

# ***Project 34: In-situ Observation of Phase and Texture Evolution Preceding Abnormal Grain Growth in Ni-based Aerospace Alloys***

***Fall Meeting***

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# Project 34: In-situ Observation of Phase and Texture Evolution Preceding Abnormal Grain Growth in Ni-based Superalloys



- Student: Byron McArthur (Mines)
- Advisors: Amy Clarke, Kester Clarke, Michael Kaufman (Mines)

**Project Duration**  
PhD: Nov 2017. to March. 2021

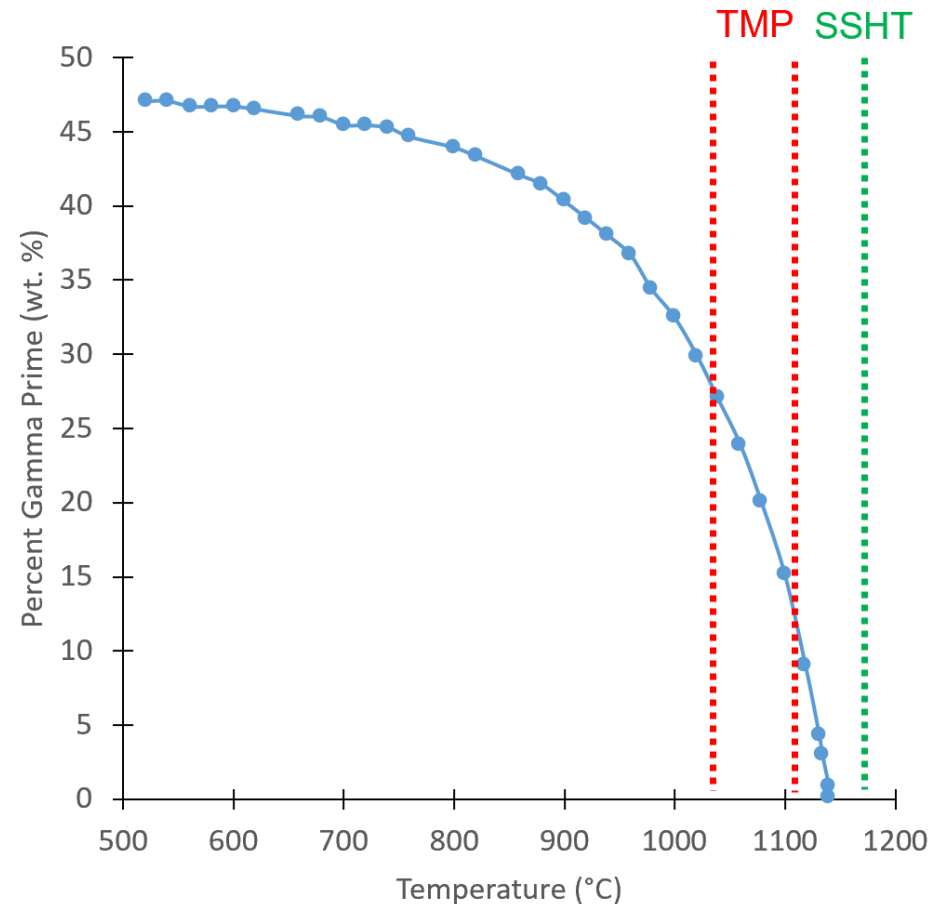
- **Problem:** Abnormal grain growth (AGG) in Ni-based superalloys (RR-1000) significantly reduces mechanical properties and occurs as a result of forging parameters.
- **Objective:** Determine the mechanism of abnormal grain growth in Ni-based superalloys using ex-situ and in-situ characterization techniques.
- **Benefit:** Improved mechanical properties for turbine disk alloys.

- Recent Progress**
- Developing mechanistic theory for AGG
  - Performed interrupted heat treatment processing to determine mechanisms for abnormal grain growth

Metrics		
Description	% Complete	Status
1. Literature review	95%	●
2. Explore abnormal grain growth forging parameters for RR1000	95%	●
3. Ex-situ and interrupted material testing and characterization	90%	●
4. Develop and test theory to explain abnormal grain growth phenomena	90%	●
5. Propose and test methods for alleviating abnormal grain growth in industrial processing	75%	●

# Material: RR1000, $\gamma$ - $\gamma'$

- Processing:
  - Powder metallurgy
  - Hot isostatic pressure compaction
  - Extruded at 5:1 ratio
  - Isothermal forging: 1035-1110°C
    - Performed in Gleeble®
  - Super solvus heat treatment (SSHT)
    - 1150-1170°C
    - Performed in dilatometer
- Critical AGG parameters:
  - Strain
  - Strain rate
  - Forging temperature
  - Heating rate to super solvus hold



M.C. Hardy, B. Zirbel, G. Shen, R. Shankar. Developing damage tolerance and creep resistance in a high strength nickel alloy for disc applications, *Superalloys 2004* 83-90 (2004).

# Isothermal Forging

- Sub-  $\gamma'$  solvus temperature
- Low strain rate
- Maintain superplastic deformation for decreased forging loads
- Primary  $\gamma'$  pins  $\gamma$  grain boundaries
  - Secondary  $\gamma'$  less effective or dissolved
- Low stored energy accumulation
  - Grain boundary sliding (Coble creep)
  - Dynamic recovery
  - Dynamic recrystallization

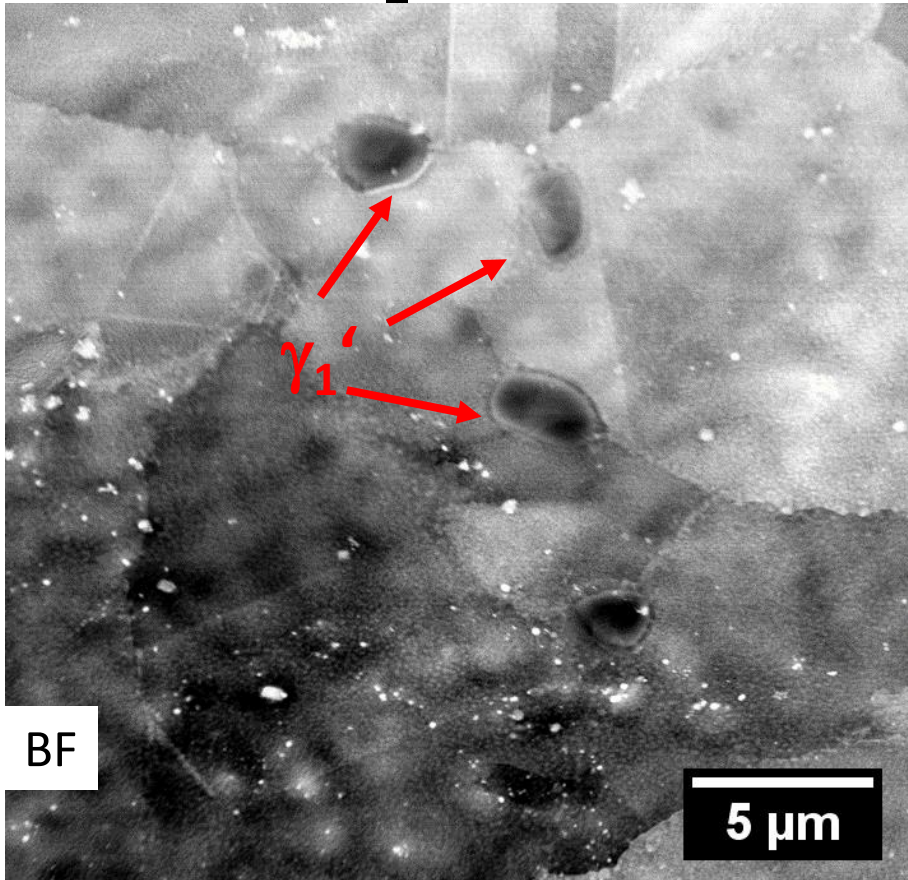


Forging ~1 Meter Diameter

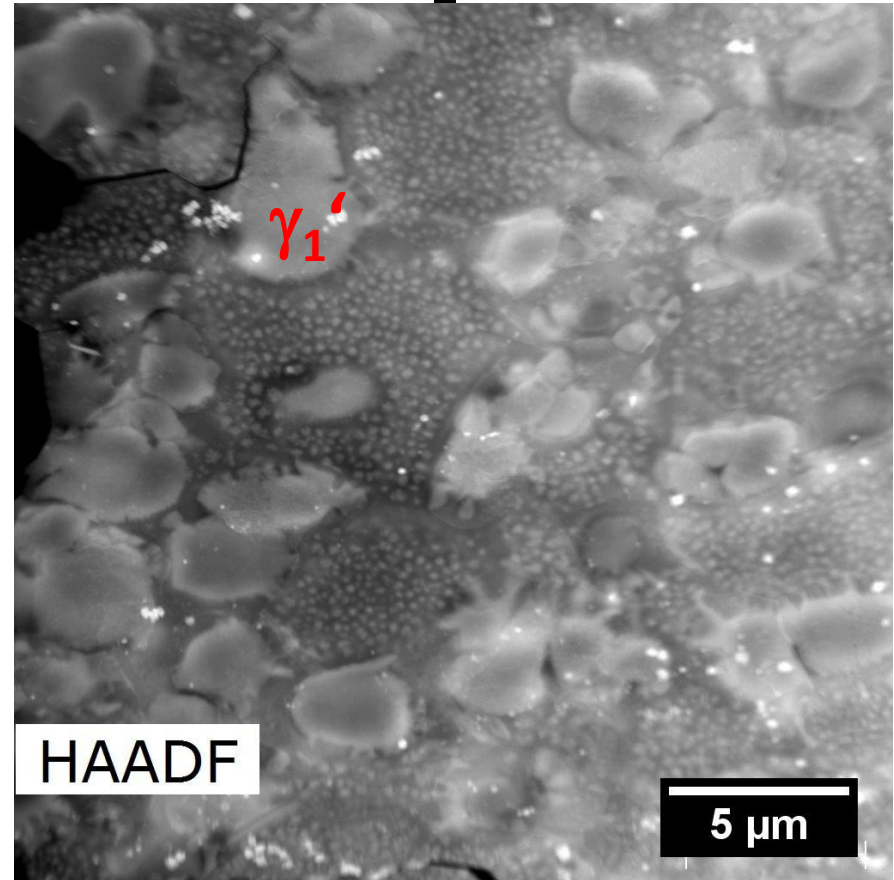
Mitchell, R. J., Lemsky, J. A., Ramanathan, R., Li, H. Y., Perkins, K. M., & Connor, L. D. *Superalloys 2008*, pp. 347–356.

# As-received Material

Low  $\gamma_1'$  Fraction



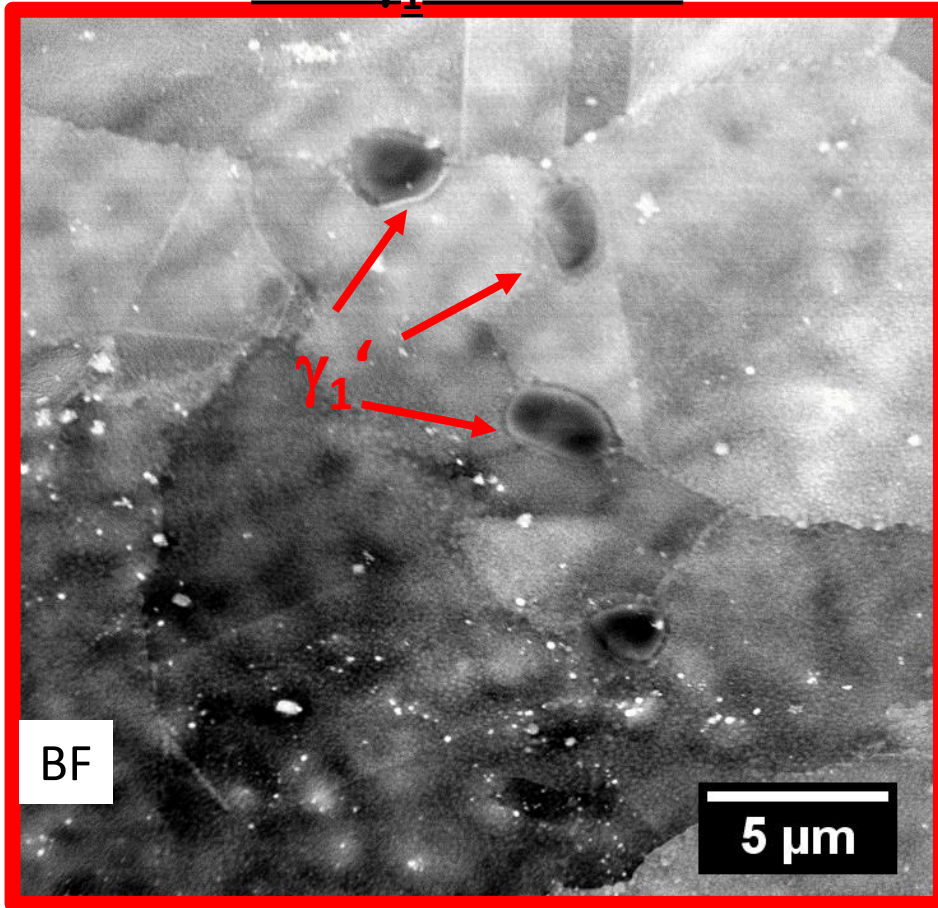
High  $\gamma_1'$  Fraction



Thanks to Yaofeng Guo for TEM imaging

# As-received Material

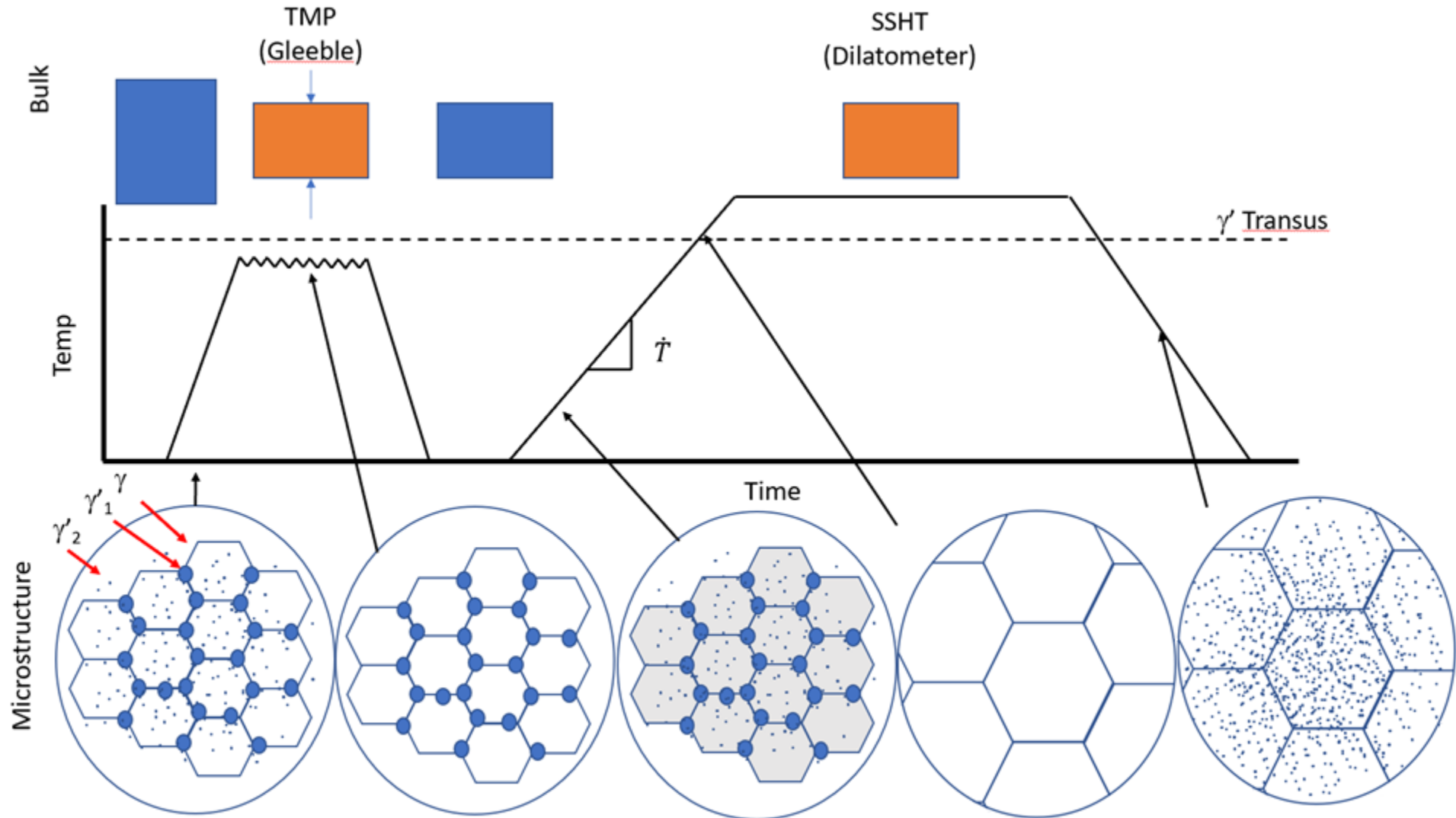
## Low $\gamma_1'$ Fraction



- Lower  $\gamma_1'$  demonstrated AGG
- Higher  $\gamma_1'$  showed no AGG
- $\gamma'$  size influences deformation mechanism, stored energy, and recrystallization
- Higher  $\gamma_1'$  may be used later for further development or support of AGG theory

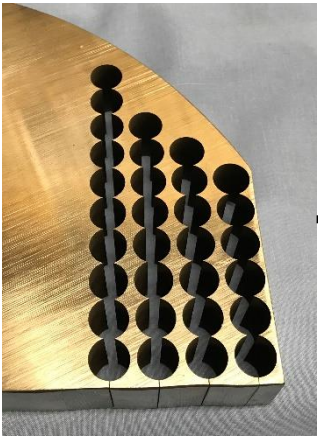
Thanks to Yaofeng Guo for TEM imaging

# Processing and Microstructure

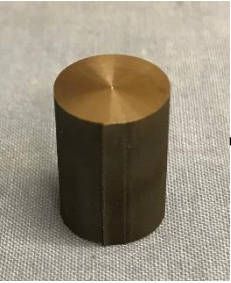


# Experimental Procedure

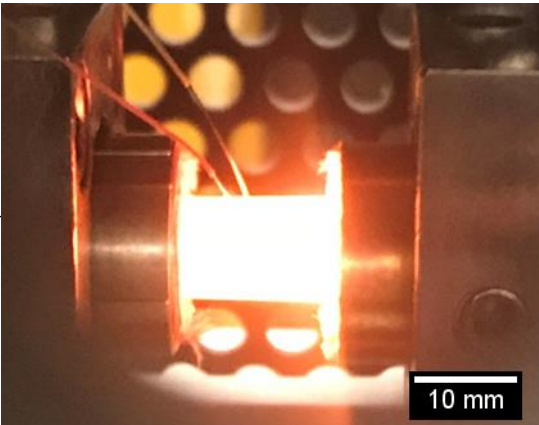
Wire-EDM



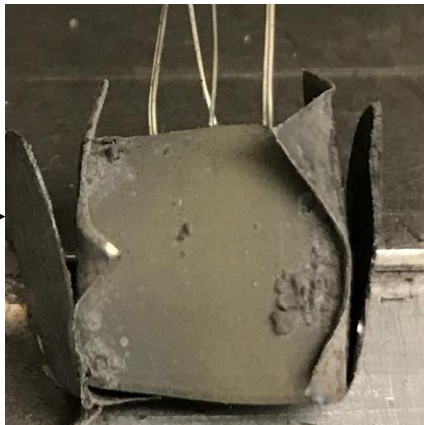
Machine to length  
with parallel faces



Isothermal forging  
in Gleeble®



Thermocouple  
locations



As-deformed  
Specimen



Dilatometer  
Specimen for SSHT

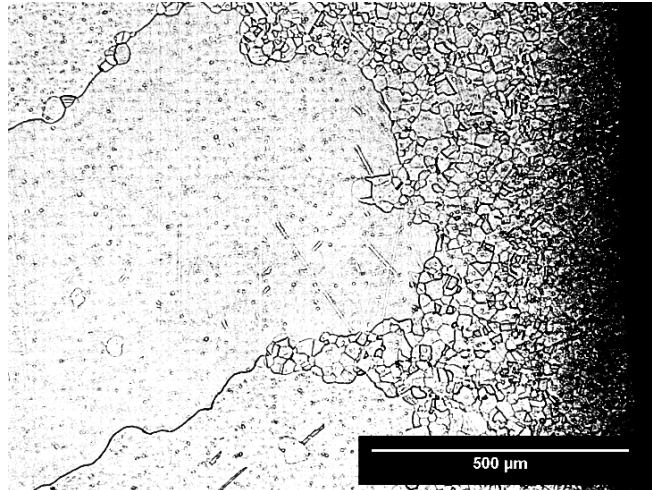
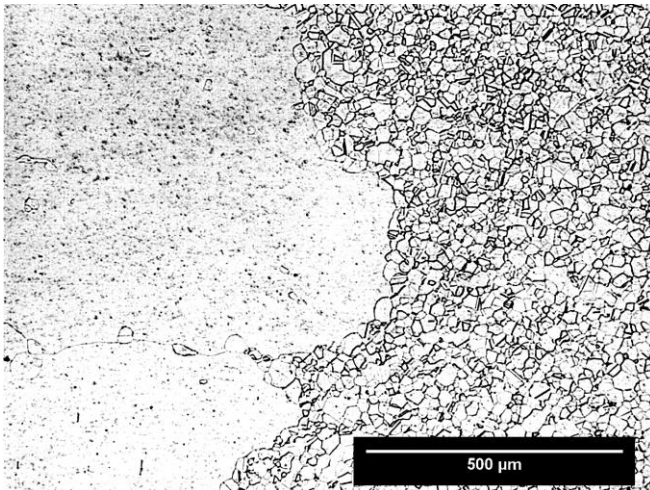


SSHT Specimen



# Summary of Prior Work & Results

- Replicate industrial processing that leads to AGG in lab-scale testing
  - High temperature, low strain & strain rate, low SSHT heating rate
  - Forging: 1110-1120°C,  $10^{-3} \text{ s}^{-1}$ , 0.15  $\epsilon$
  - Heating Rate: 8°C/min
- Determine influential processing parameters and their roles
  - Varying parameters shift AGG based upon stored energy
- Consistently produce AGG via Gleeble TMP and heat treating
- Exploring experimental techniques to detail phenomena

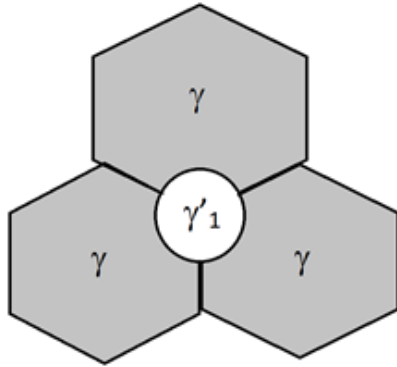


# Theory of Abnormal Grain Growth

# Coherent $\gamma$ Recrystallization

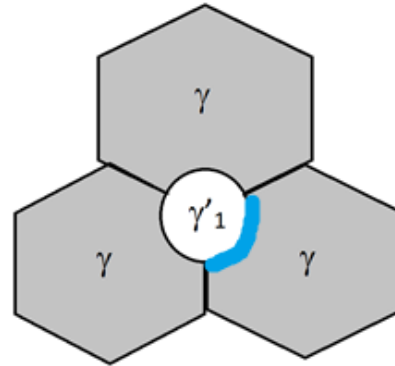
## Hetero-epitaxial Recrystallization (HERX) (Charpagne)

1



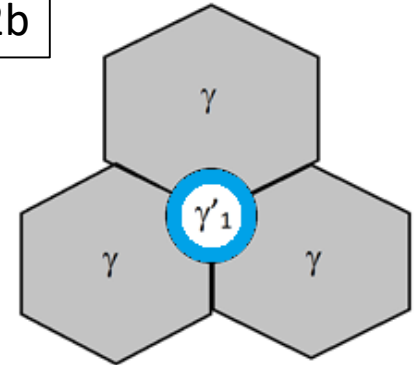
$\gamma'_1$  is incoherent with neighboring  $\gamma$

2a

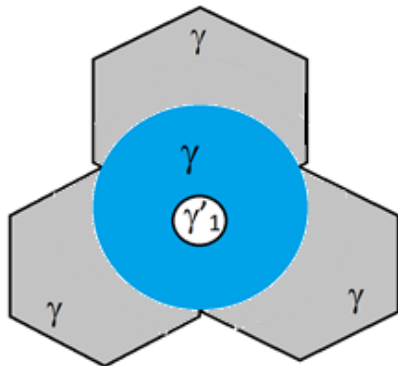


$\gamma$  nucleates coherently off  $\gamma'_1$  or during order-disorder transformation

2b



3



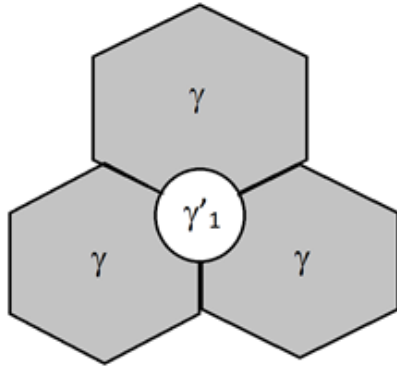
Growth to consume stored energy in  $\gamma$

- Possible  $\gamma$ - $\gamma'$  disorder-order transformation induced, or coherent nucleation
- Reduced energy barrier for nucleation
- Explains required heating rate
  - HERX occurs before RX
  - Growth until hard impingement
- $\gamma'_1$  serves as nucleation sites
- Different than particle stimulated nucleation

# Coherent $\gamma$ Recrystallization

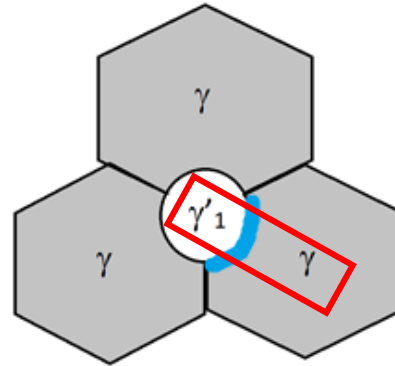
## Hetero-epitaxial Recrystallization (HERX) (Charpagne)

1



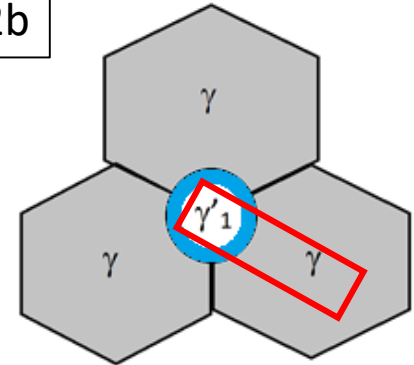
$\gamma'_1$  is incoherent with neighboring  $\gamma$

2a

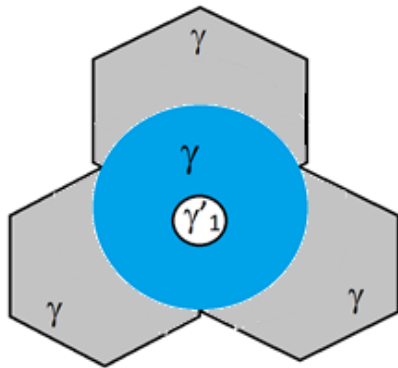


$\gamma$  nucleates coherently off  $\gamma'_1$  or during order-disorder transformation

2b



3



Growth to consume stored energy in  $\gamma$

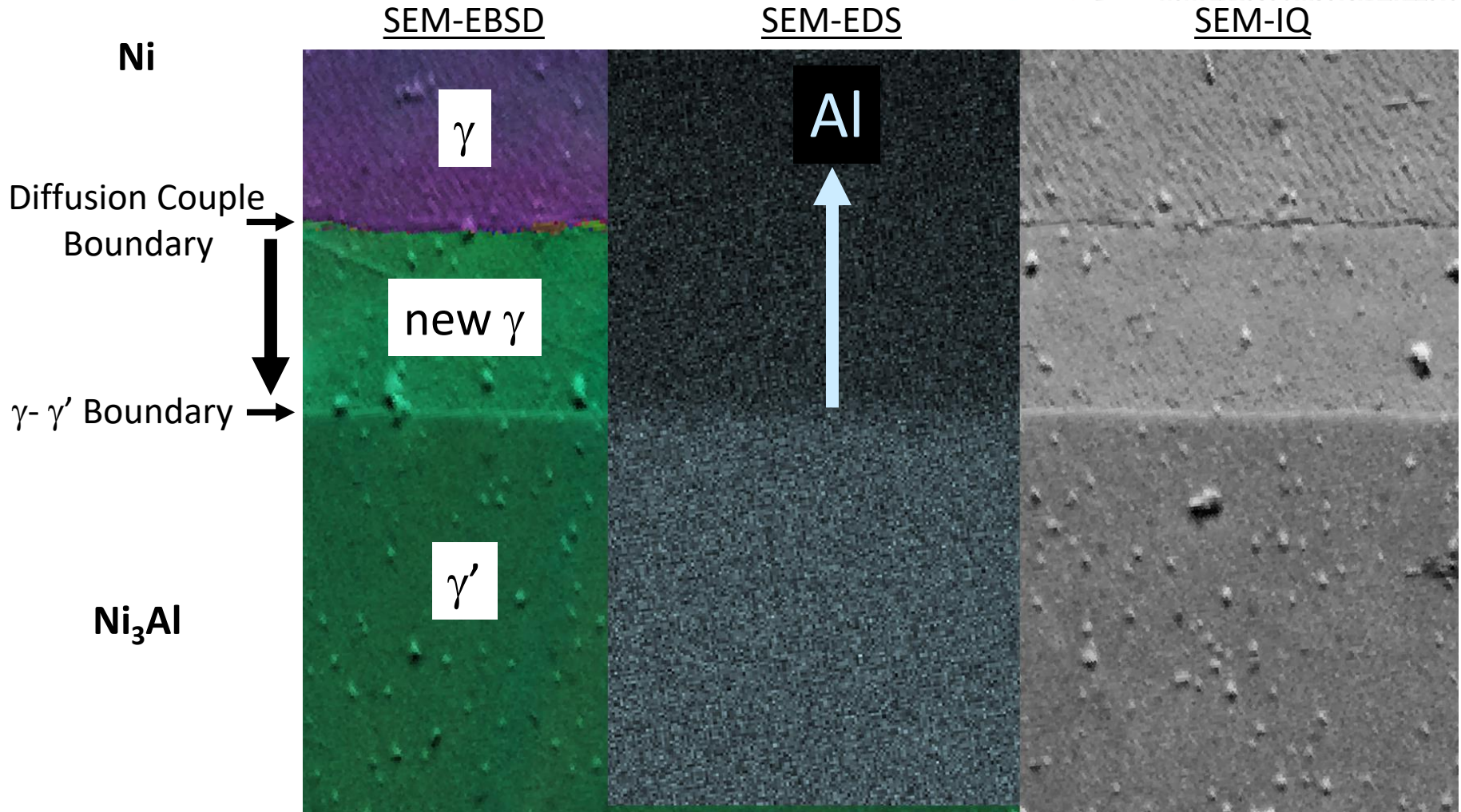
- Want to observe microstructural development at interface
- Occurs at  $\sim 1080-1110^\circ\text{C}$
- Rapidly in limited instances
- Statistically difficult with 2-D sectioning

# Mesososcopic $\gamma$ - $\gamma'$ Interface Study

- Diffusion couple to create  $\gamma$ - $\gamma'$  interface
- $\gamma'$  created through  $\text{Ni}_3\text{Al}$  button melted specimen
  - Stoichiometric composition
  - Homogenized at  $1000^\circ\text{C}$  for 24 hours
- Pure nickel for  $\gamma$
- Aluminum diffusion driving  $\gamma' - \gamma$  transformation
- Polished, flat surfaces in dilatometer ( $10^{-6}$  torr)
- $1000^\circ\text{C}$  for 4 hours



# Diffusion Couple $\gamma - \gamma'$



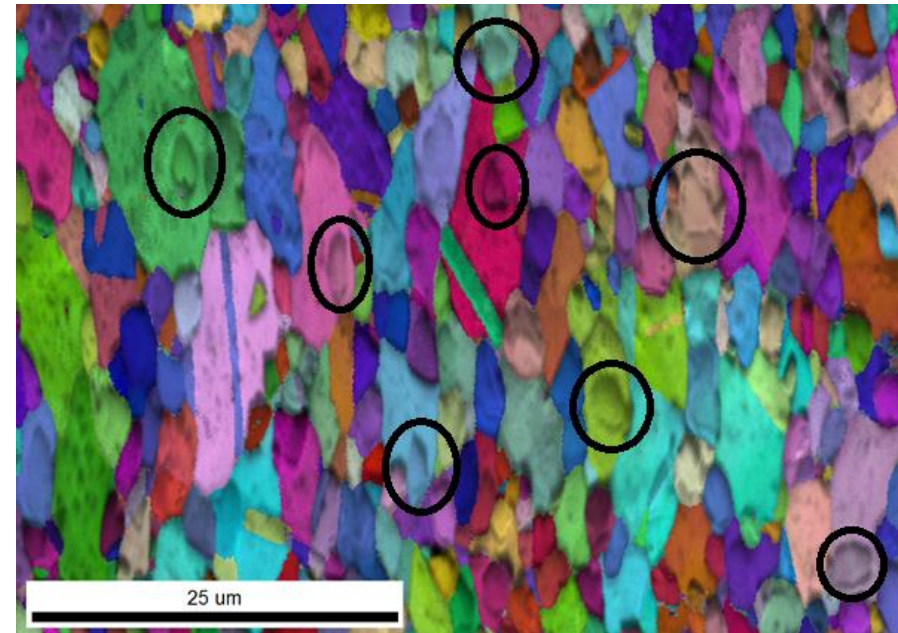
Experiment demonstrates formation of new  $\gamma$  and  $\gamma - \gamma'$  boundary is energetically favored over movement of existing  $\gamma - \gamma'$  boundary.

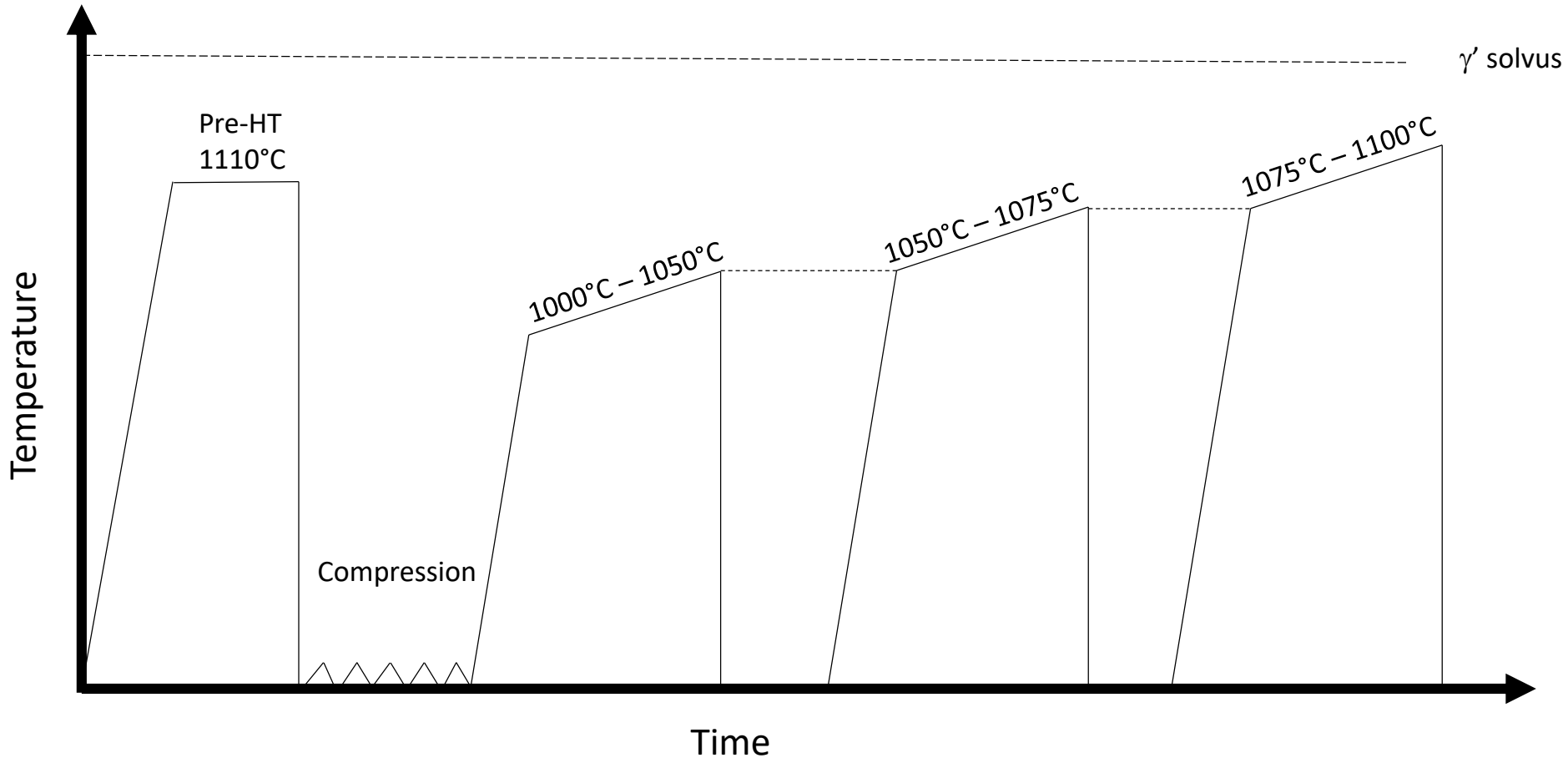
# Interrupted Heat Treatments

## Methods:

- Utilize room temperature deformation for homogeneous, controlled distribution of stored energy
- Pre-heat treatment to remove existing  $\gamma'_1$  coherent with matrix  $\gamma$ 
  - Sub-solvus heat treatment (1110°C)
  - DRX or MDRX sourced
- Interrupted heating intervals at controlled heating rate
  - Viewing same region

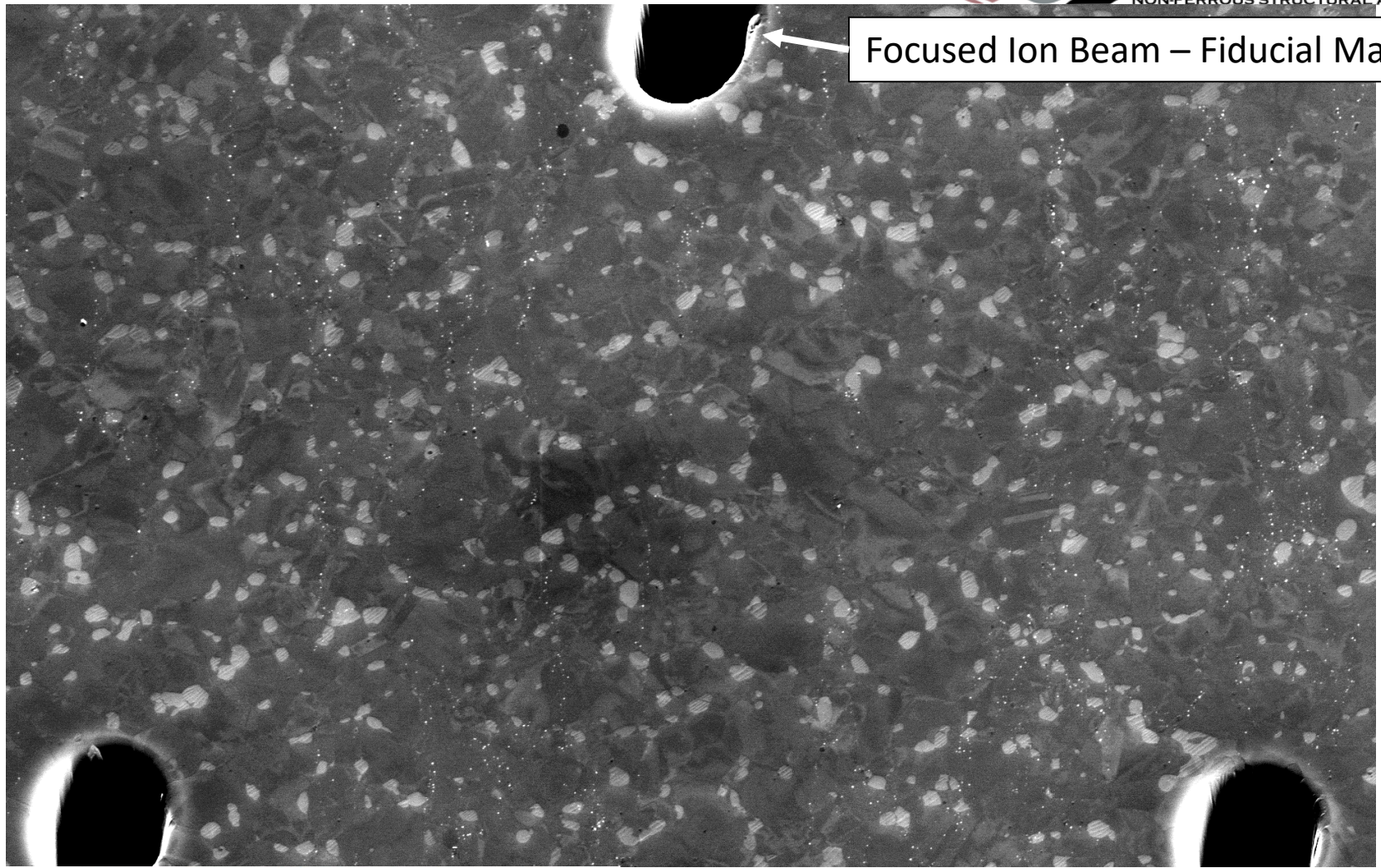
As-Received Microstructure







# Interrupted Heat Treatments SEM/SEI – As Deformed

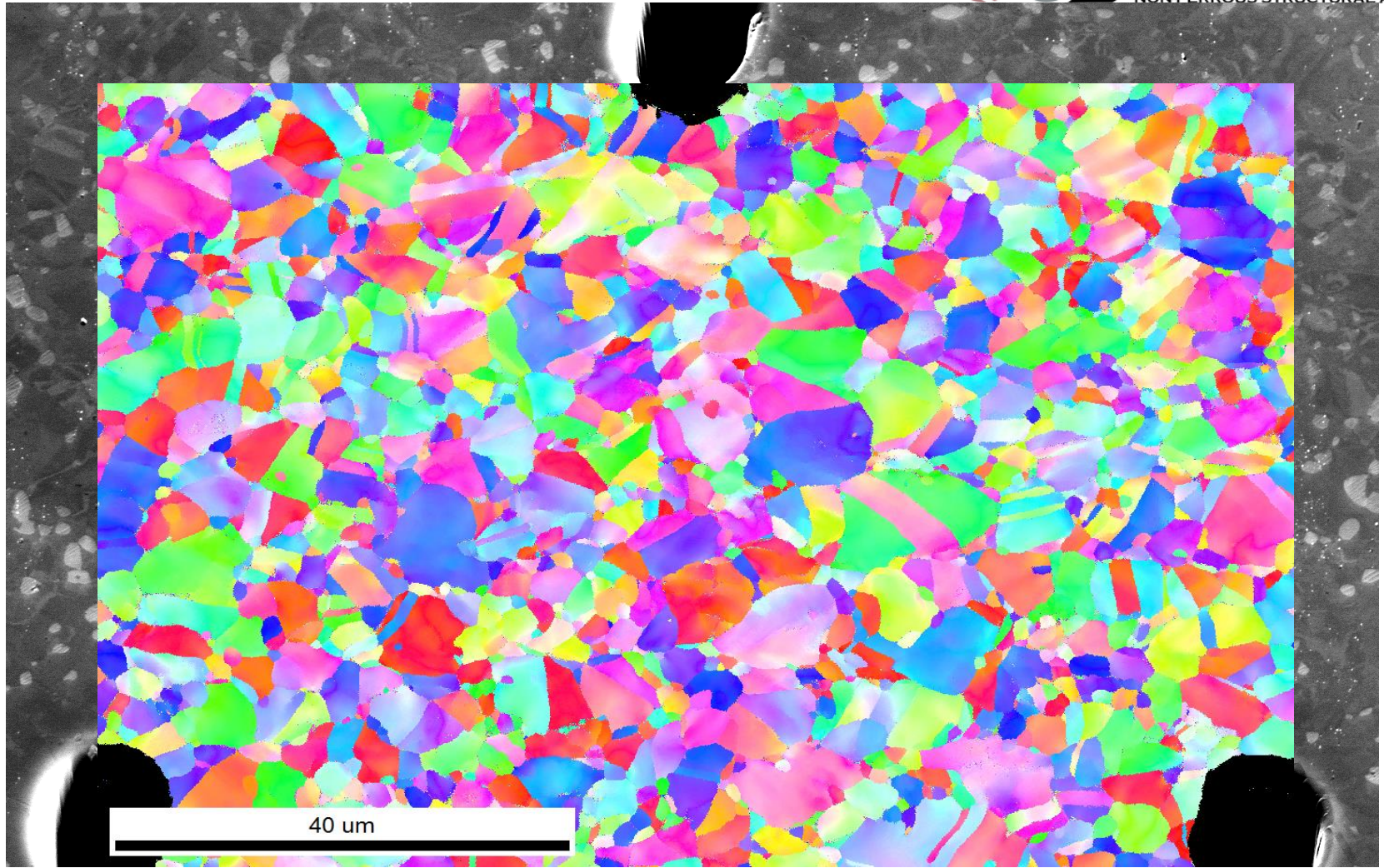


Focused Ion Beam – Fiducial Marks

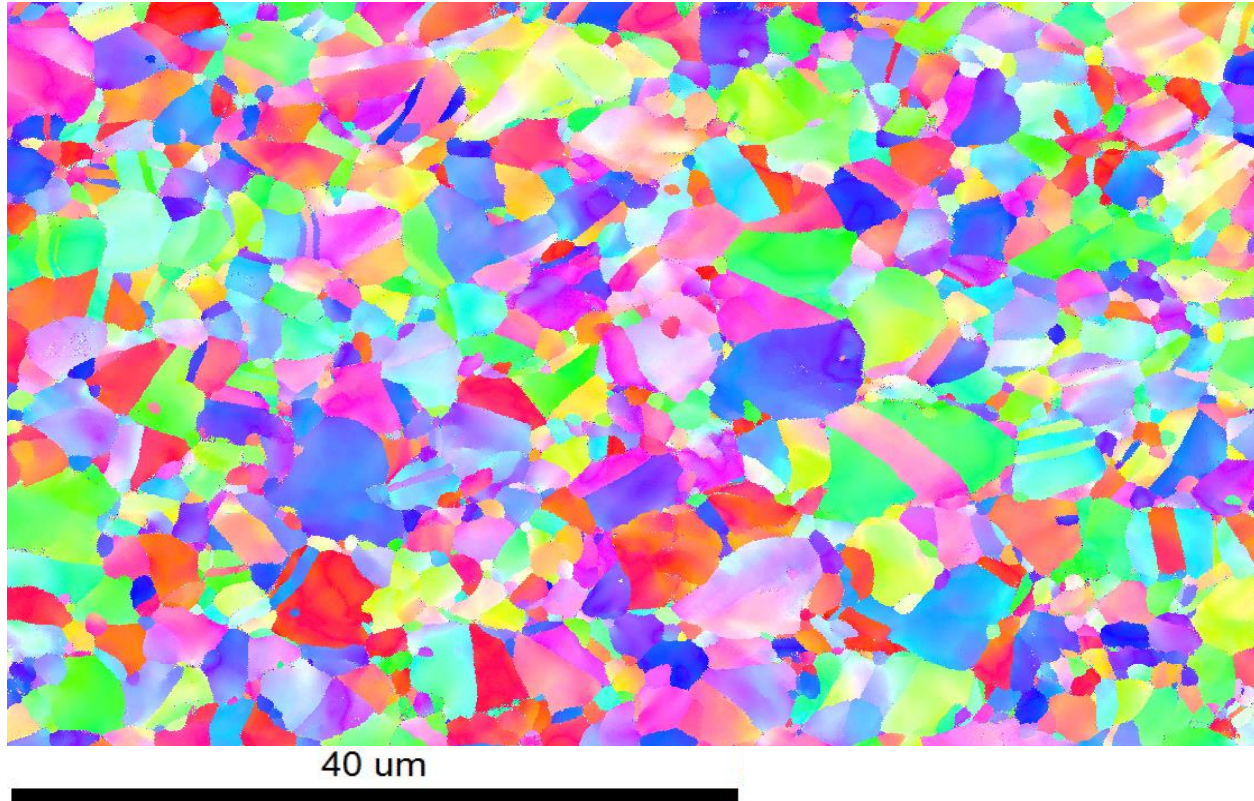
40 um



# Interrupted Heat Treatments EBSD – As Deformed

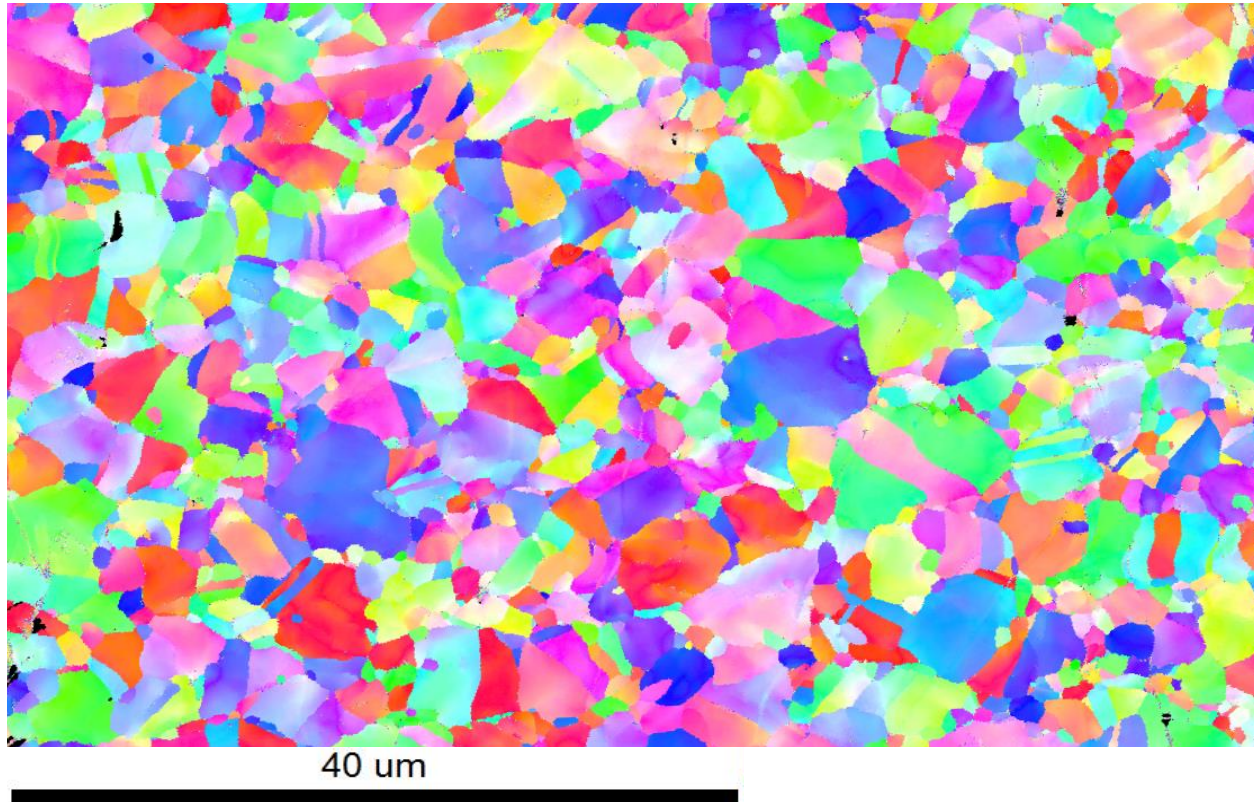


# Interrupted Heat Treatments EBSD – As Deformed

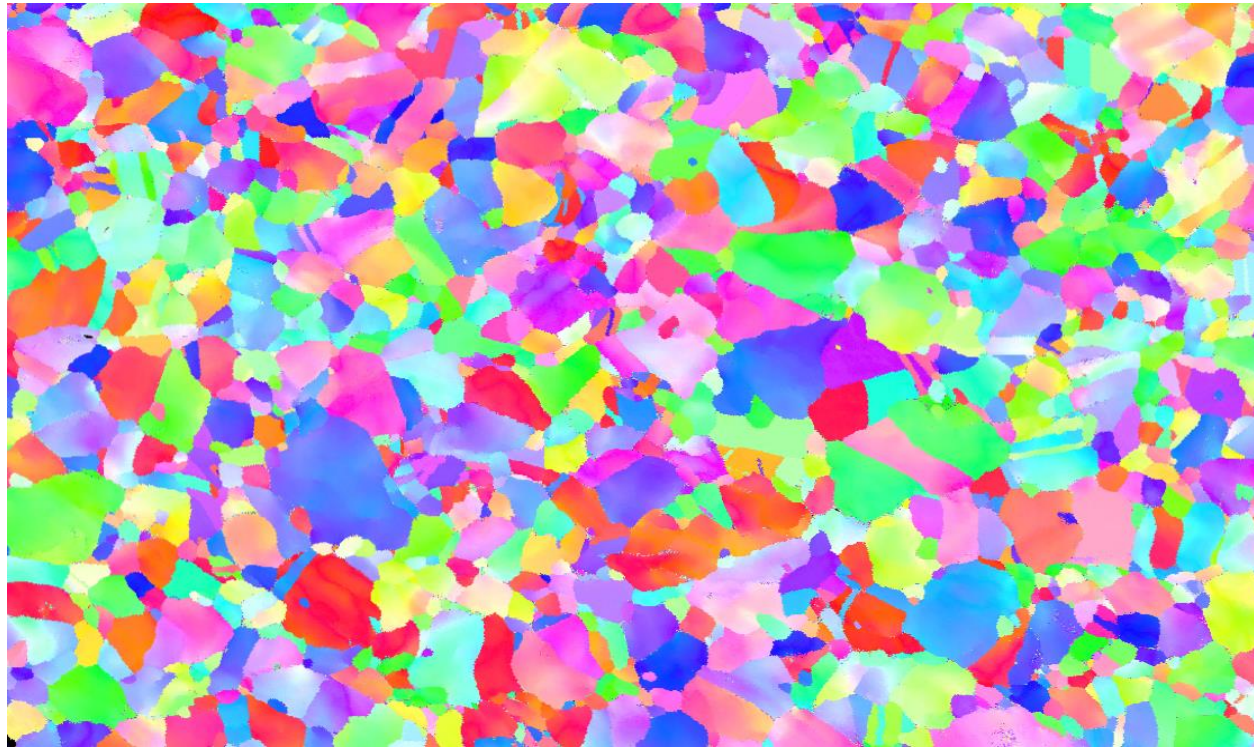


# Interrupted Heat Treatments

## EBSD – 1050°C

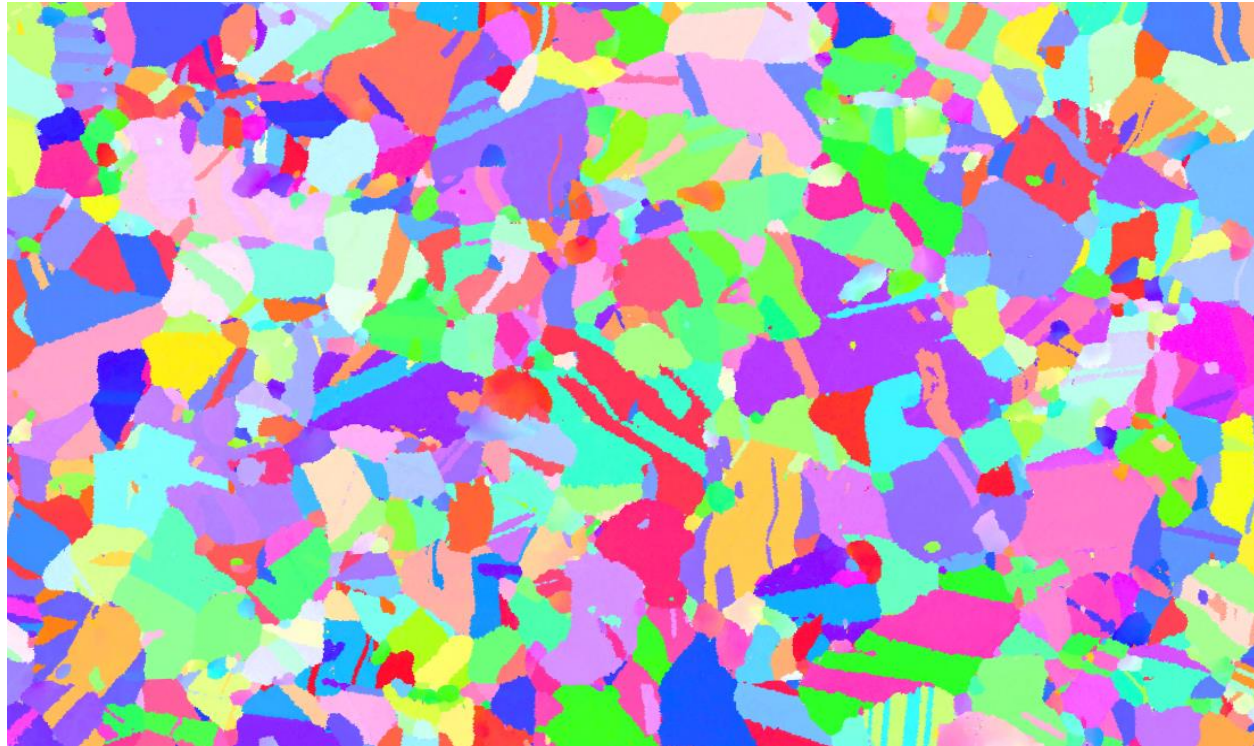


# Interrupted Heat Treatments EBSD – 1075°C



40 um

# Interrupted Heat Treatments EBSD – 1100°C



40 um

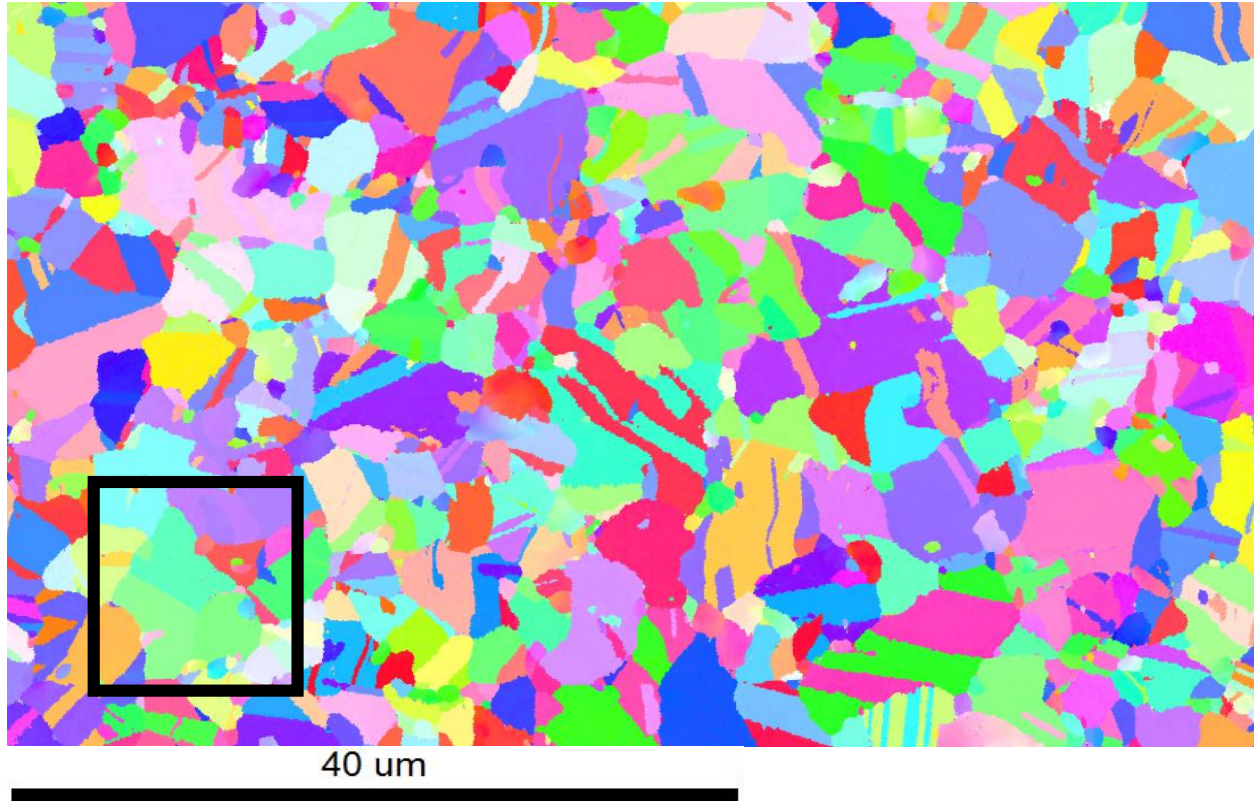
# Interrupted Heat Treatment Results



- Temperatures below 1050°C show no major microstructural changes
- Some recrystallization nucleation sites appear in plane, while most are out of plane
- Full recrystallization (determined by GROD) by 1100°C for 1110°C preheat treatment temperature
  - Preliminary 1130°C preheat treatment specimen shows delayed RX growth
- $\gamma$  boundaries able to pass by  $\gamma_1'$  to create intragranular, incoherent  $\gamma_1'$
- Lower RX temperature than preheat treatment may suggest  $\gamma$  templating method rather than  $\gamma_1'$  dissolution (?)

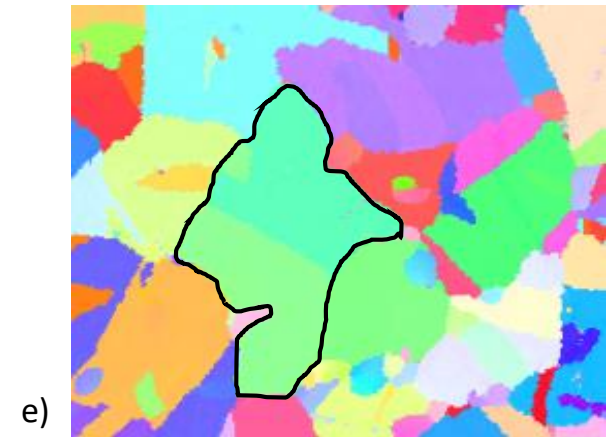
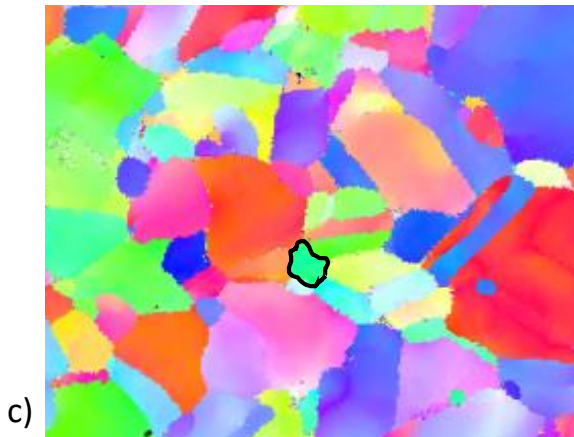
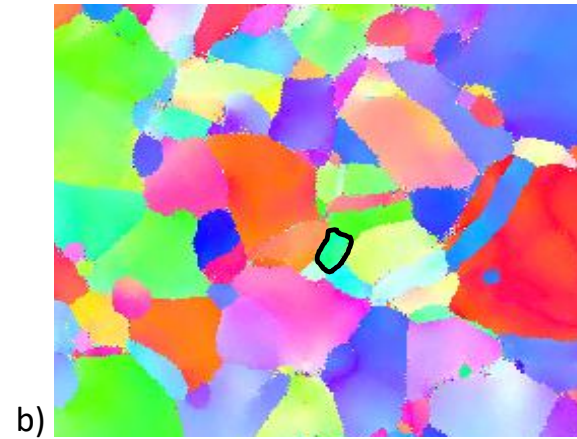
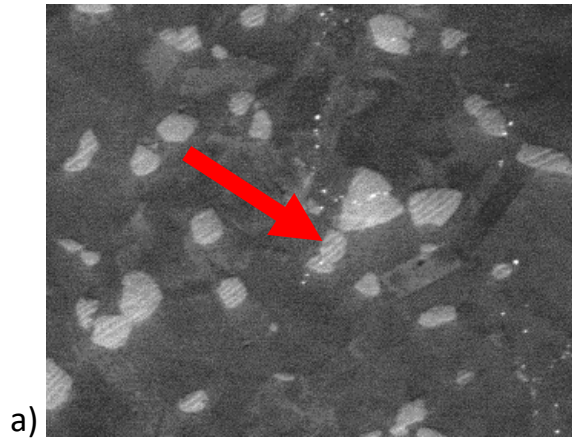
# Interrupted Heat Treatments

## EBSD – 1100°C

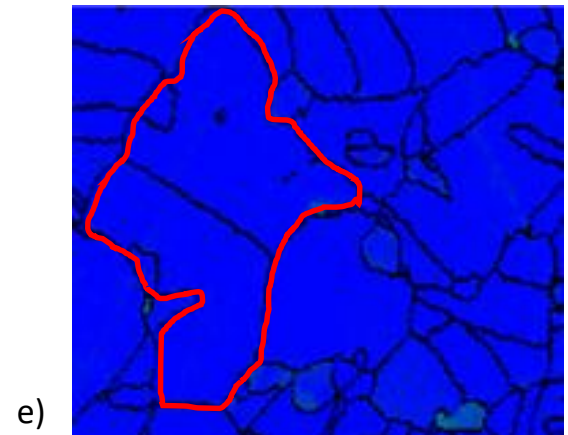
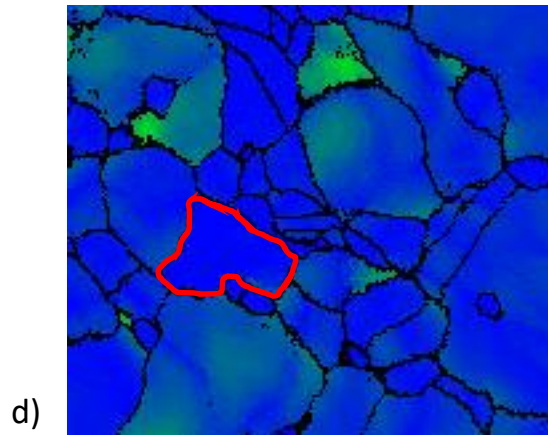
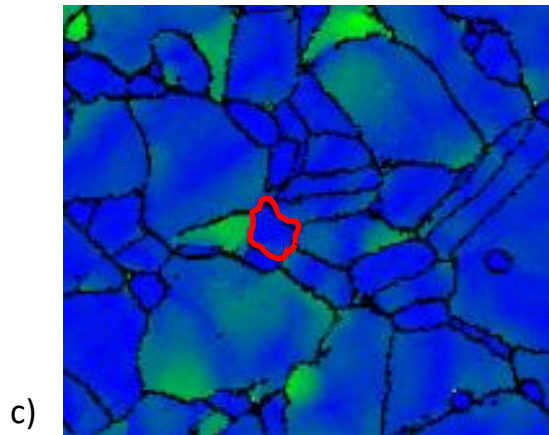
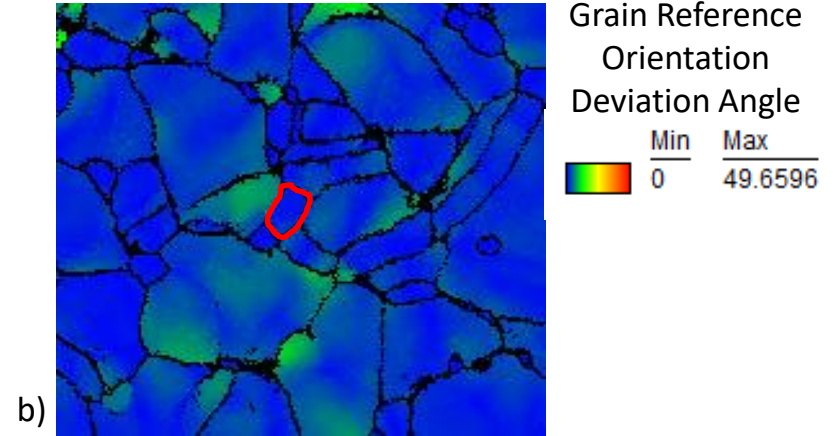




# Progression of $\gamma$ Growth From $\gamma'_1$



# Consumption of Stored Energy



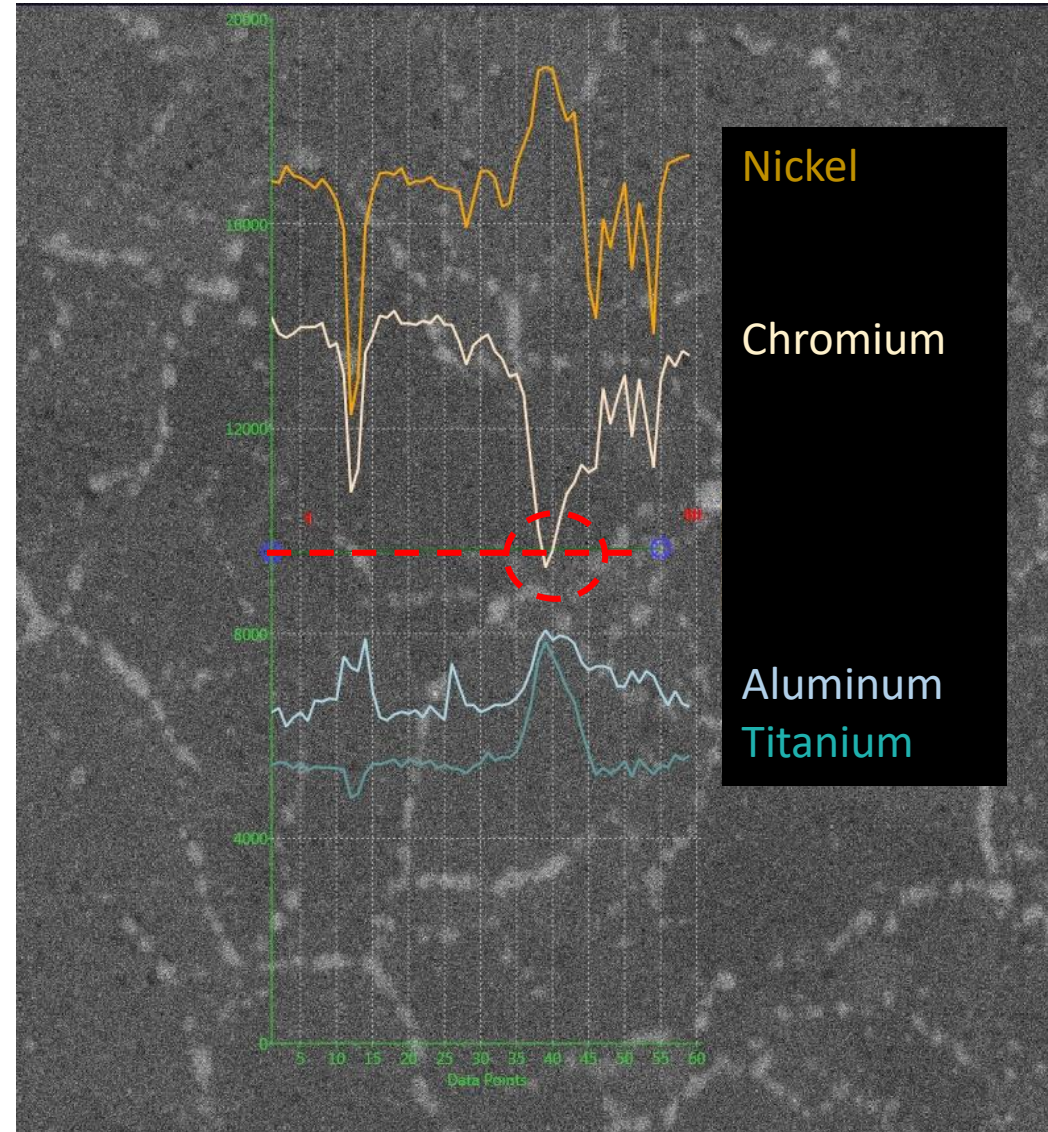
# $\gamma'_1$ - $\gamma$ Orientation

- SEM-EBSD analysis shows same orientation for  $\gamma'_1$  precipitate as recrystallized & strain free  $\gamma$  that grew to consume neighboring  $\gamma$  containing stored energy
- $\gamma'_1$  precipitate shown in red circle
- $\gamma$  twin boundary shown by dashed red line



# Elemental Analysis (EDS)

- SEM-EDS line scan analysis demonstrates  $\gamma'$  composition for particle
- Neighboring surface oxide present as well
  - Superfluous data



# Future Work



## Interrupted Heat Treatments

- Repeat experiment for higher pre-heat treatment temperature
  - Decreased

## Coherency Analysis

- Appears that  $\gamma_{RX}$  should be coherent with parent  $\gamma'_1$
- Orientation alone is insufficient to classify as coherent
- Planning TEM analysis of FIB liftout traversing  $\gamma$ - $\gamma'_1$  boundary
  - Misfit dislocations, coherency strain, lattice continuity

## Industrial Processing Remedies

- Increased strain rate during late processing possible to impart more strain in critical regions
  - Preliminary results show some promise

# Challenges & Opportunities

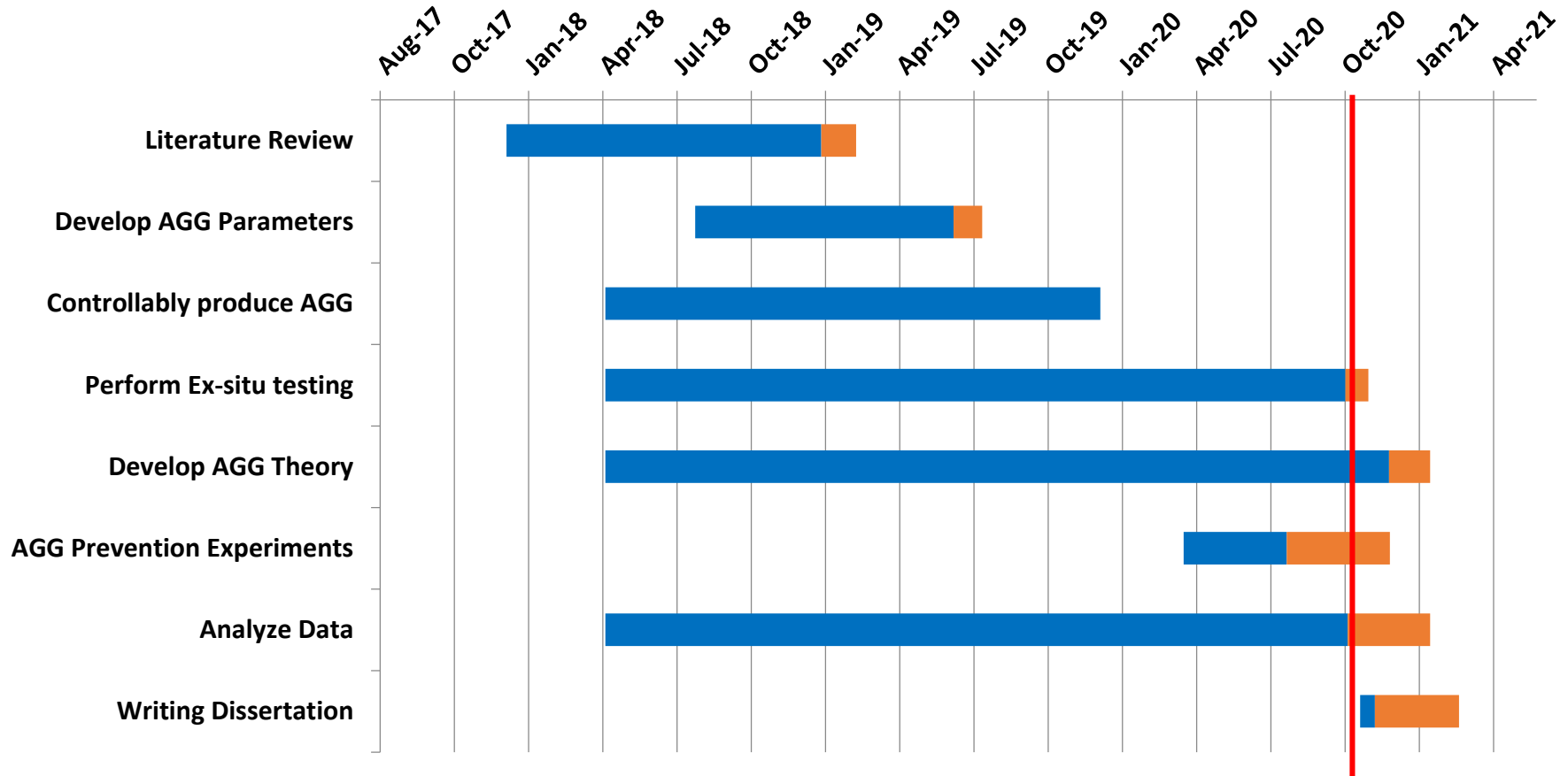


- Determining coherency at  $\gamma$ - $\gamma'_1$  interface
  - Loss of coherency as  $\gamma_{RX}$  grows doesn't necessarily change hypothesis
- Calculate theoretical size for coherency loss
  - Low lattice parameter misfit  $\sim 0.05\%$

## Possible future work:

- Interesting cyclic  $\gamma'_2$  coarsening/splitting behavior observed
  - Previous literature, proposed homogenization process
- Slow cooling appears to promote  $\gamma$ - $\gamma'_1$  shelling
  - Locally supersaturated in  $\gamma$  forming elements?
  - Inflection point in  $\gamma$ - $\gamma'_1$  solvus line?

# Progress



*Thank you!*

*Byron McArthur*  
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# 1110°C Pre-HT, 15% Compression Animated

