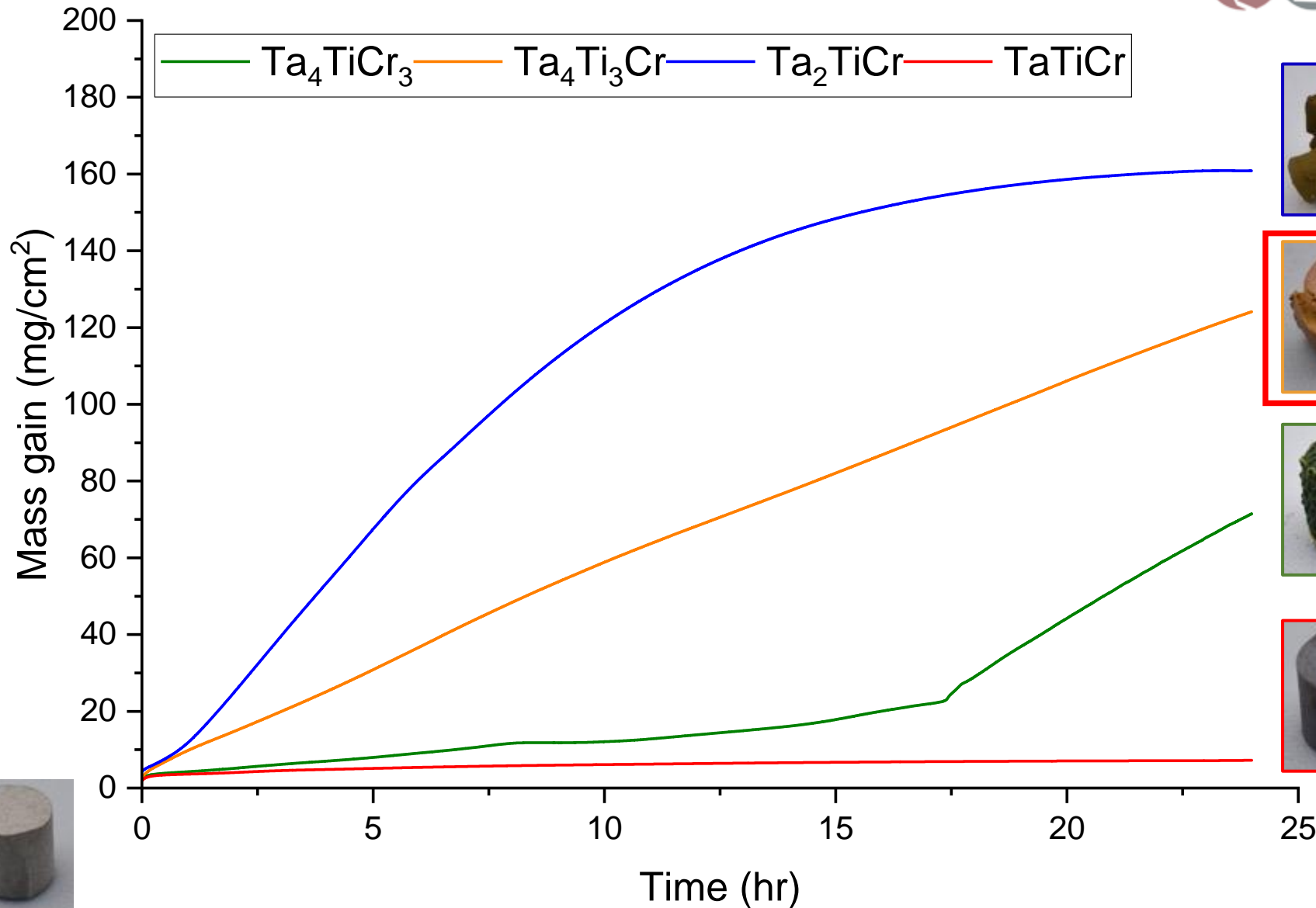


Scale surface



- Outer scale has repeating morphology due to local solute depletion phenomena from selective oxidation
- Consists primarily of “mixed” rutile oxides with pockets of Ta₂O₅
- Ta₂O₅ is harmful, offers no oxidation resistance

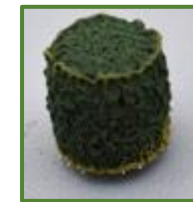
TGA Oxidation Tests – 1200°C



Ta₂TiCr
160.9 g/cm²



Ta₄Ti₃Cr
124.1 g/cm²



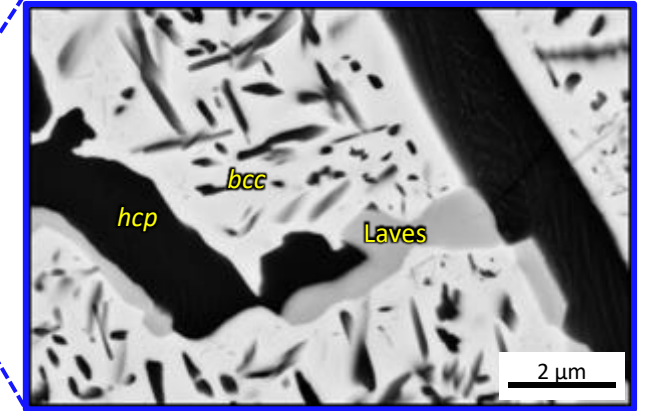
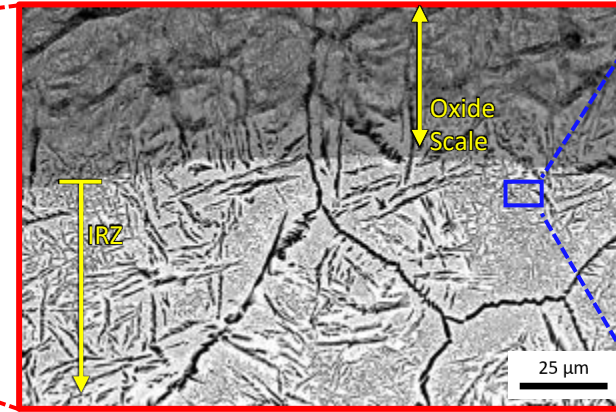
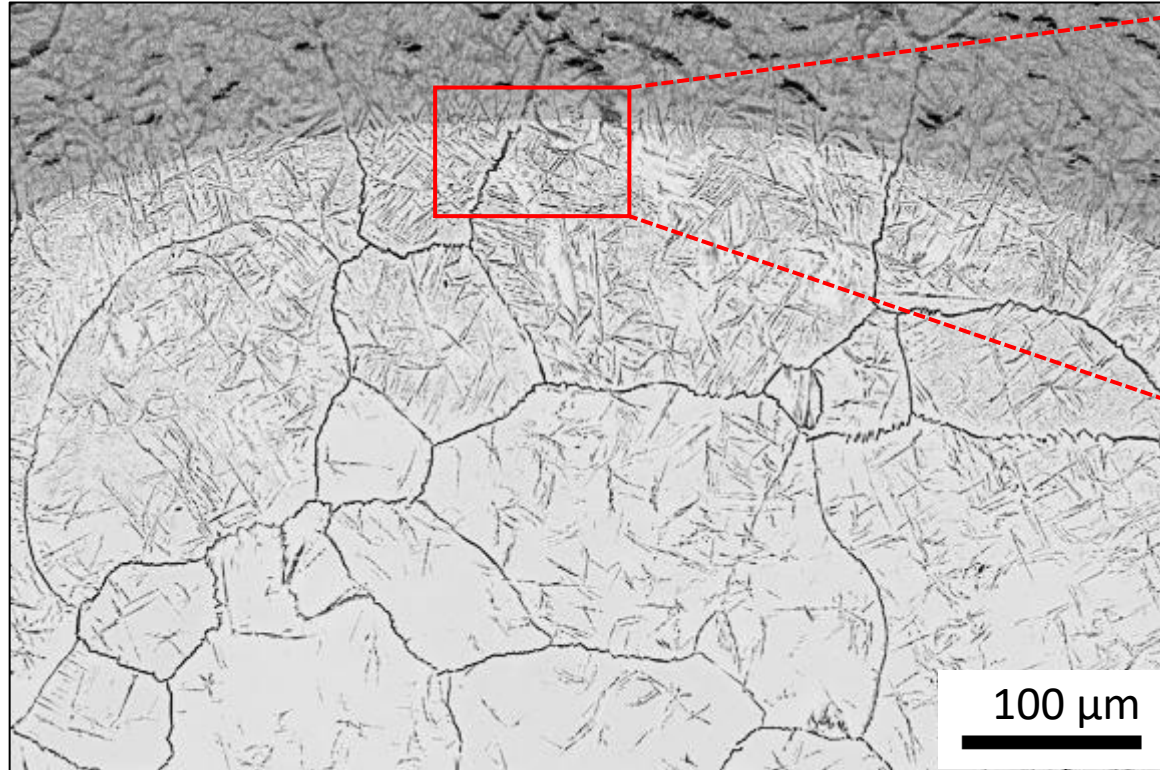
Ta₄TiCr₃
71.5 g/cm²



TaTiCr
7.2 g/cm²



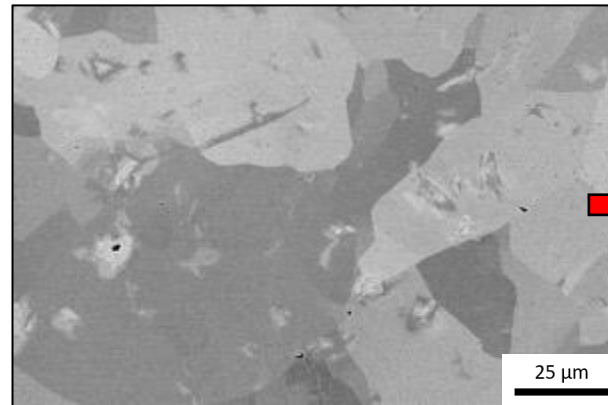
Post-oxidation microstructure – Ta₄Ti₃Cr (1200°C, 24 hrs)



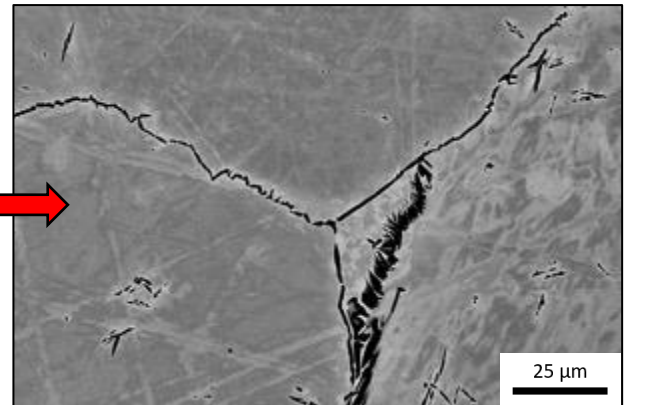
External scale: 1.29 mm
Internal reacted zone (IRZ): Through-thickness

- Thick oxide scale
- Through-thickness hcp precipitation along grain boundaries
- Fine Laves and hcp precipitates near oxide-IRZ interface

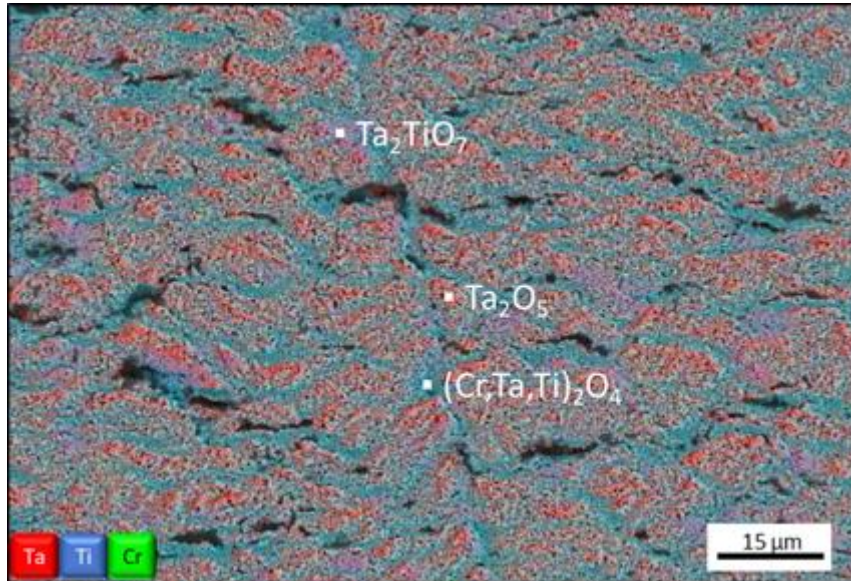
Bulk before oxidation



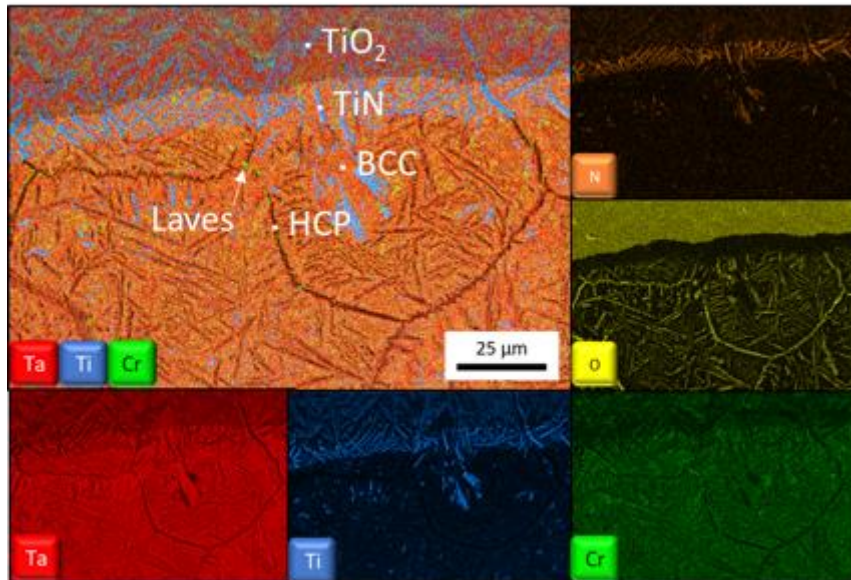
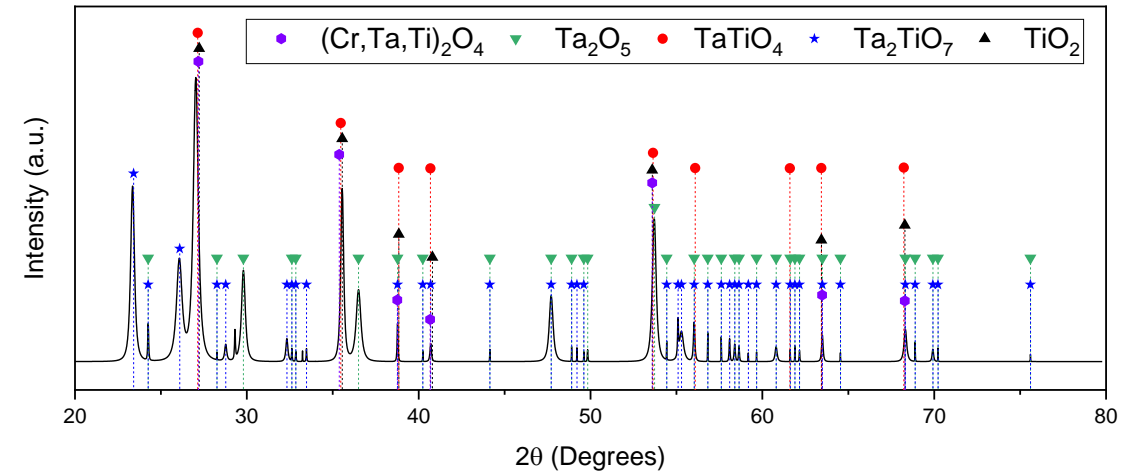
After 24 hrs at 1200°C



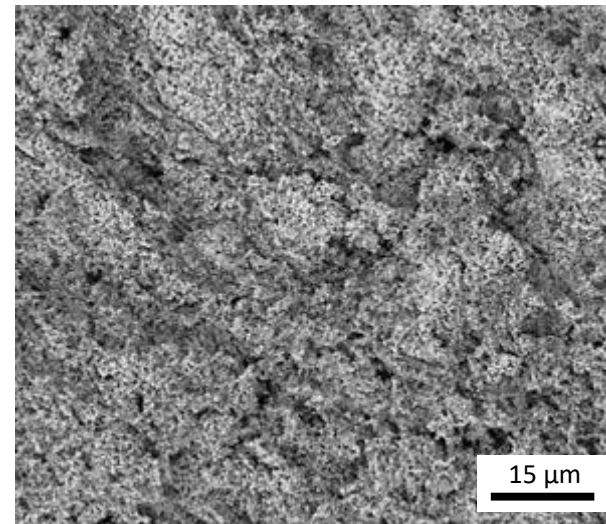
Oxide Products – Ta₄Ti₃Cr (1200°C, 24 hrs)



Powder XRD from oxide scale

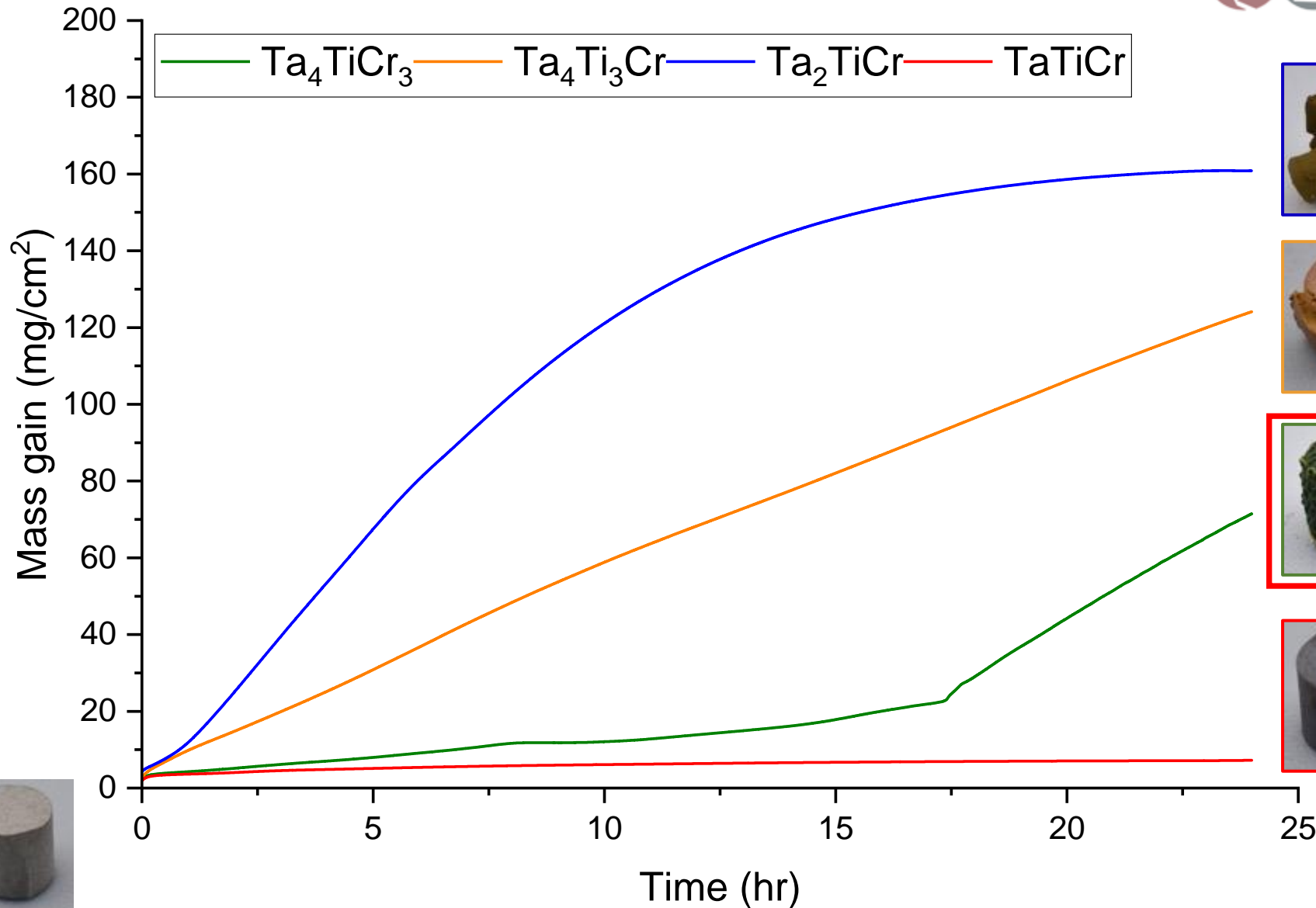


Scale surface



- Outer scale mostly Ta₂O₅ with branched (Cr,Ta,Ti)₂O₄ structures
- Matrix Ti depleted after oxidation, selectively oxidized

TGA Oxidation Tests – 1200°C



Ta₂TiCr
160.9 g/cm²



Ta₄Ti₃Cr
124.1 g/cm²



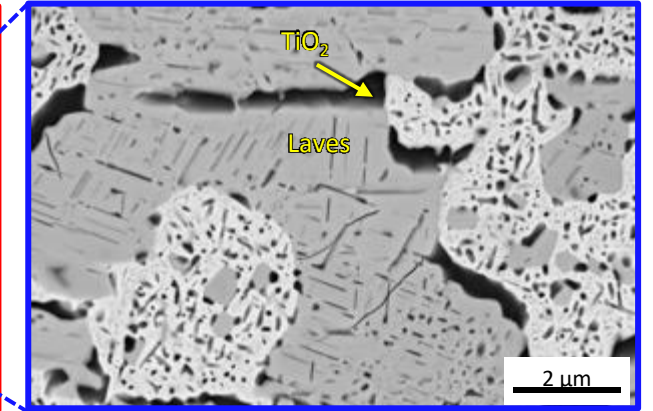
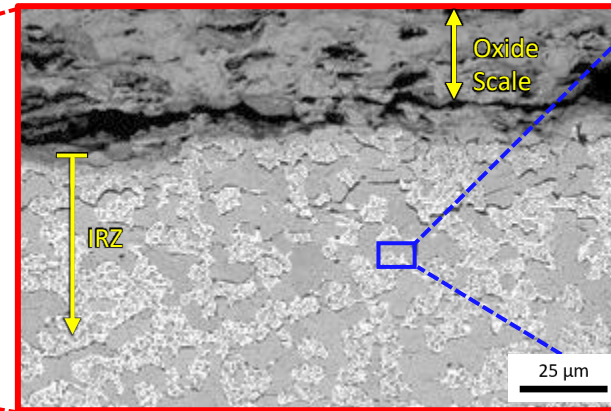
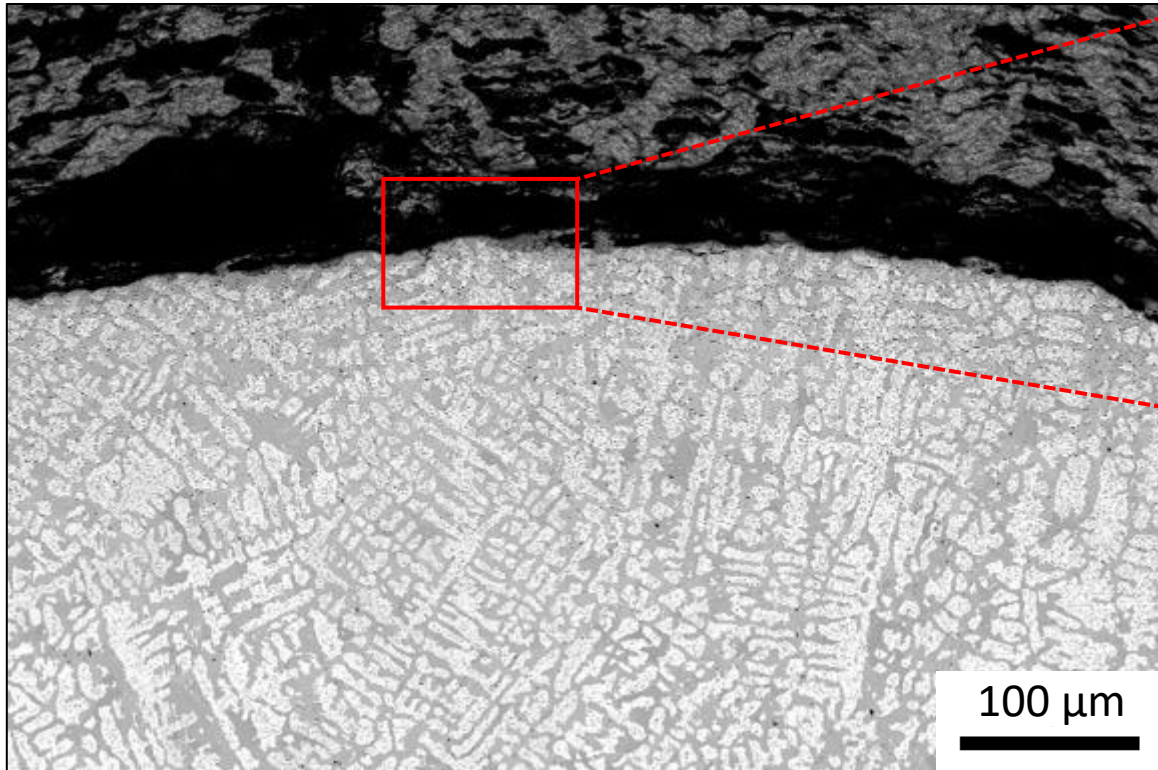
Ta₄TiCr₃
71.5 g/cm²



TaTiCr
7.2 g/cm²



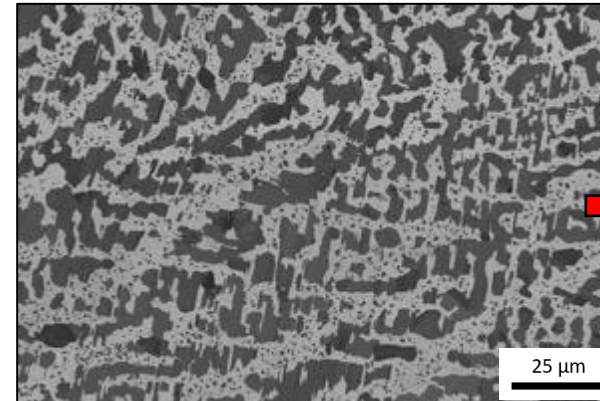
Post-oxidation microstructure – Ta₄TiCr₃ (1200°C, 24 hrs)



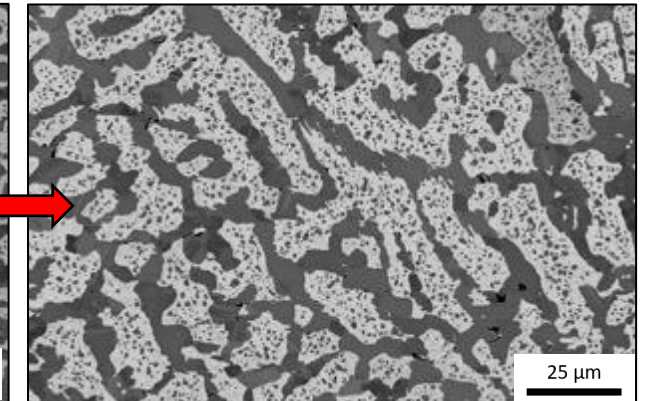
External scale: 600 μm
Internal reacted zone (IRZ): 100 μm

- Thick, separated scale
- Fine matrix precipitates and TiO₂ precipitations along phase boundaries near oxide-IRZ interface

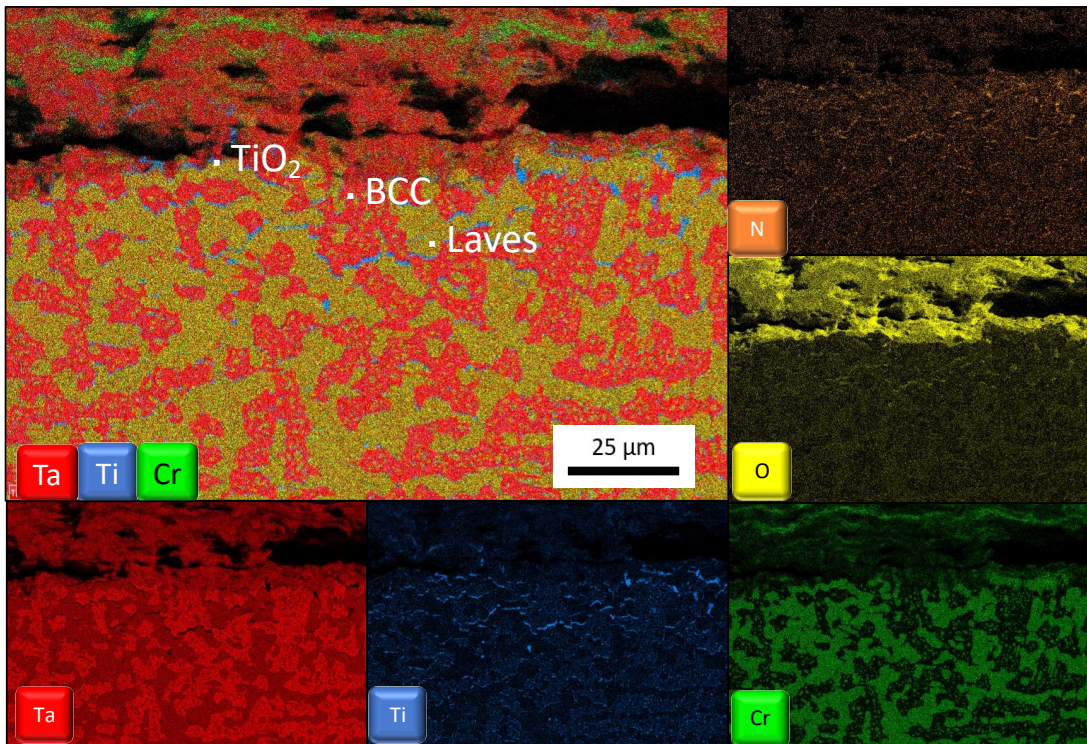
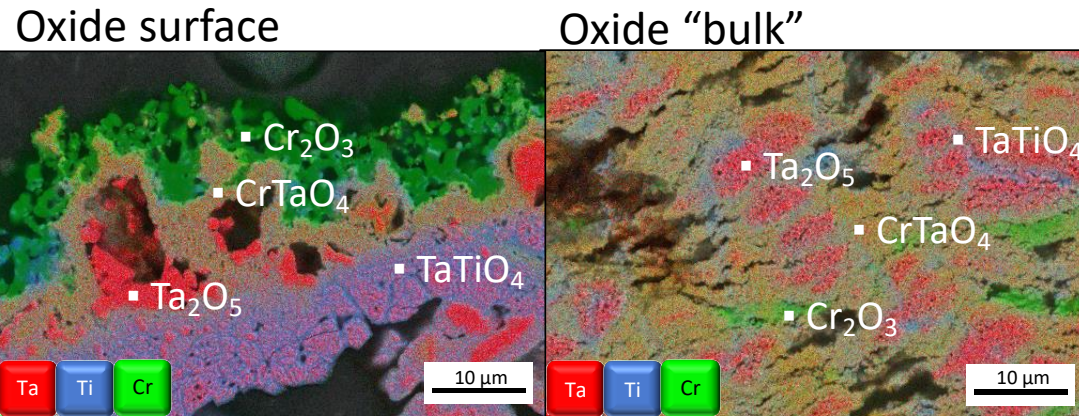
Bulk before oxidation



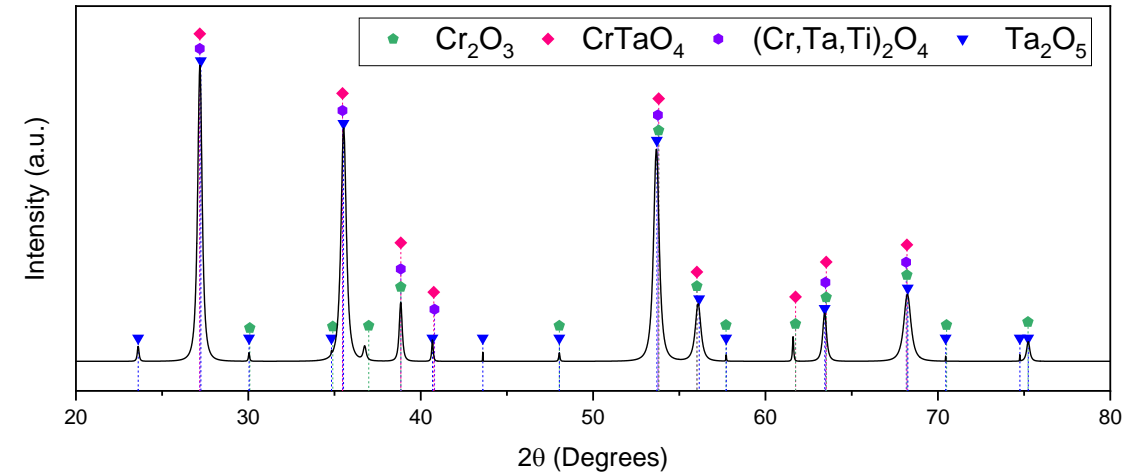
After 24 hrs at 1200°C



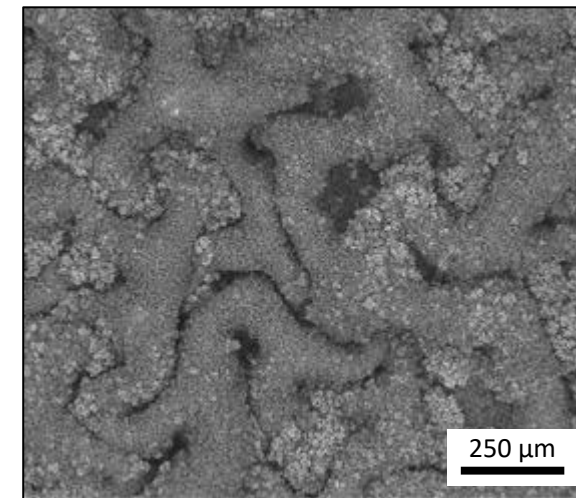
Oxide Products – Ta₄TiCr₃ (1200°C, 24 hrs)



Powder XRD from oxide scale

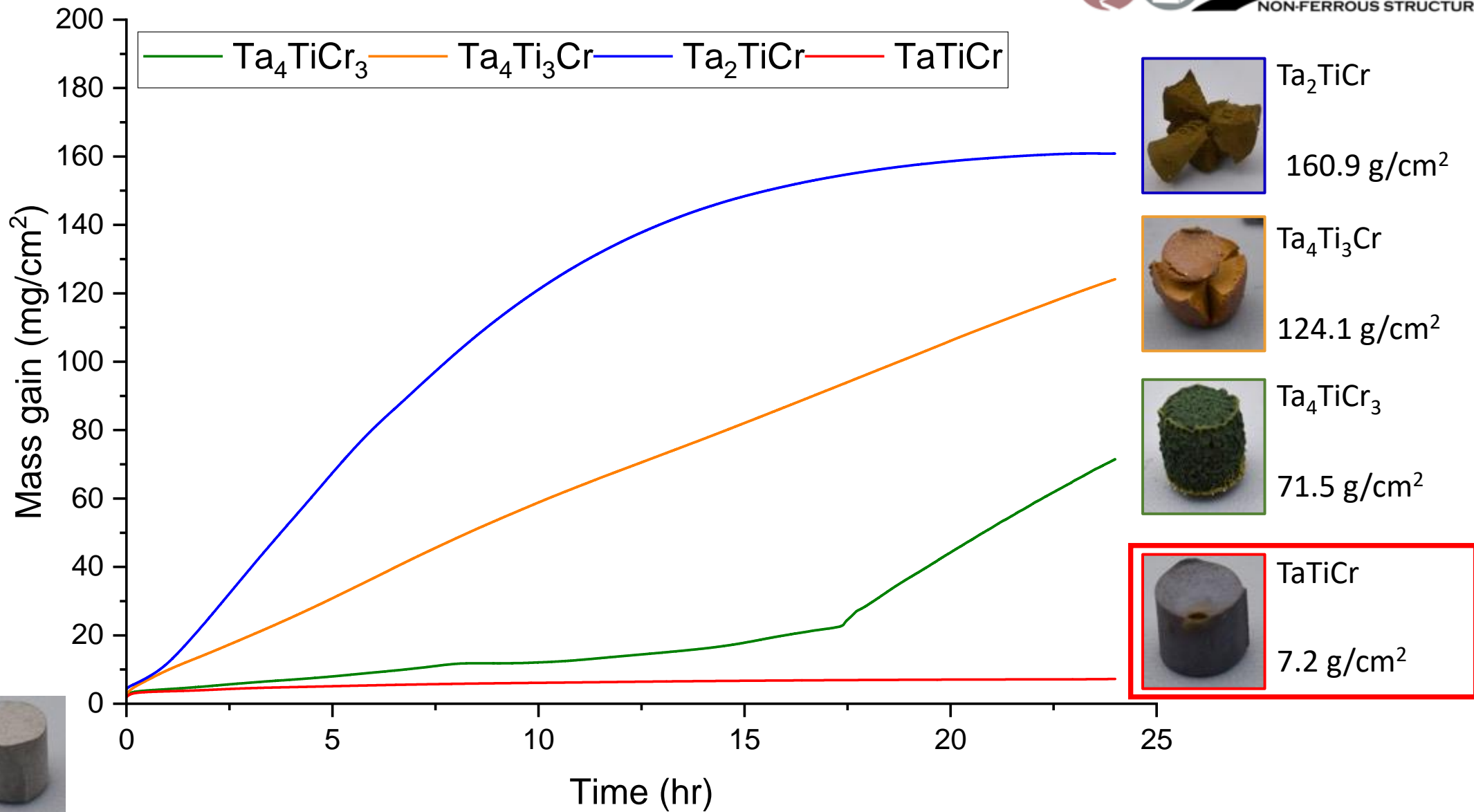






Scale surface



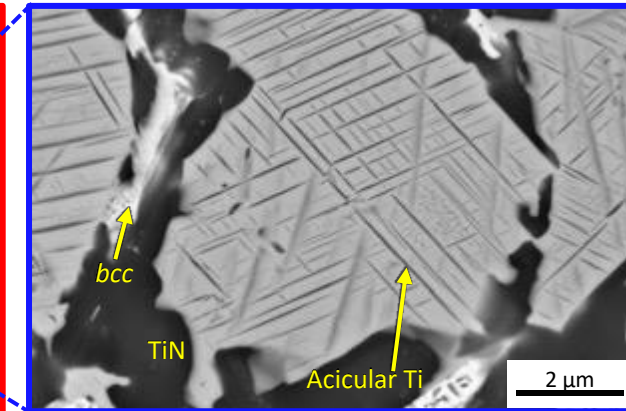
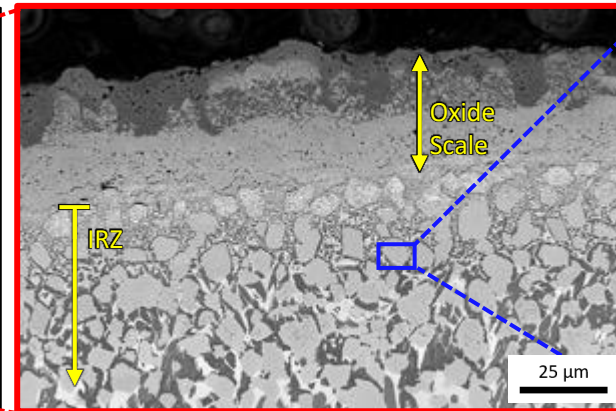
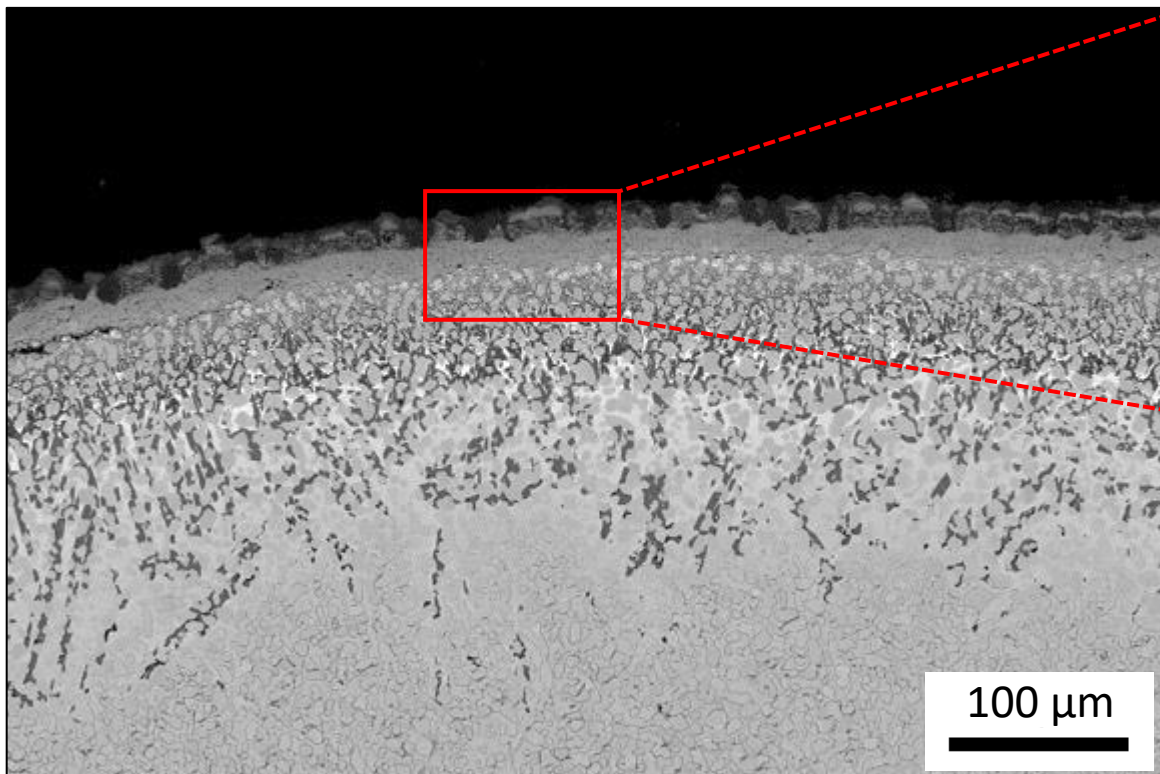
- 1st kinetic regime: Outer Cr₂O₃ layer provided good protection
- 2nd kinetic regime: Scale “rumpling” initiated due to volatilization, growth stress
- 3rd kinetic regime: breakaway oxidation and periodic structures

TGA Oxidation Tests – 1200°C



	Ta ₂ TiCr 160.9 g/cm ²
	Ta ₄ Ti ₃ Cr 124.1 g/cm ²
	Ta ₄ TiCr ₃ 71.5 g/cm ²
	TaTiCr 7.2 g/cm ²

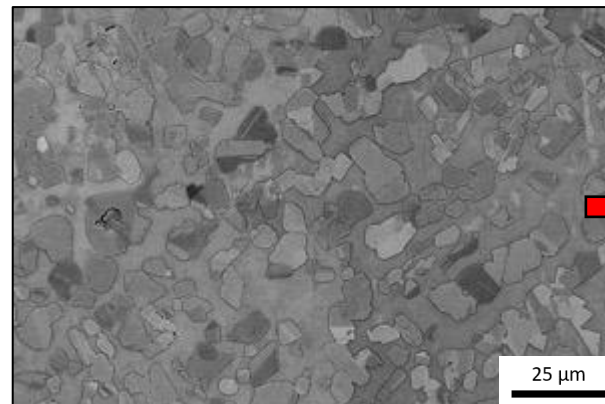
Post-oxidation microstructure – TaTiCr (1200°C, 24 hrs)



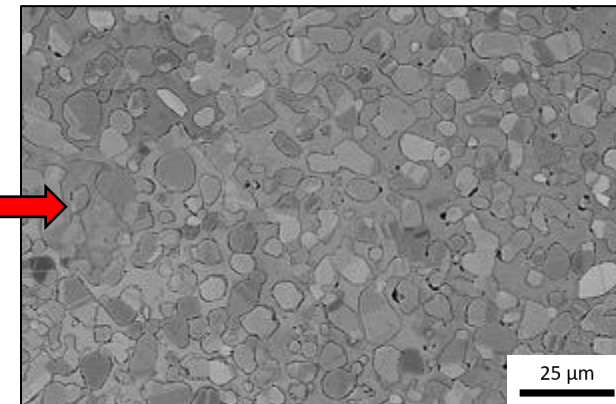
External scale: 30 μm
Internal reacted zone (IRZ): 170 μm

- Adherent, layered oxide scale
- Coarse, lenticular TiN precipitates in matrix from high Ti matrix concentration
- Fine, acicular Ti-rich precipitates in Laves particles near oxide-IRZ interface

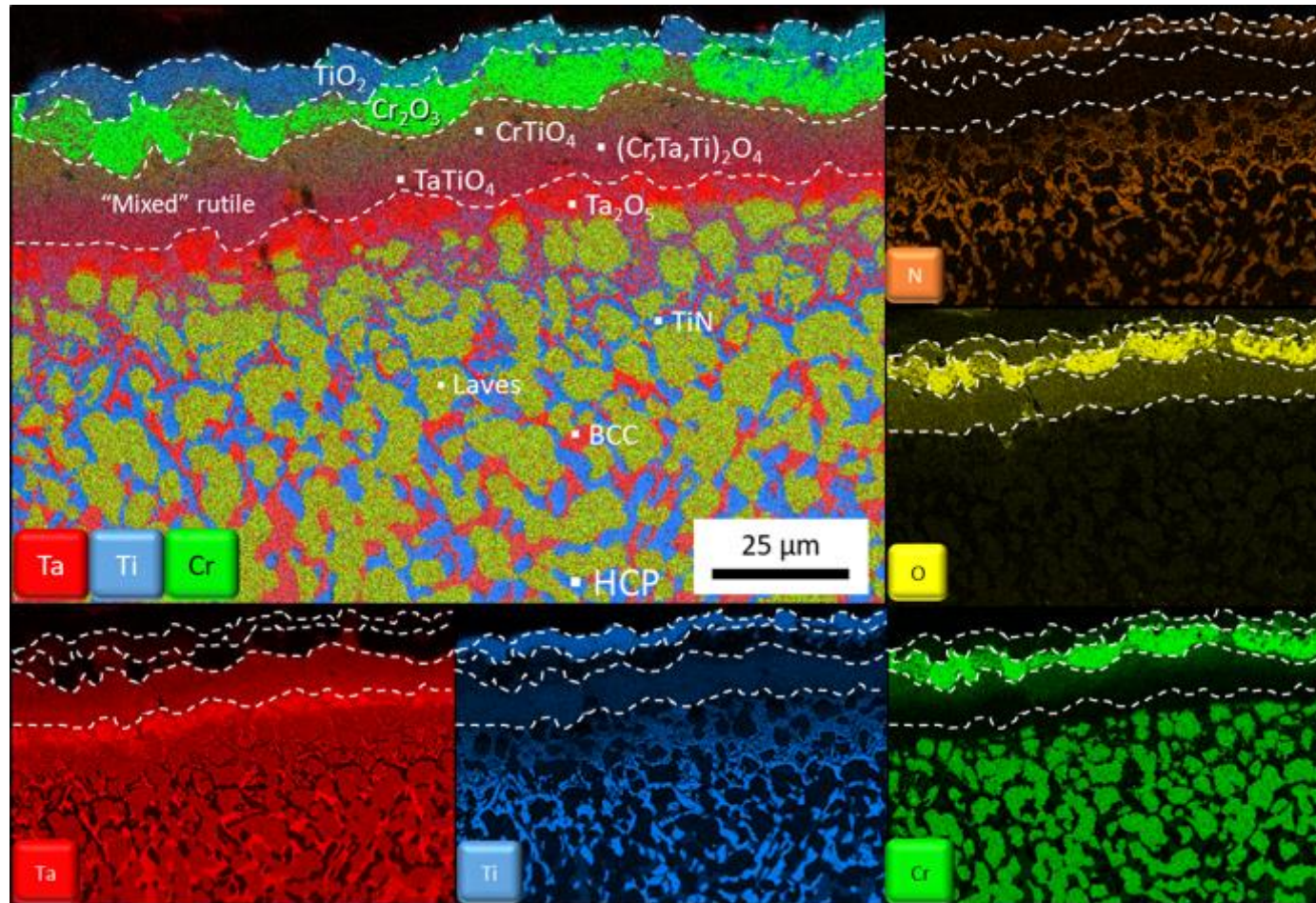
Bulk before oxidation



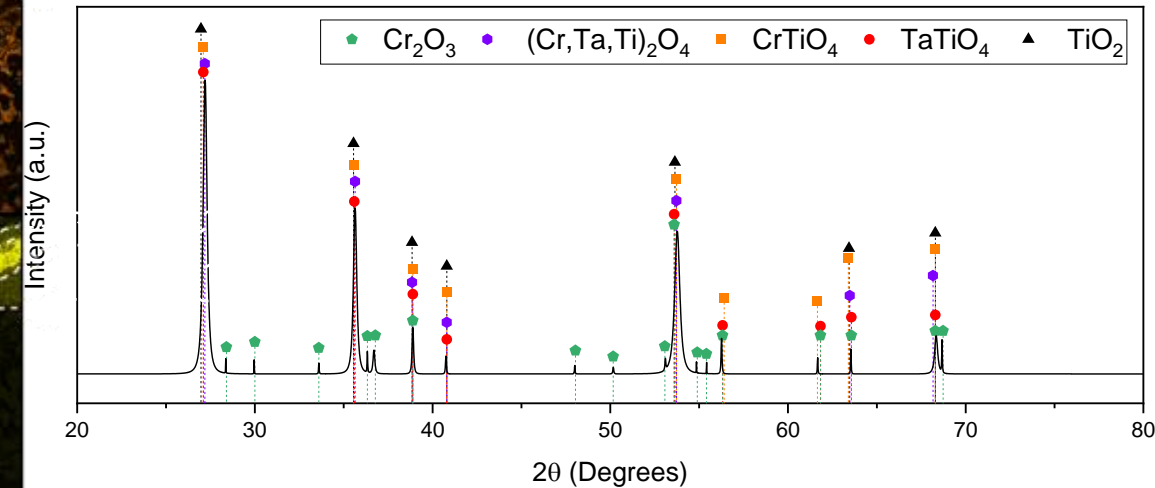
After 24 hrs at 1200°C



Oxide Products – TaTiCr (1200°C, 24 hrs)



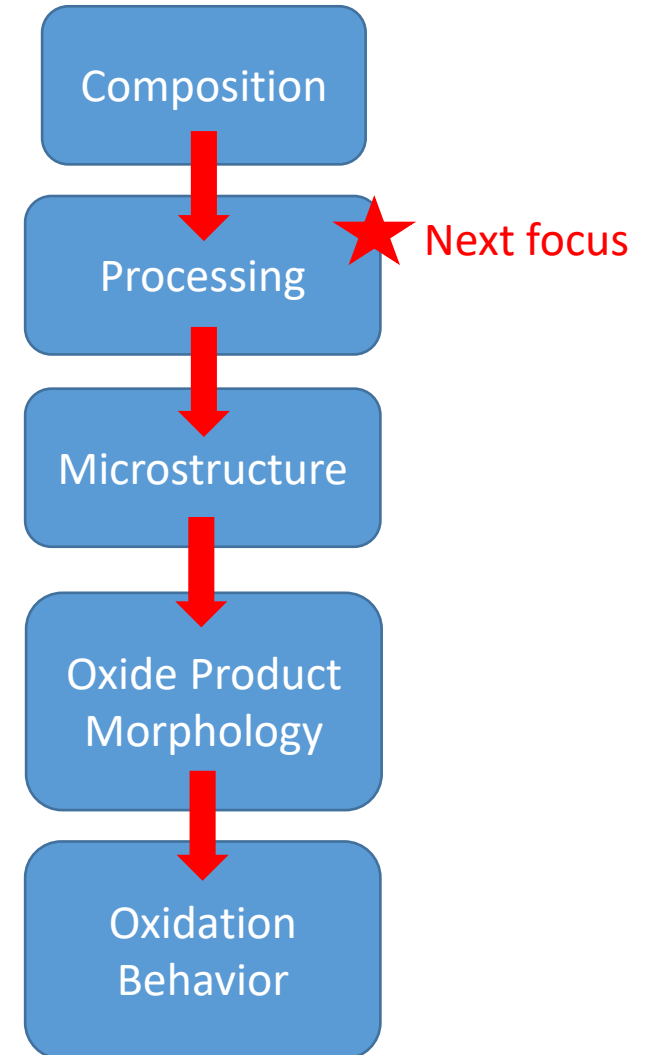
Powder XRD from oxide scale



- Outer scale contains TiO_2 , Cr_2O_3 , and "mixed" rutile structured CrTiO_4 , $(\text{Cr,Ta,Ti})_2\text{O}_4$, and TaTiO_4
- Coarse TiN morphology in IRZ may support continuous, protective scale growth

Conclusions

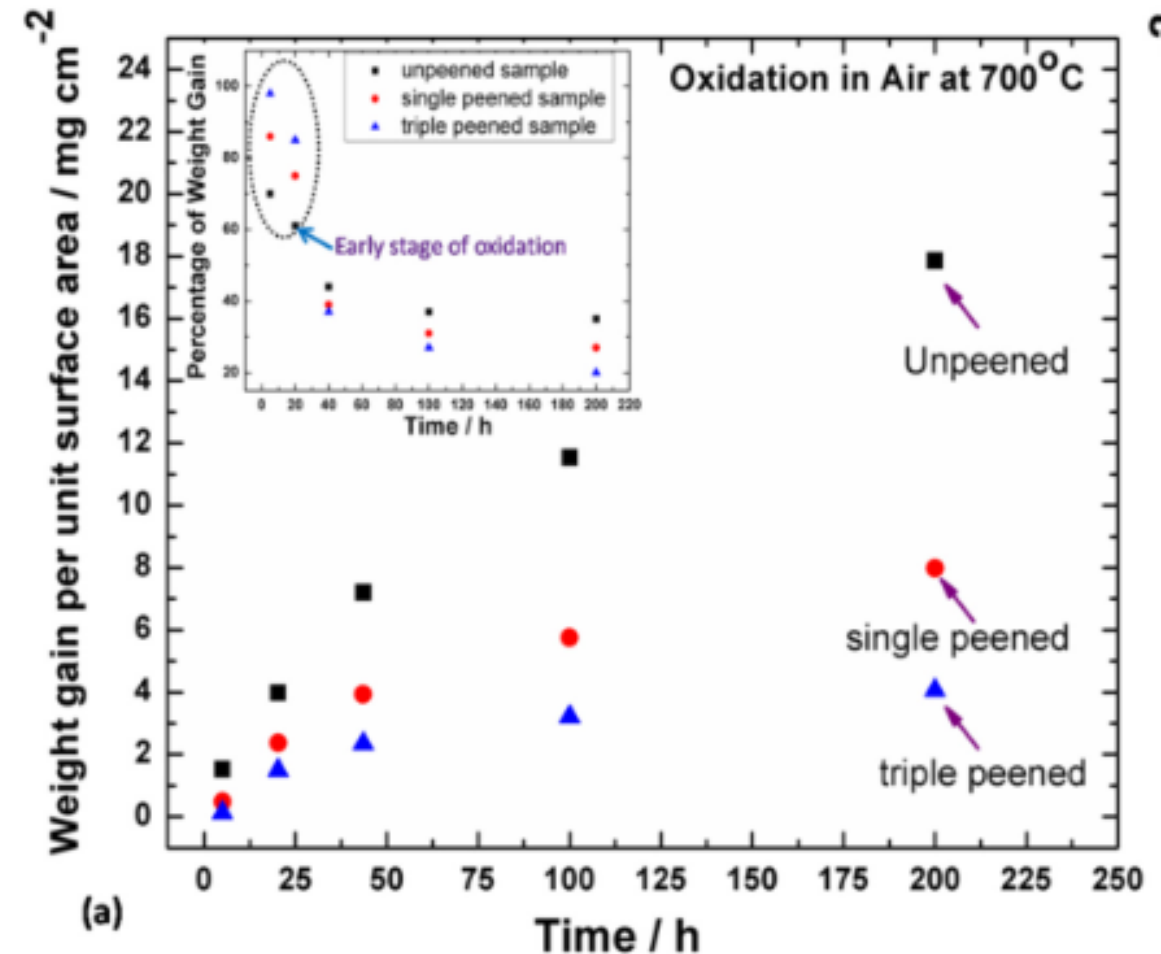
- All alloys formed similar oxide structures, however oxide morphology varied drastically
- Good performance requires continuous oxide morphology and no deleterious oxide formation
- Laves act as "Cr reservoirs" for Cr_2O_3 formation, coarse internal TiN morphology may reduce O ingress and support continuous oxide morphology
- Design for:
 - Laves phase to provide Cr
 - High Ti content in matrix to form advantageous TiN morphology
 - Low Ta content to dissuade Ta_2O_5 formation



Future work

AM and LSP surface modification

- Explore Ta-lean/Ti-rich compositions using Optomec Laser Engineered Net Shaping (LENS) system and measure oxidation performance in as-printed/HIPed conditions
- Investigate effect of Laser Shock Peening (LSP) on TaTiCr as an oxidation inhibitor and a recrystallization starter to modify surface microstructure



Mass gain of grade P91 steel in unpeened, single peened, and triple peened conditions

Future Work



- Planned publication: *High-Temperature Oxidation Behavior of TaTiCr, Ta₄Ti₃Cr, Ta₂TiCr, and Ta₄TiCr₃ Concentrated Refractory Alloys*
- Compression Tests on HIP specimens
- Composition range exploration with AM
- Laser Shock Peening Experiments

Thank you!
Noah Welch
njwelch@iastate.edu

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Noah Welch
njwelch@iastate.edu

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