

Spatially Resolved Acoustic Spectroscopy (SRAS)

***Spring 2019 Semi-Annual Meeting
Iowa State University, Ames, IA
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Principal Developer: Thomas K. Ales (ISU)

Postdoc: Maria J. Quintana (ISU)

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Other Participants: Lucas Koester (ISU), Dan Barnard (ISU)

SRAS Inventors and Experts (U. Nottingham): Matt Clark, Richard Smith and Wenqi Li

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project N00014-17-1-2294
“Analytical serial sectioning
with orientation
microscopy capabilities”*

Spatially Resolved Acoustic Spectroscopy (SRAS)



- Principal Developer: Thomas Ales (ISU)
- Postdoc: Maria Quintana (ISU)
- Advisor(s): Prof. Peter Collins (ISU)

- **Problem:** Need for a new instrument that can rapidly analyze crystal orientations at the ‘mesoscale’ (beyond the nanometer and micrometer length scales).
- **Objective:** Establish and demonstrate a new 3D characterization tool to integrate microstructure, texture and defects, involving the use of surface acoustic waves.
- **Benefit:** Instrument that measures crystal orientations at the ‘mesoscale’ and eventually in 3D datasets.

Project Duration
August 2017 to June 2020

Recent Progress

- The optic train is assembled and its alignment is in progress
- Forward model code is almost finished
- Transfer system from Robomet to SRAS is designed

Metrics

Description	% Complete	Status
1. Design strategy	100%	●
2. Review of Materials State Awareness	100%	●
3. Mathematics that underpin the forward and inverse models and Coding	95%	●
4. Assembly, alignment and coupling to Robo.met	50%	●
5. 2D and 3D datasets	0%	●

Spatially Resolved Acoustic Spectroscopy (SRAS)



- Need for a new instrument that can rapidly analyze crystal orientations at the ‘mesoscale’
 - Beyond the nanometer and micrometer length scales
- Spatially Resolved Acoustic Spectroscopy (SRAS) has been developed at the University of Nottingham
 - One possibility would involve the use of surface acoustic waves.



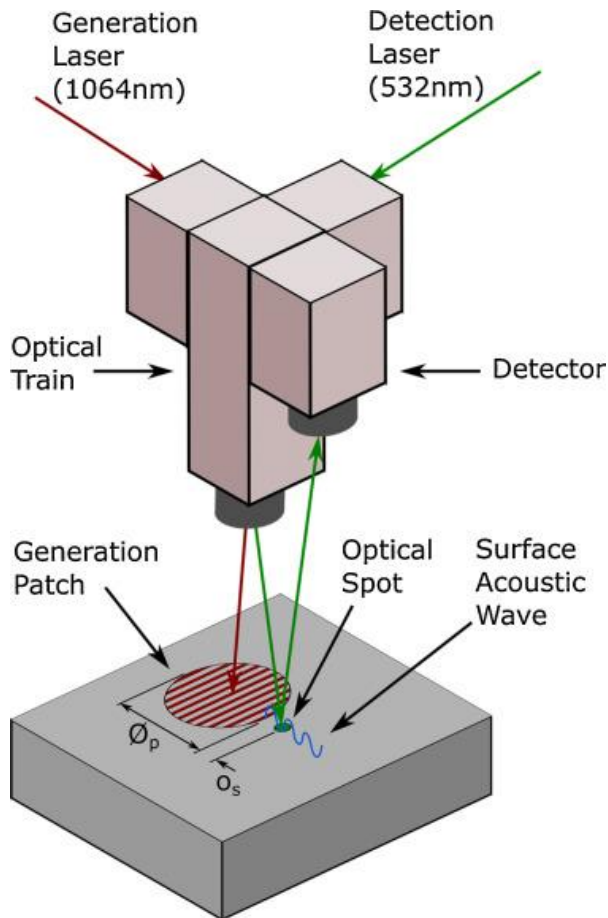
Spatially resolved acoustic spectroscopy (SRAS):
texture and microstructure characterisation

Wenqi Li, Rikesh Patel, Richard Smith, Matthias Hirsch,
Matt Clark, Adam Clare and Steve Sharples

**Optics & Photonics Group, Faculty of
Engineering, University of Nottingham, UK.**

QNDE Workshop 2017, Provo, Utah, US

Spatially Resolved Acoustic Spectroscopy (SRAS)



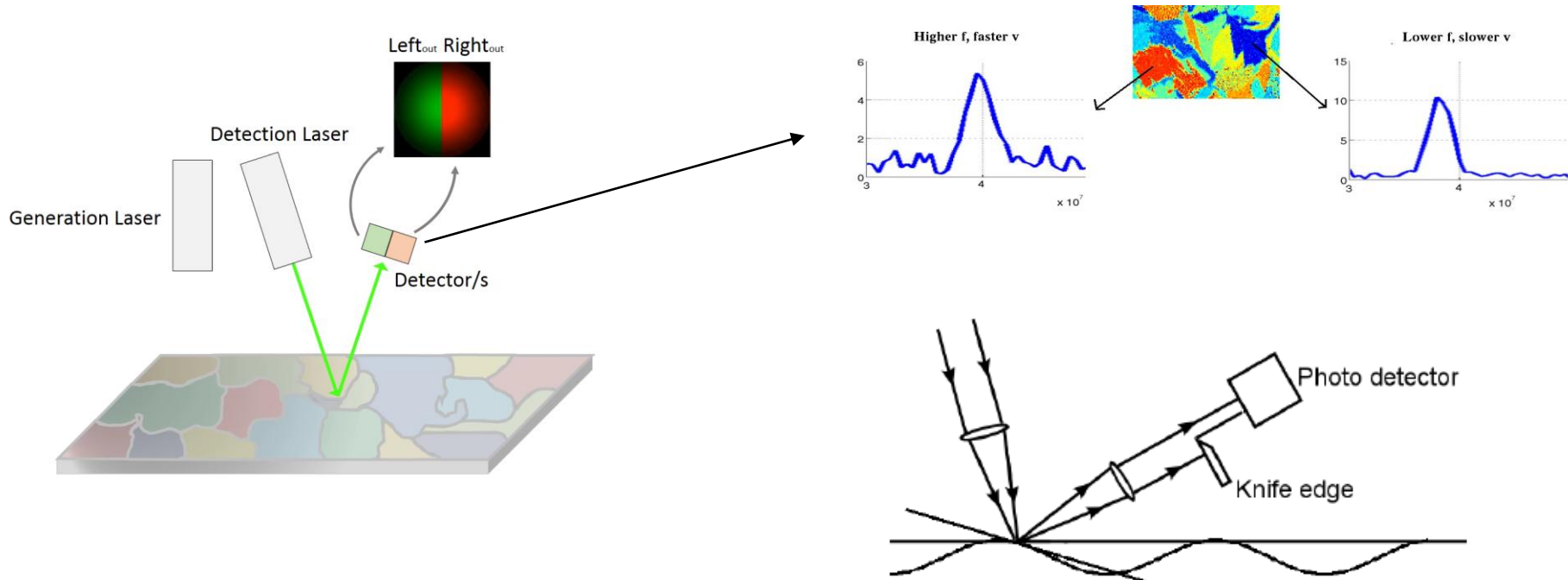
- Laser based microscopy to obtain texture information for a large sample
- A pulsed laser is imaged to the sample surface, where the absorbed pulses generate acoustic waves that have a characteristic frequency f
 - This frequency is measured by monitoring the interaction of the acoustic waves with a probe laser and is then processed to recover the surface wave acoustic velocity (SAW)
 - The SAW velocity varies with grain orientation giving information about the grain size and orientation distribution
- The sample is raster scanned to build up an image
- If multiple velocity images are taken with different acoustic wave propagation directions then it is possible to recover the actual orientation of the grains

Richard J.S. et al, J of Material Processing Tech., Vol 236, 2016, pg 93

SRAS theory

- The size of the grating patch defines your resolution
- The direction of the lines defines the direction of wave propagation
- $v = f\lambda$

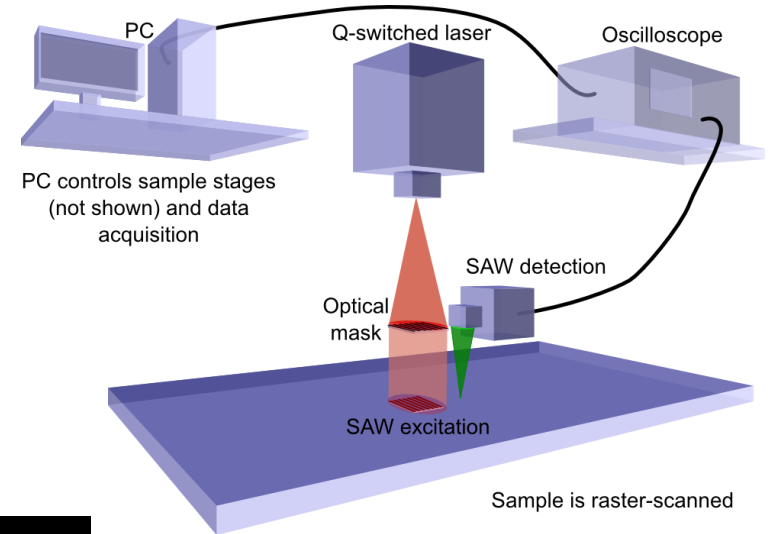
Frequency \rightarrow Velocity



(Patent No.: GB2441953, 2009)

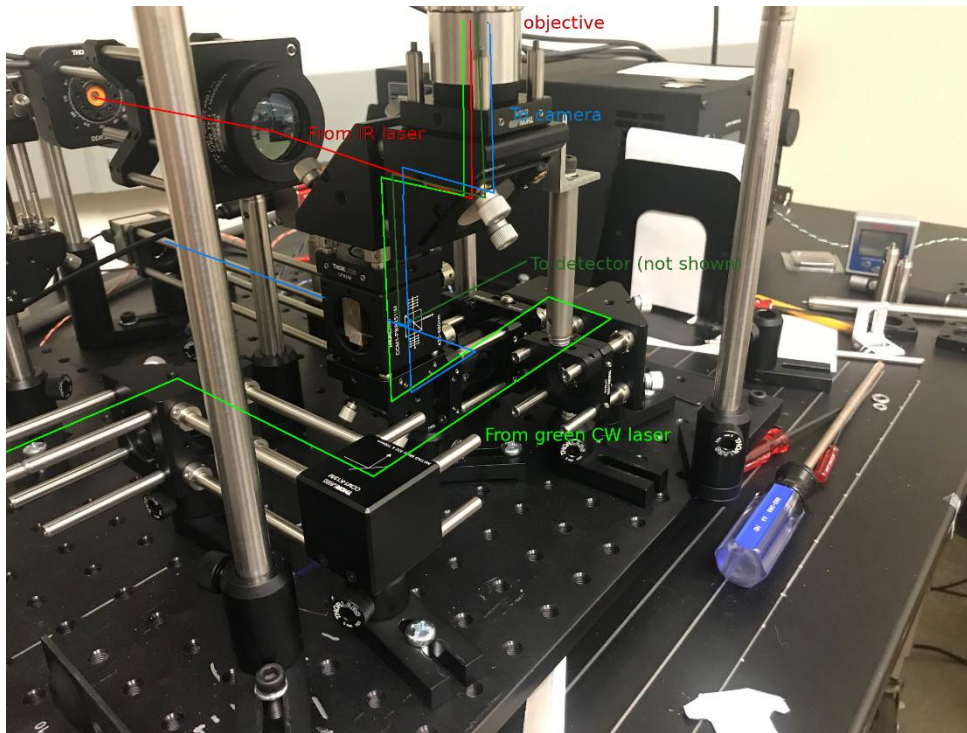
SRAS instrument

- At each point generate SAWs using laser and a grating – fixed acoustic wavelength
- Detect the SAWs with another laser
- Find the peak of the frequency spectrum of the detected waves

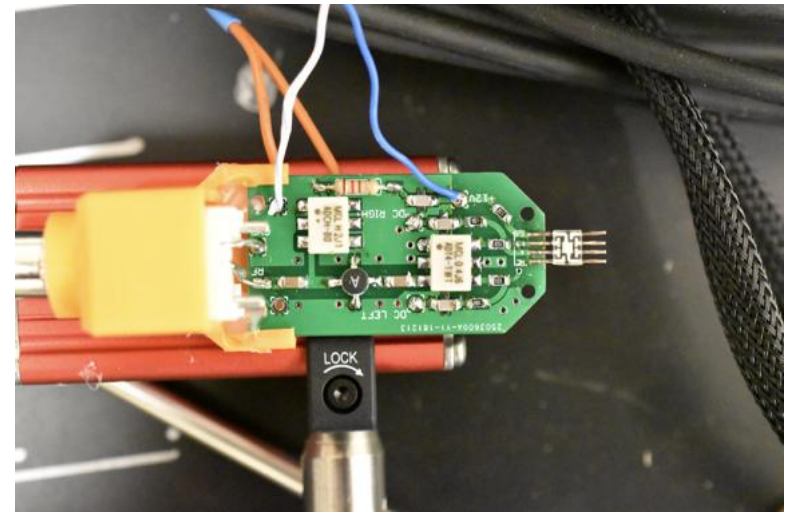


- Calculate the velocity using $v = f\lambda$

SRAS instrument



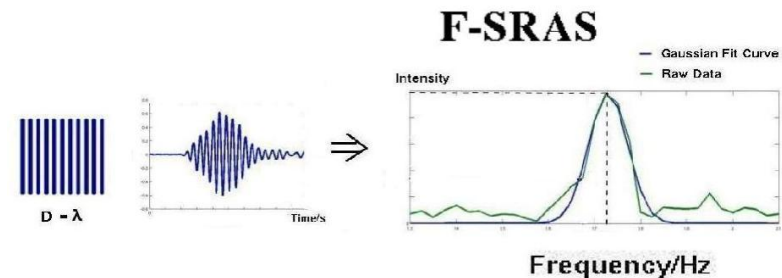
Current state of optical train



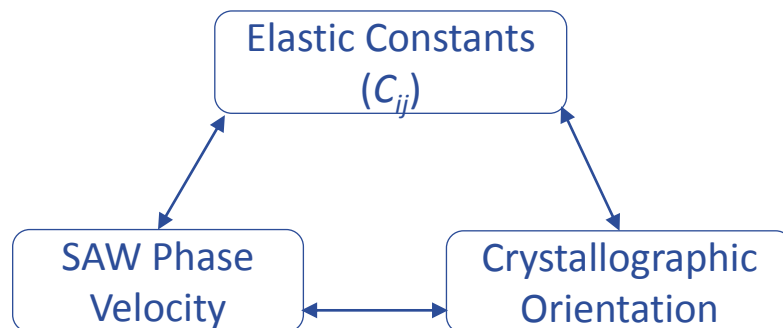
Custom made printed circuit boards

Orientation Determination

- $v = f\lambda$
 - λ is the fringe spacing of the mask
 - Mask is glass coated with Cr
 - Grating acts as a filter.
 - f is the peak frequency from the experiment
 - Velocity measured
 - FFT, interpret frequency domain to determine peak



Elastic constants, SAW Phase Velocity, and Crystallographic Orientation are interrelated.



- **EASY:**
 - Calculating the elastic constants
 - Predicting SAW Phase Velocity
- **HARD:**
 - Calculating crystallographic orientation
- **SOLUTION:**
 - Predict SAW velocity, index against solutions

Predict SAW velocities

- Wave equation:

$$\rho \frac{\partial^2 u_j}{\partial t^2} = \frac{\partial T_{ij}}{\partial x_i}, \quad (i, j = 1, 2, 3)$$

- Boundary condition:

$$T_{3j} = c_{3jkl} \partial u_k / \partial x_l = 0, \quad \text{for } j = 1, 2, 3.$$

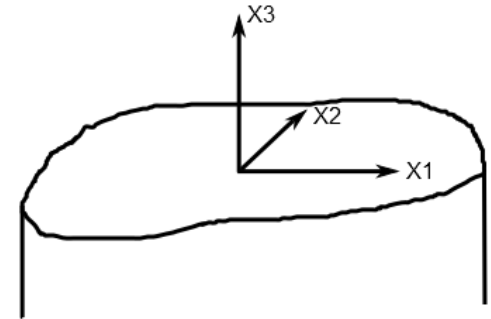
- Solution of the wave equation:

$$u_i = \sum_{n=1}^3 C_n \alpha_i^{(n)} \exp[-j\beta l_3^{(n)} x_3] \exp[j(\omega t - \beta l_1 x_1 - \beta l_2 x_2)]$$

- Determinant of the boundary condition:

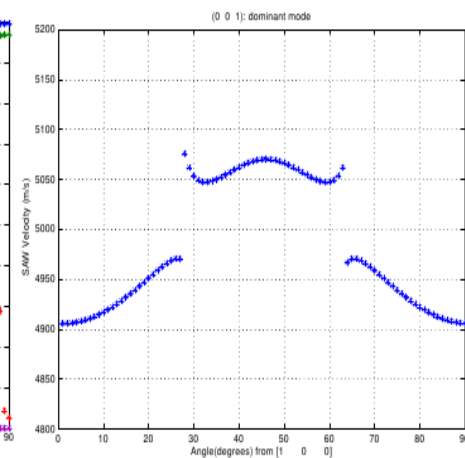
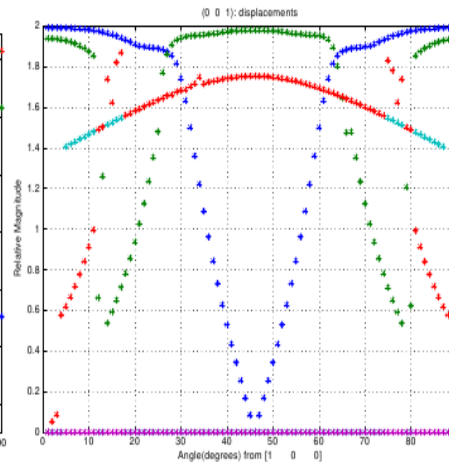
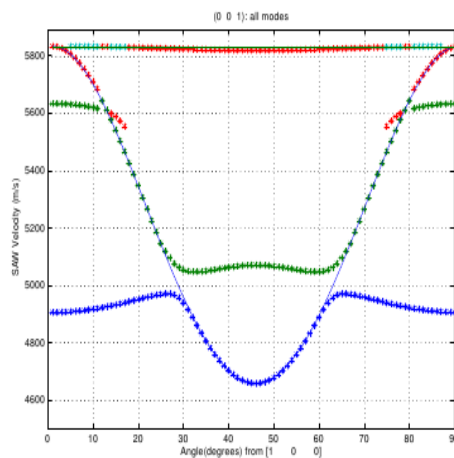
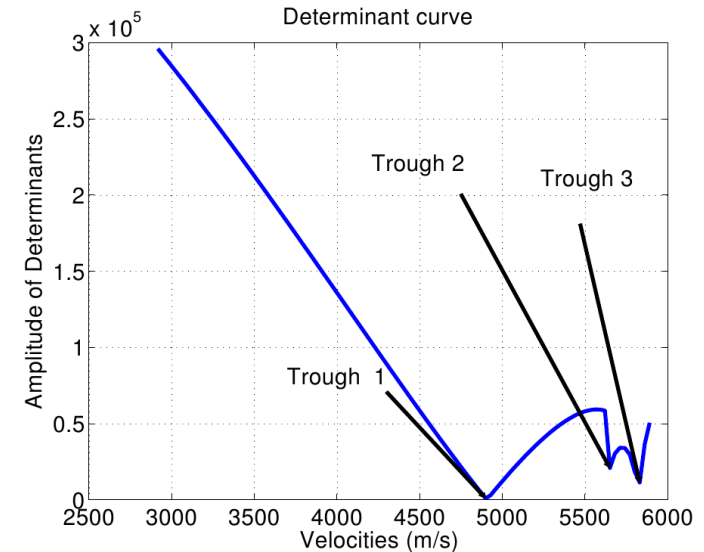
$$d_{mn} = c_{m3kl} \alpha_k^{(n)} l_l^{(n)} = 0, \quad \text{with } l_1^{(n)} \equiv l_1, \quad l_2^{(n)} \equiv l_2.$$

- Li, W., Thesis, Laser ultrasonic method for determination of crystallographic orientation of large grain metals by spatially resolved acoustic spectroscopy (SRAS), University of Nottingham, 2012
- Farnell, G.W., Properties of Elastic Surface Waves, *Physical Acoustics*, 6 (1970): 109-166
- Viktorov, I.A., Rayleigh and Lamb Waves: Physical Theory and Applications, Trans. From Russian. Plenum Press, 1967



Predict SAW Velocities

- The determinant of the boundary condition is calculated at a specific velocity
- The curve of the determinant is plotted as a function of the velocity
- Troughs of the curve correspond to the wave modes
- The 'dominant' mode is selected according to the out-of-plane displacement



Forward Model

- Root Finding

- Involves solving for v for the selected microstructural anisotropy
- Calculation of the amplitudes and down selection of the dominant modes of propagation as a function of direction

$$\begin{vmatrix} \Gamma_{11} - \rho v^2 & \Gamma_{12} & \Gamma_{13} \\ \Gamma_{21} & \Gamma_{22} - \rho v^2 & \Gamma_{23} \\ \Gamma_{31} & \Gamma_{32} & \Gamma_{33} - \rho v^2 \end{vmatrix} = 0$$

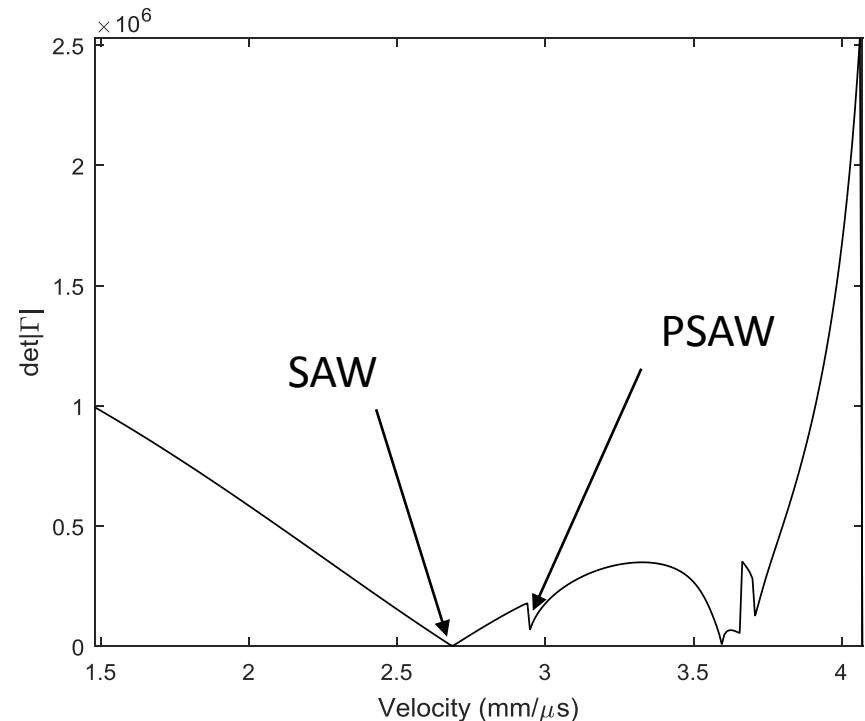
$$\Gamma_{11} = c_{11} + c_{44}l_3^2,$$

$$\Gamma_{22} = c_{44}(1 + l_3^2),$$

$$\Gamma_{33} = c_{44} + c_{11}l_3^2,$$

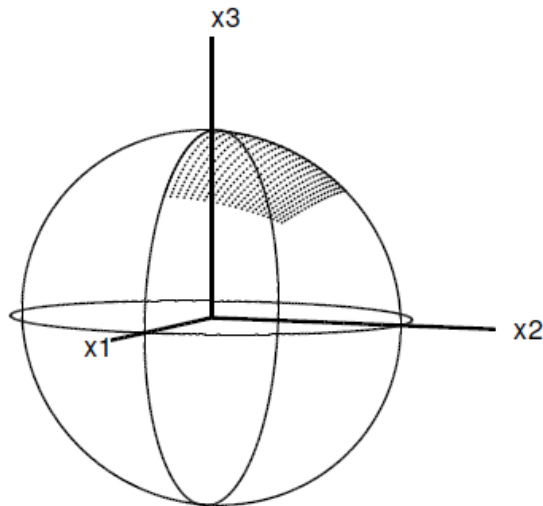
$$\Gamma_{13} = \Gamma_{31} = (c_{11} - c_{44})l_3,$$

$$\Gamma_{12} = \Gamma_{21} = \Gamma_{23} = \Gamma_{32} = 0.$$

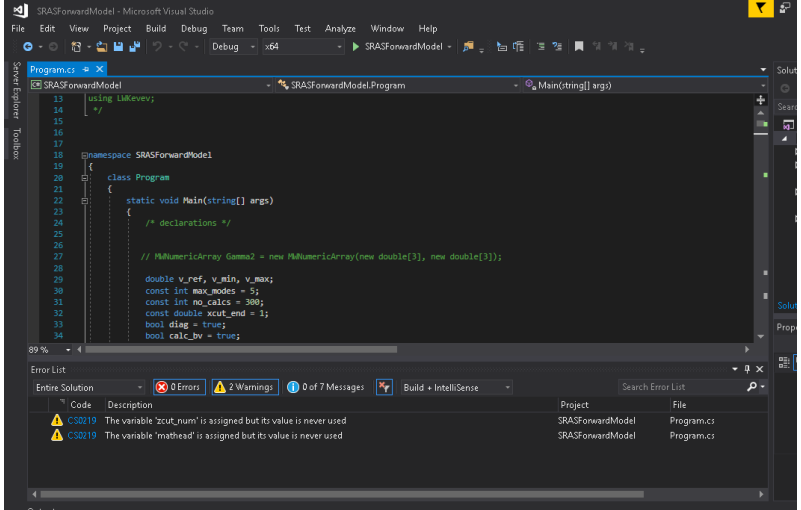


Forward model

- Utilizes crystal symmetry to reduce calculations necessary
- Data is stored and can be calculated in advance for a particular material system



Poles on the unit sphere at which wavespeeds and amplitudes are calculated. All other points are repetitions of these values (cubic symmetry)



```
using Likevevy;
//
namespace SRASForwardModel
{
    class Program
    {
        static void Main(string[] args)
        {
            /* declarations */

            // NNumericArray Gamma2 = new NNumericArray(new double[3], new double[3]);

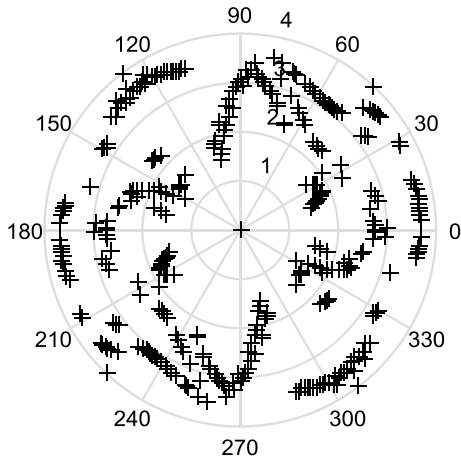
            double v_ref, v_min, v_max;
            const int max_modes = 5;
            const int no_calcs = 300;
            const double xcut_end = 1;
            bool diag = true;
            bool calc_bv = true;
        }
    }
}
```

Code	Description	Project	File
CS0219	The variable 'zcut_num' is assigned but its value is never used	SRASForwardModel	Programcs
CS0219	The variable 'msthead' is assigned but its value is never used	SRASForwardModel	Programcs

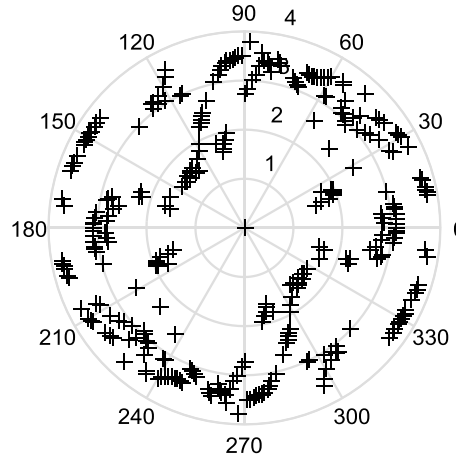
Written in C# for speed and portability

Example of forward model in Nickel

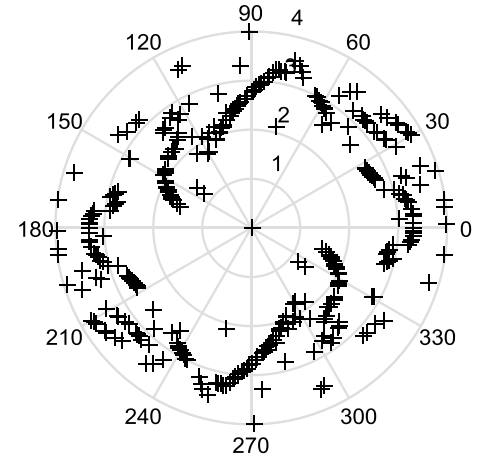
0, 0, 1



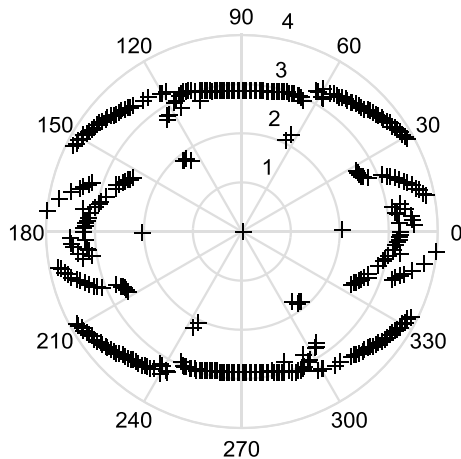
0, 0.25, 1



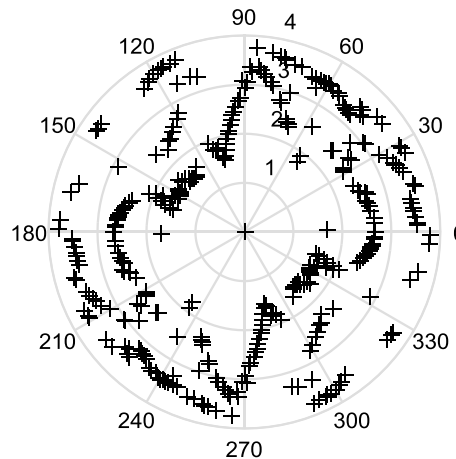
0, 0.5, 1



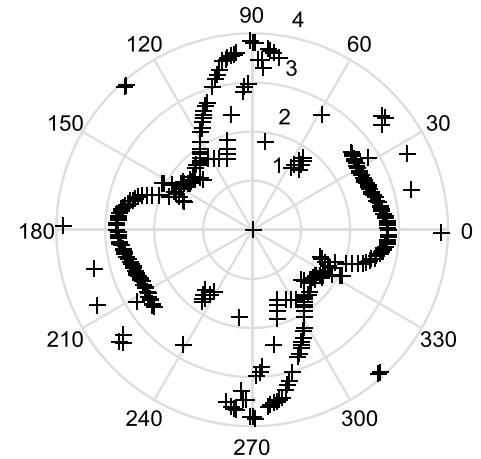
0, 1, 1



0.25, 0, 1

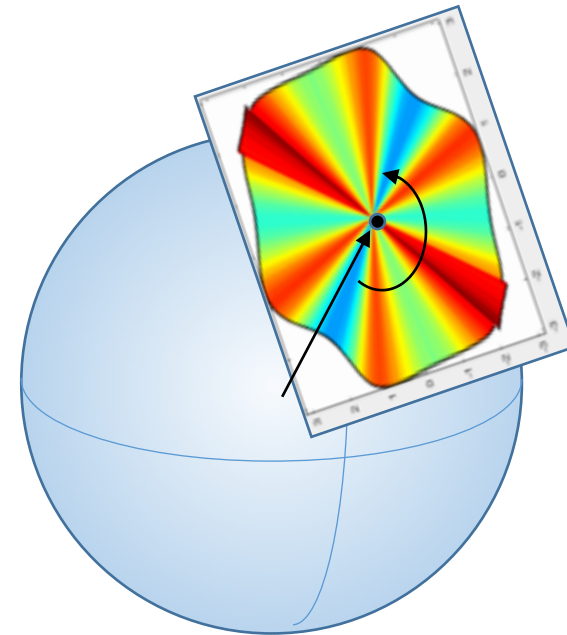


0.25, 0.25, 1

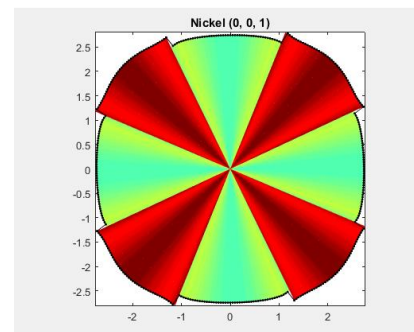


SRAS Forward Model Result

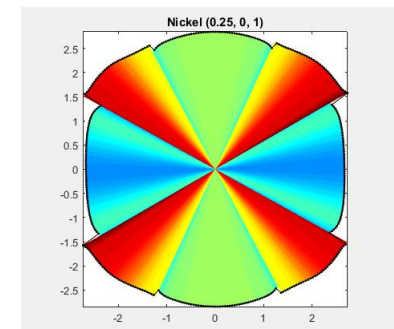
- Example at a single crystal plane shown at right
- All directions (0:180 + symmetry)
- Speeds of dominant modes saved for fitting
- Calculated at 1° intervals for 120 planes



(0,0,1)

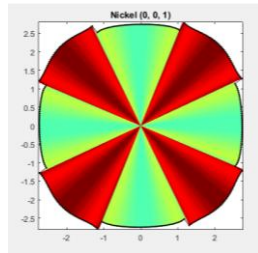


(0.25,0,1)

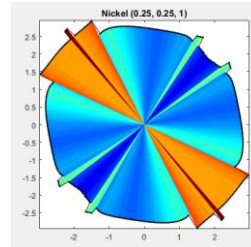
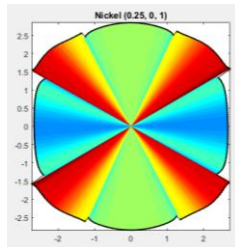


Example of forward model in Nickel

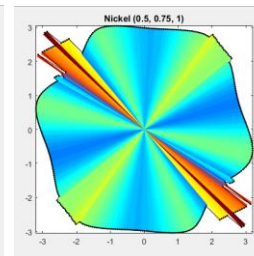
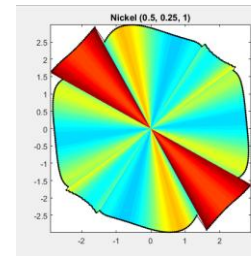
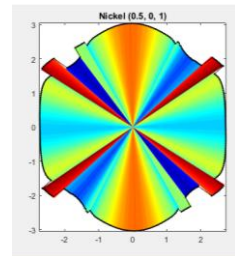
(0,0,1)



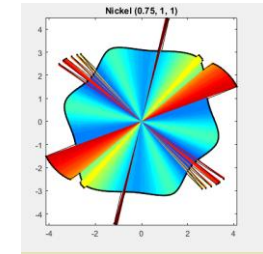
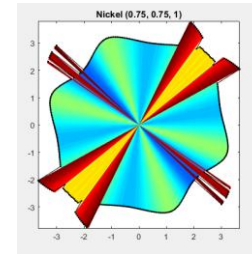
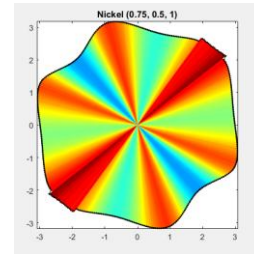
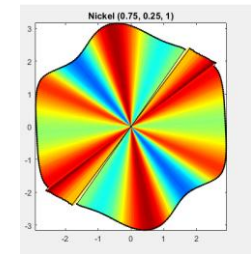
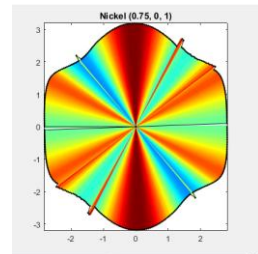
(0.25,X,1))



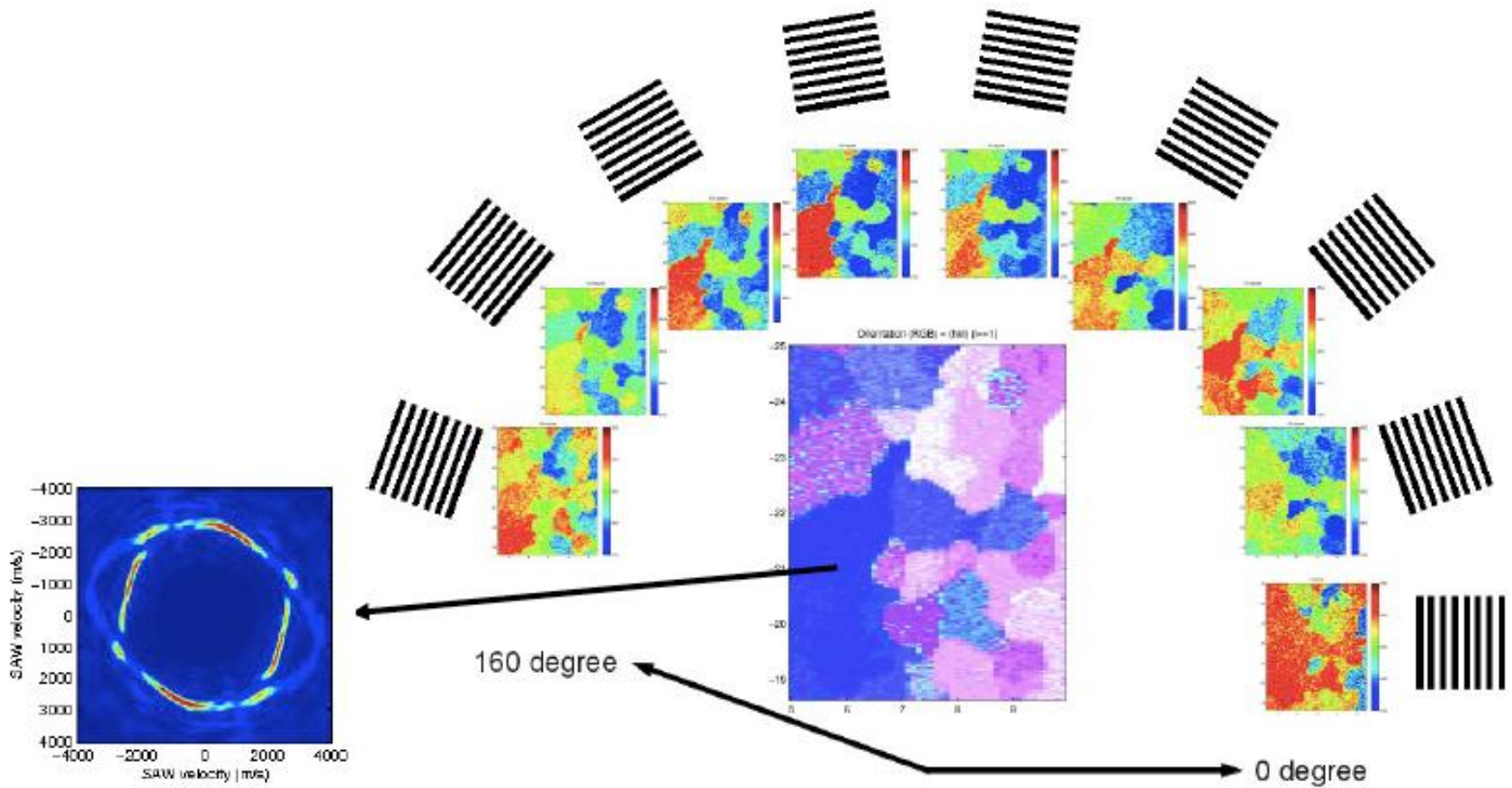
(0.5,X,1))



(0.75,X,1))

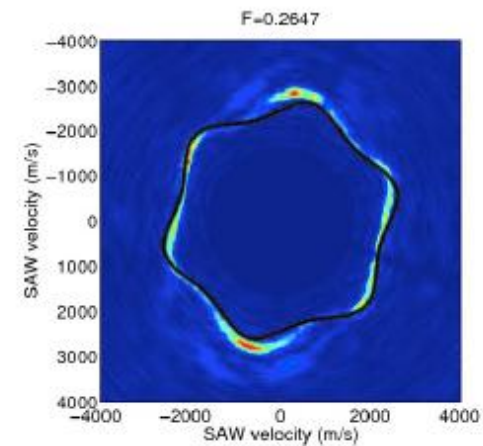
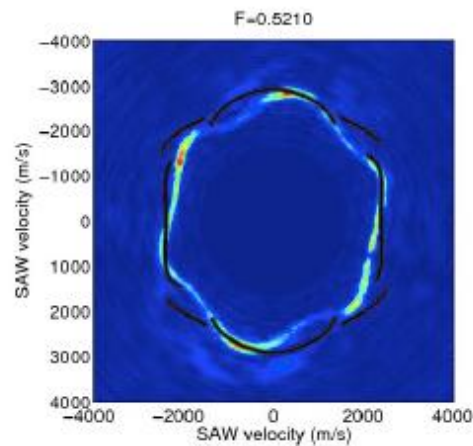
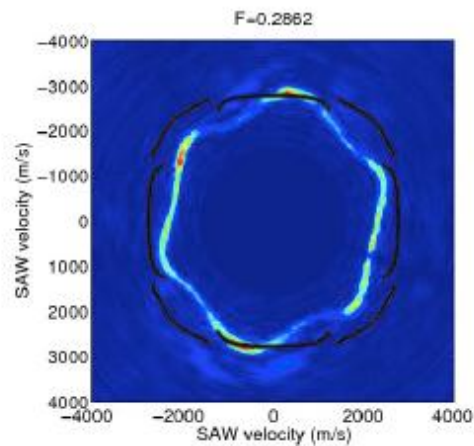


Collect data



Orientation imaging and fit to data

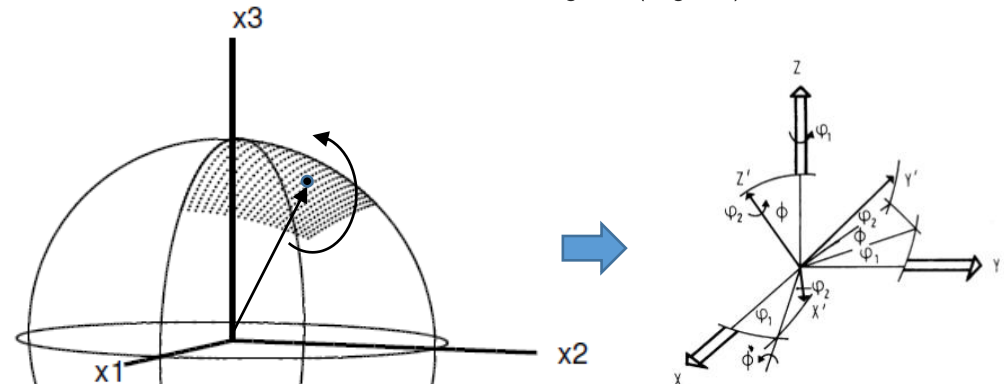
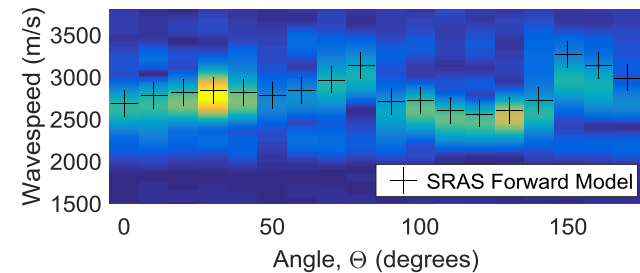
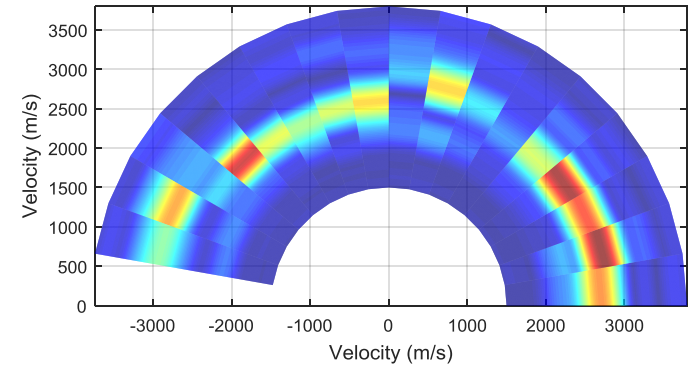
$$F(h, k, l, \theta) = \sum_{\phi=0}^{\phi=\frac{n-1}{n}\pi} A(\phi, v_{(h,k,l,(\phi-\theta))}), \quad (n = 1, 2, 3, \dots)$$



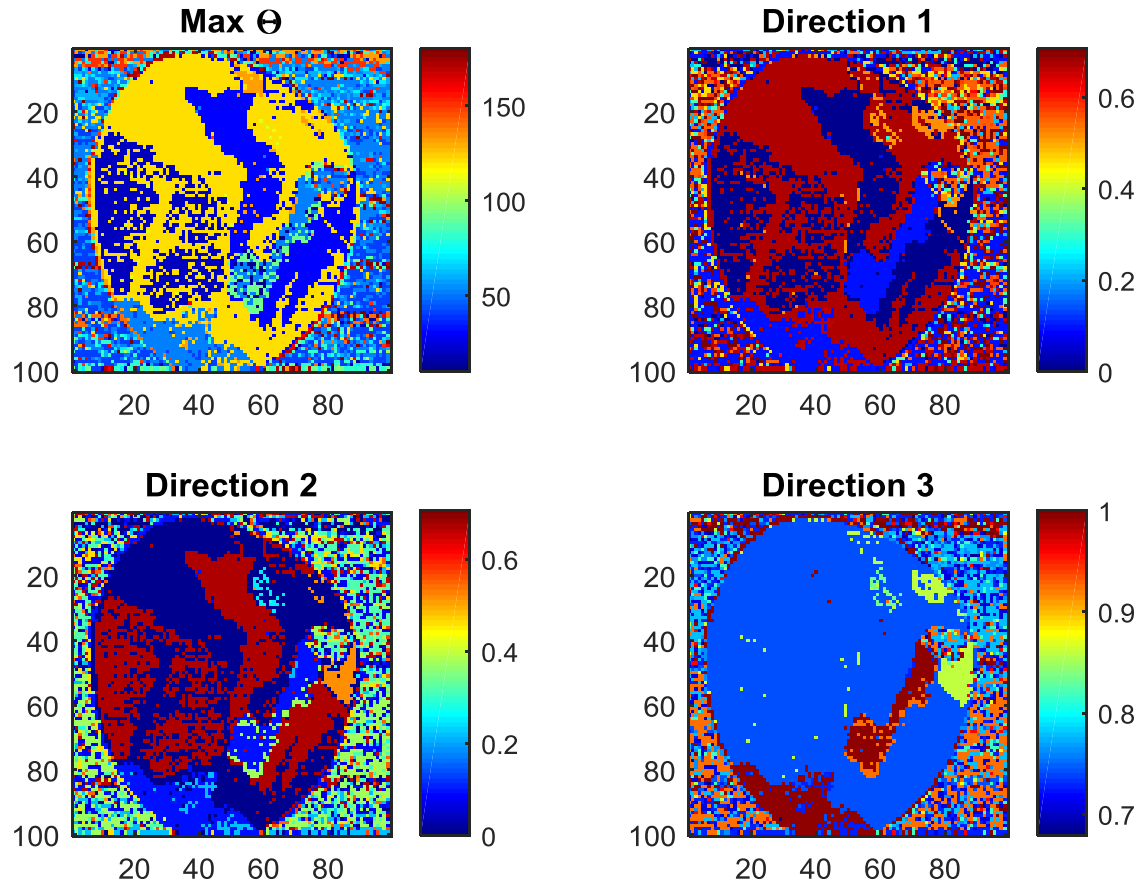
- The merit function is simply the sum of the amplitude under the black '+' on the graphs
- This procedure is repeated for all combinations of plane and propagation direction

Forward Model Inversion

- Raw data consists of wavespeeds and amplitudes vs direction
- Model data is interpolated onto experimental data and a best fit is found
- Fit includes crystal plane + rotation and can be converted to Euler angles, IPF map, etc. as seen in EBSD data

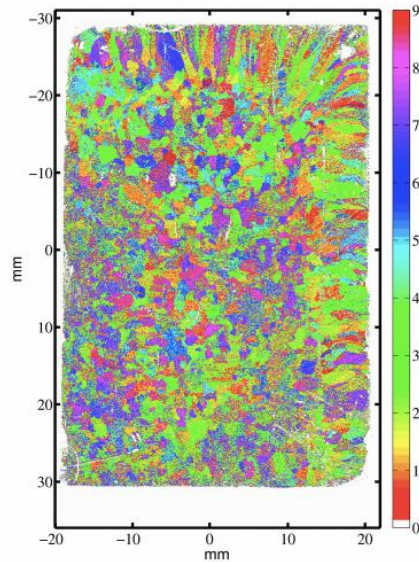
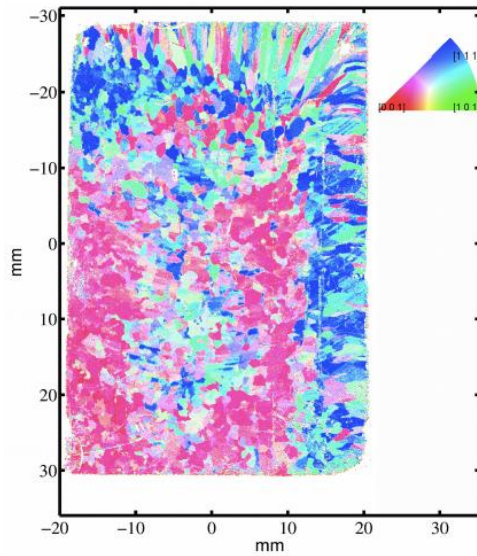


Example of Forward Model Inversion on Nickel

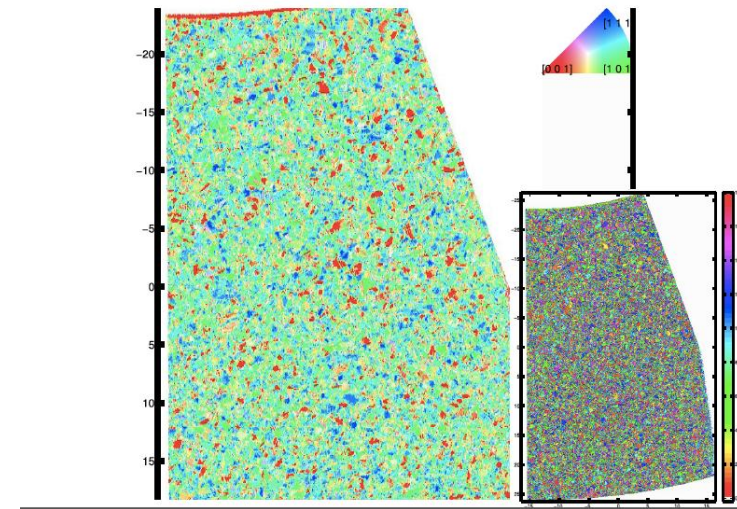


Examples – U. Nottingham

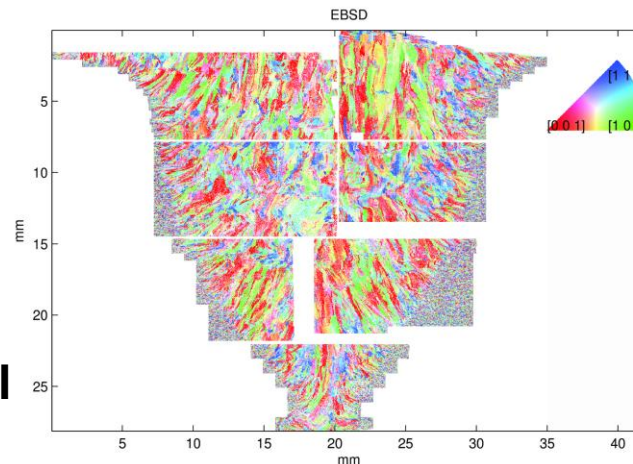
Large grain aluminium



Inconel

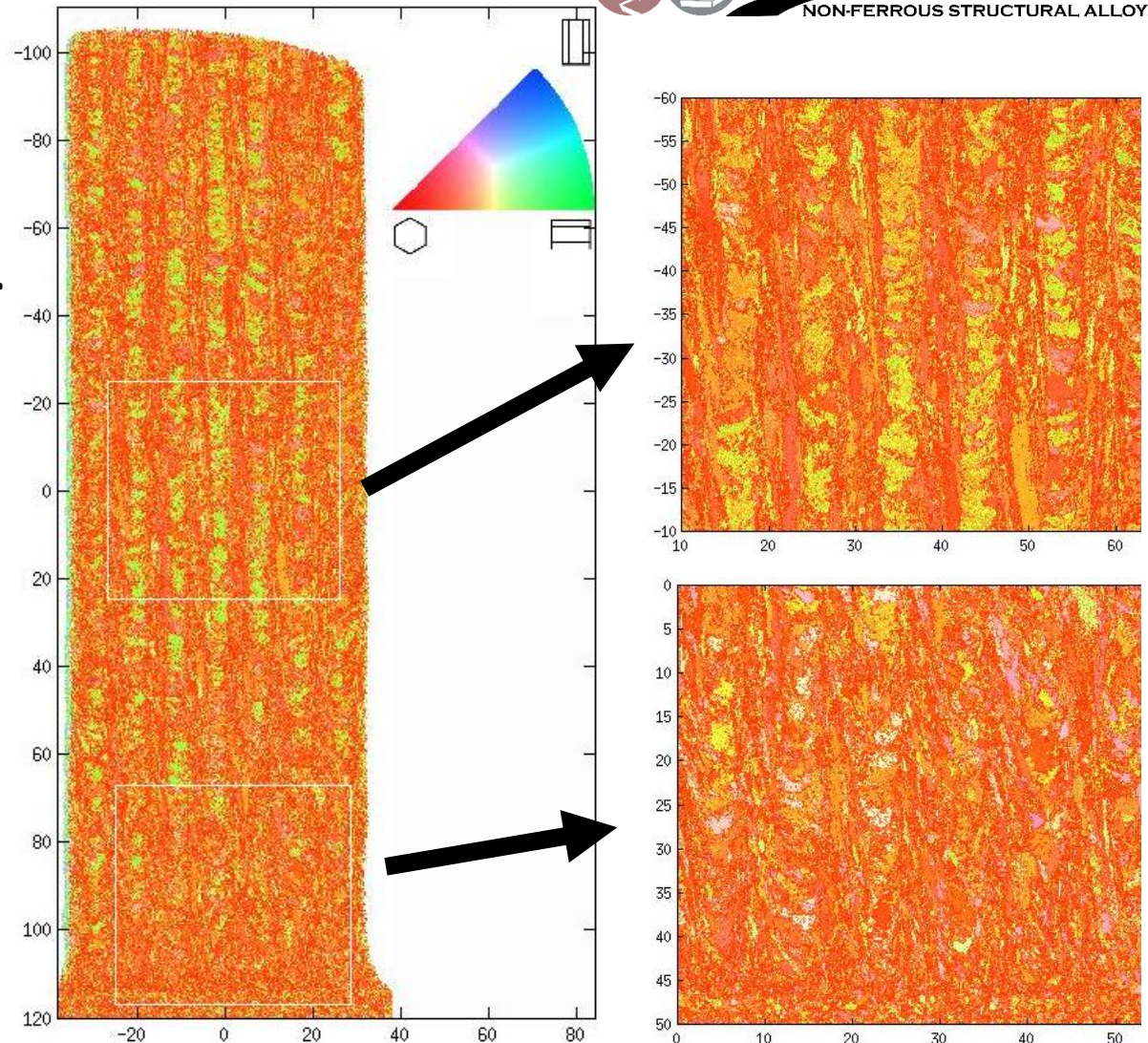


Stainless Steel

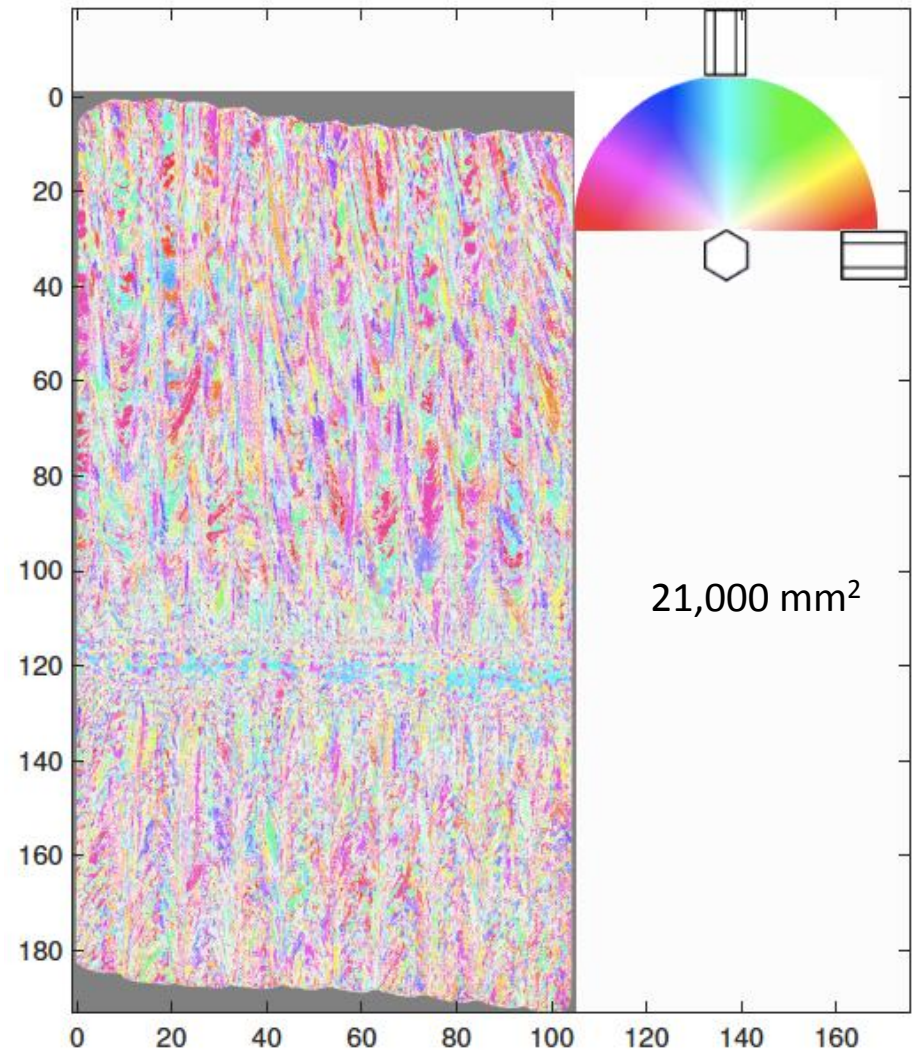
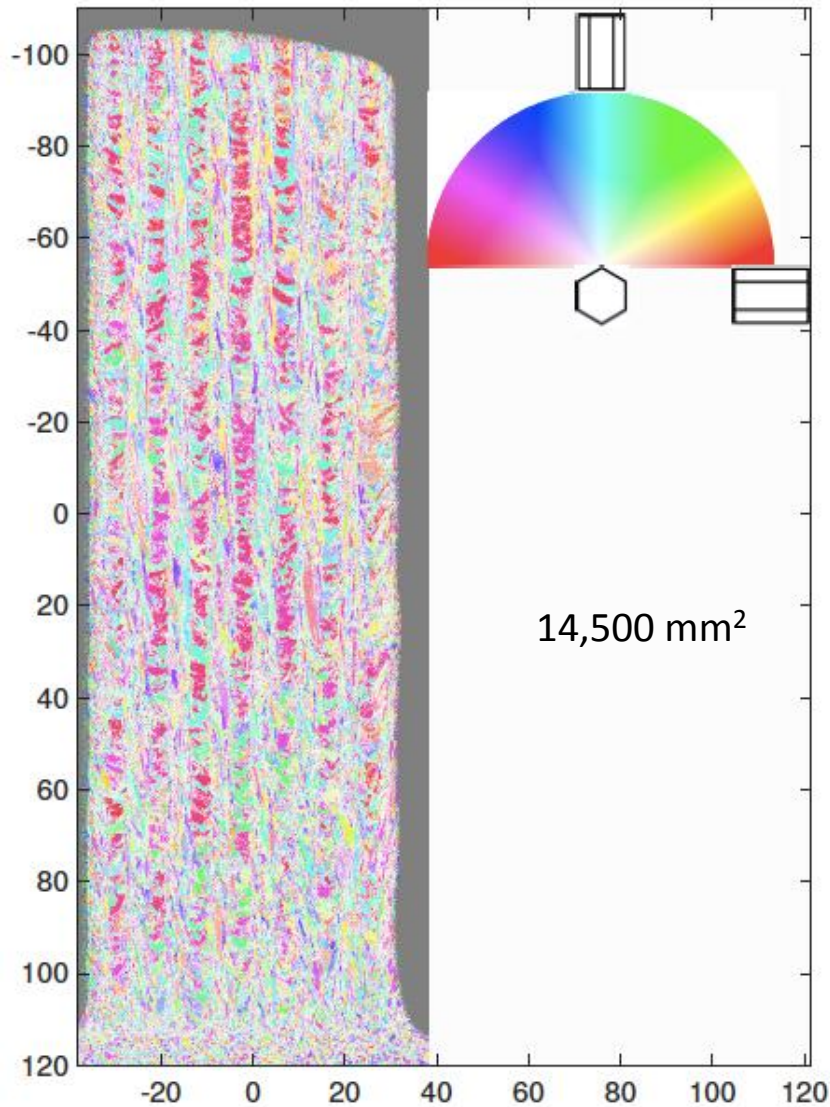


Hexagonal materials: SRAS on Ti 64

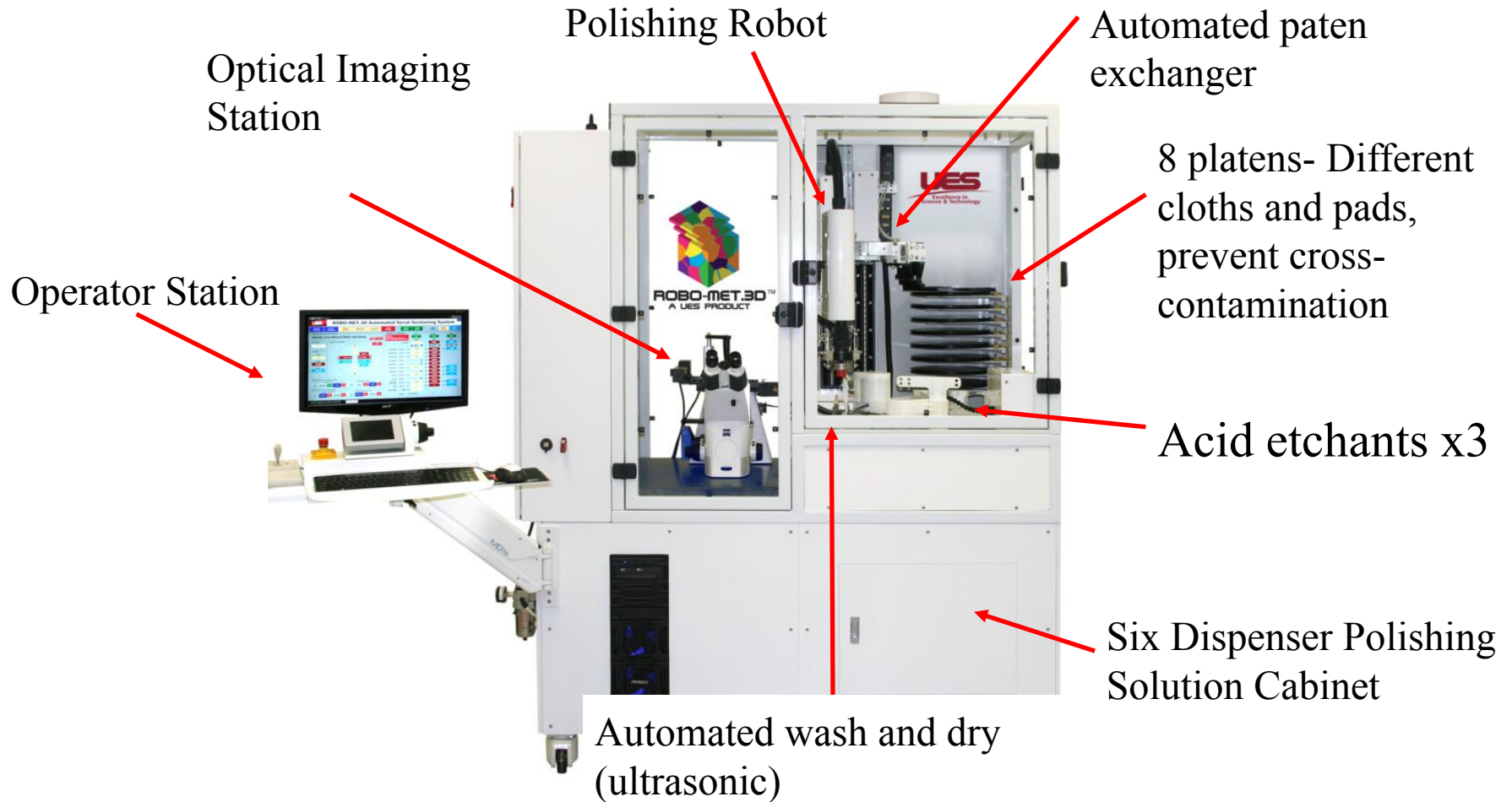
- ~14,500 mm²
- This scan was obtained in 16 hours.
- A conventional SEM with EBSD, operating under “normal” modes, would take ~10 years of 24 hour operation to obtain this scan.



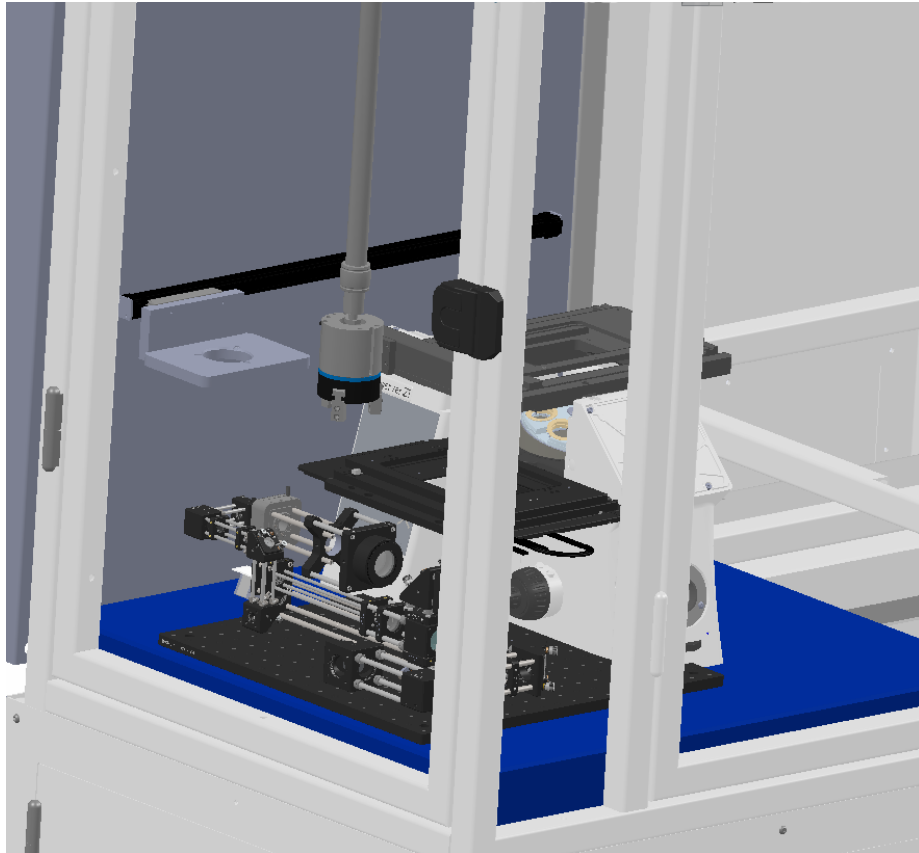
Hexagonal materials: SRAS on Ti 64



Integrating SRAS onto a Robo.Met-3D platform

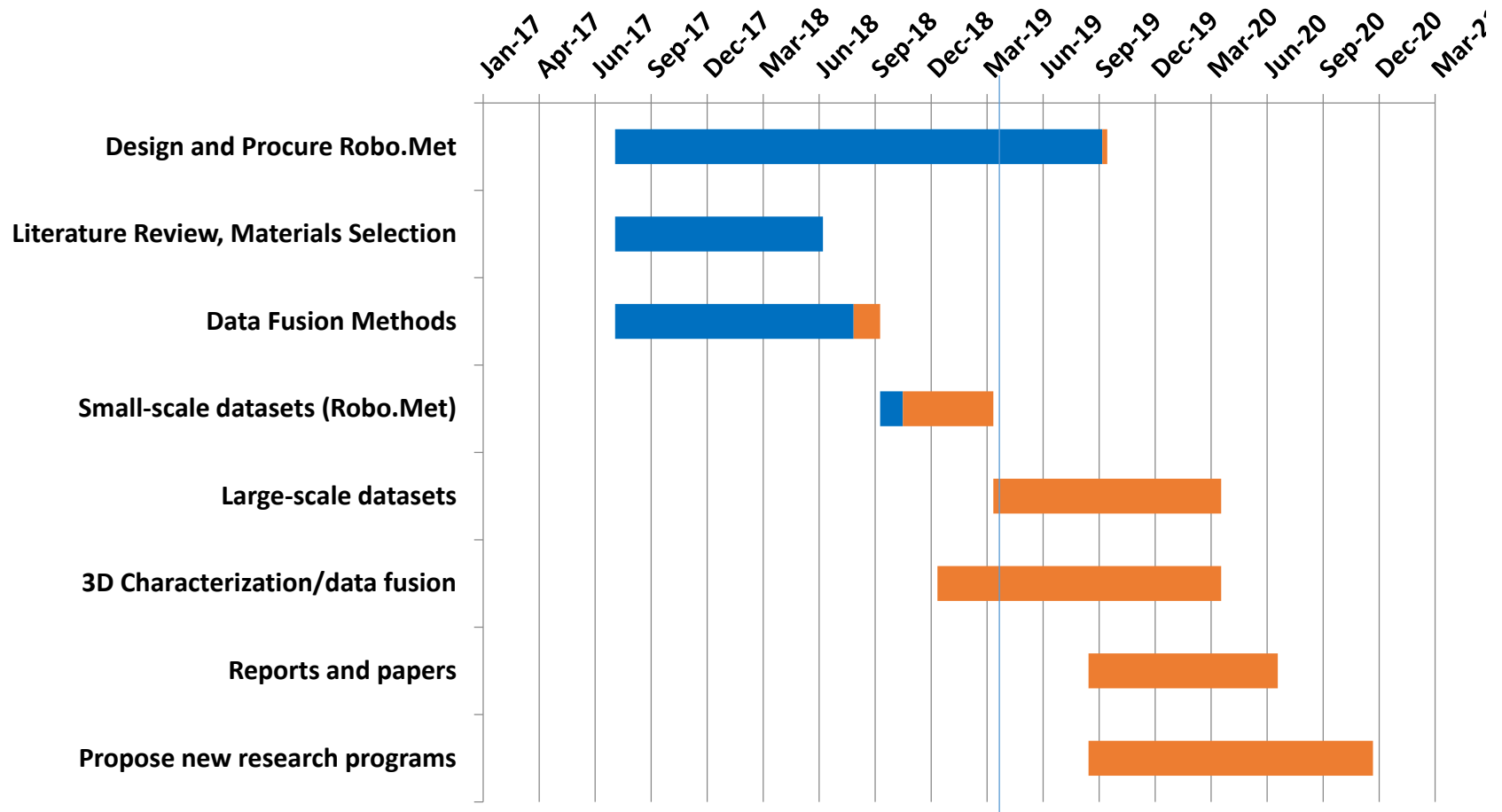


Integrating SRAS onto a Robo.Met-3D platform



- Evolution of plans:
 - Integrate the laser into the optical microscope (Zeiss wouldn't enable it)
 - Build a SRAS system to fit in the Robo.Met with a simple pneumatic transfer mechanism (where we are – space is very tight; laser-safe). Need to include z-axis on final optic.
 - Possibly replacing the optical microscope with a SRAS/OM system.

Gantt chart



Thank you!

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