

Project 31-L: Accumulative Roll Bonding of Al and Ti Sheets Toward Low Temperature Superplasticity

***Spring 2019 Semi-Annual Meeting
Iowa State University, Ames, IA
April 3-5, 2019***

Student: Brady McBride (Mines)

Faculty: Dr. Kester Clarke (Mines)

Industrial Mentors: Ravi Verma (Boeing), John Carpenter (LANL)

Project 31-L: Accumulative Roll Bonding of Al and Ti Sheets Toward Low Temperature Superplasticity



- Student: Brady McBride (Mines)
- Advisor(s): Kester Clarke (Mines)

Project Duration
PhD: September 2017 to March 2021

- **Problem:** Superplastic forming requires high temperatures and very low strain rates.
- **Objective:** Develop an in-depth understanding of how accumulative roll bonding affects temperature dependent strength and superplastic properties of Al and Ti alloys.
- **Benefit:** Low temperature superplasticity could result in reduced cost and cycle time due to reduced deformation temperatures and increased strain rates.

- Recent Progress**
- Five successful ARB cycles of Al 5083
 - Modification of existing ARB process to reduce edge cracking
 - Preliminary EBSD, TEM data from Al 1100 and Al 5083 roll bonded material
 - Design grips for superplastic tensile testing to mitigate sources of error

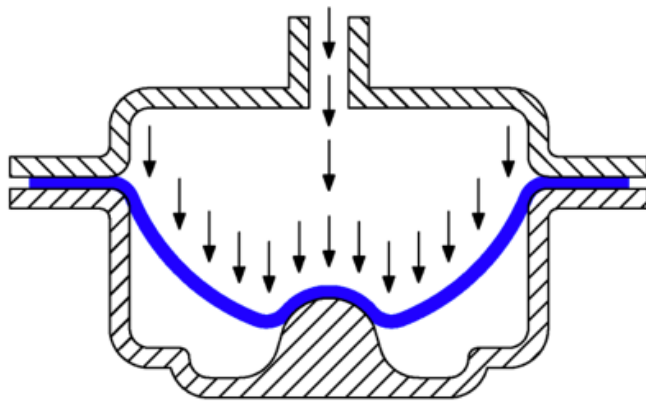
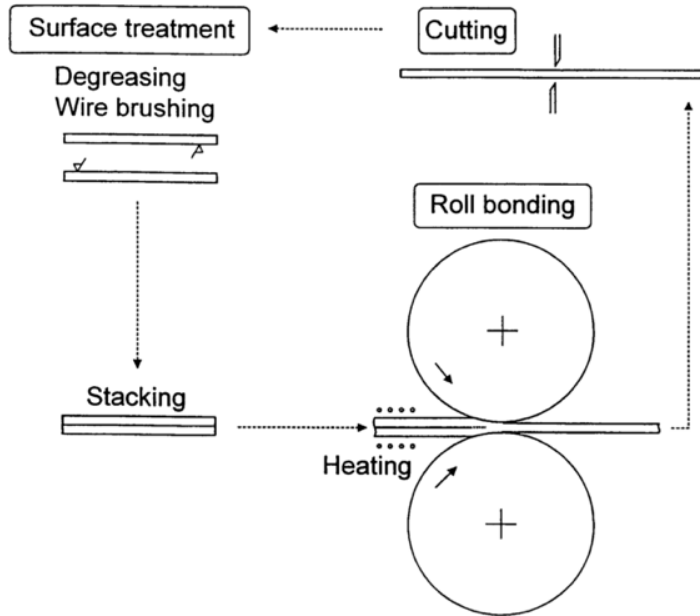
Metrics		
Description	% Complete	Status
1. Literature review	65%	●
2. ARB process development	100%	●
3. Investigate roll bonding process parameters (literature review)	100%	●
4. Mechanical & microstructural characterization	10%	●
5. Process refinement / alloy selection for optimized superplasticity	0%	●

Outline



- Project Overview / Industrial Relevance
- Introduction to Accumulative Roll Bonding (ARB) process
- Development of ARB Process
 - Al 1100 → Al 5083
- Mitigation of edge cracking
- Tensile testing for superplasticity
- Techniques for microstructural analysis
- Future Work

Industrial Relevance



Enhanced properties:

- Hall-Petch strengthening
- low temperature superplasticity

Applications:

- superplastic forming
- high strength sheet components

Benefits:

- reduced cycle time
- reduced die wear
- reduced processing cost

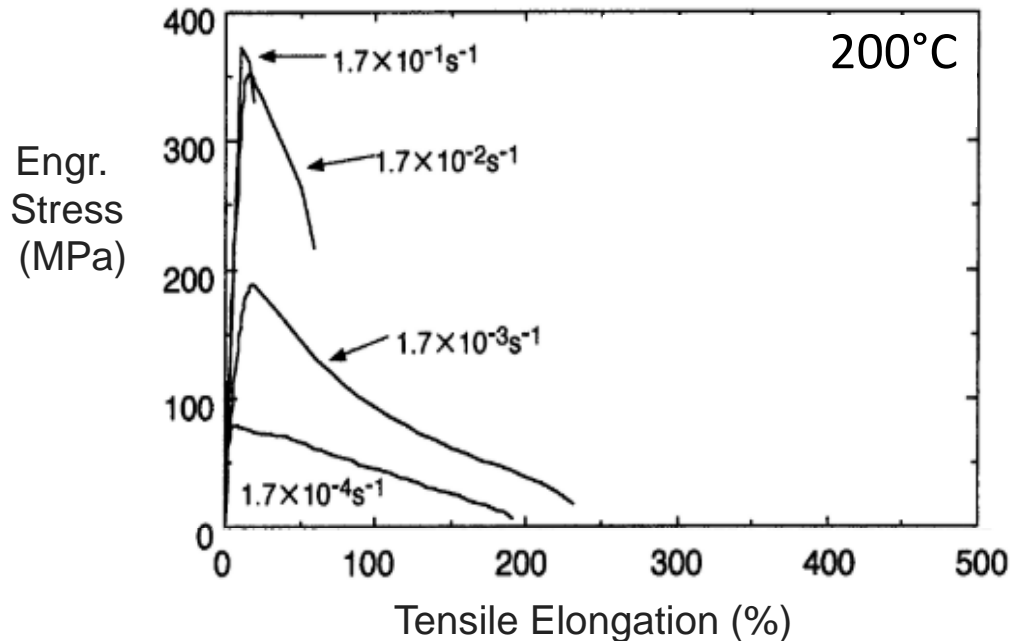
Project Motivation

Conventional superplasticity:

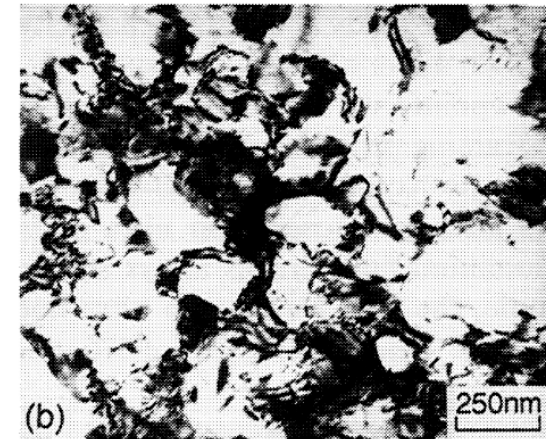
Grain Size: $< 10 \mu\text{m}$

Temperature: $\sim 500 \text{ }^\circ\text{C}$ ($0.9 T_H$)

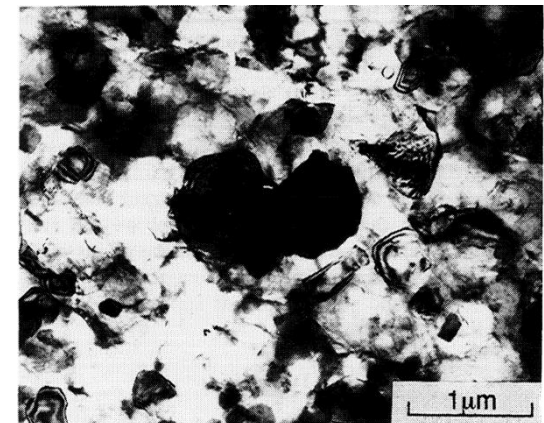
Elongation: $\sim 300\%$



6 ARB Cycles – 250 nm

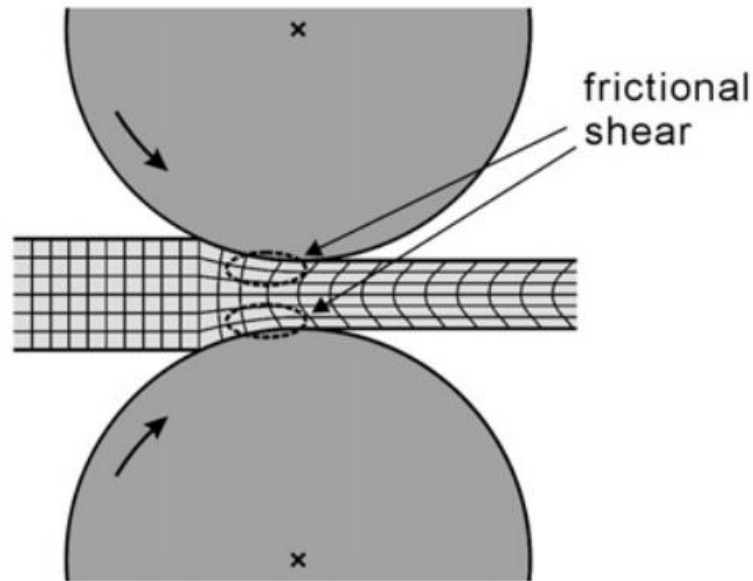


200 °C, 220% elongation – 580 nm

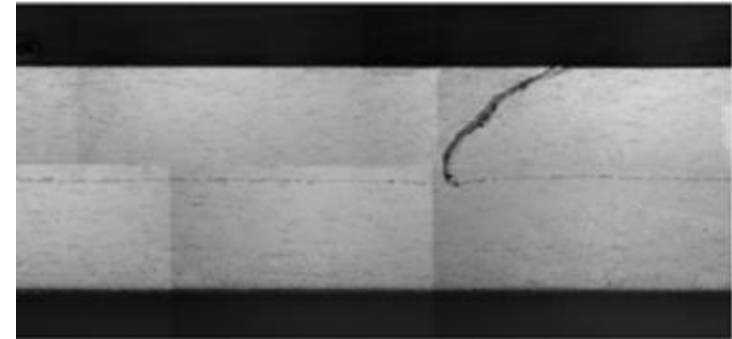


Role of Redundant Shear

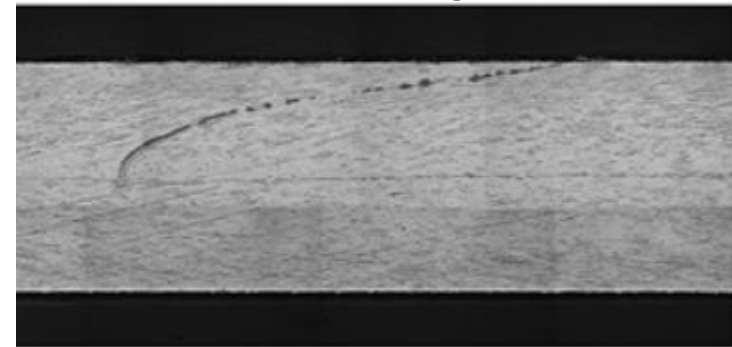
Q: How is ARB different from conventional rolling?



Lubricated – low friction



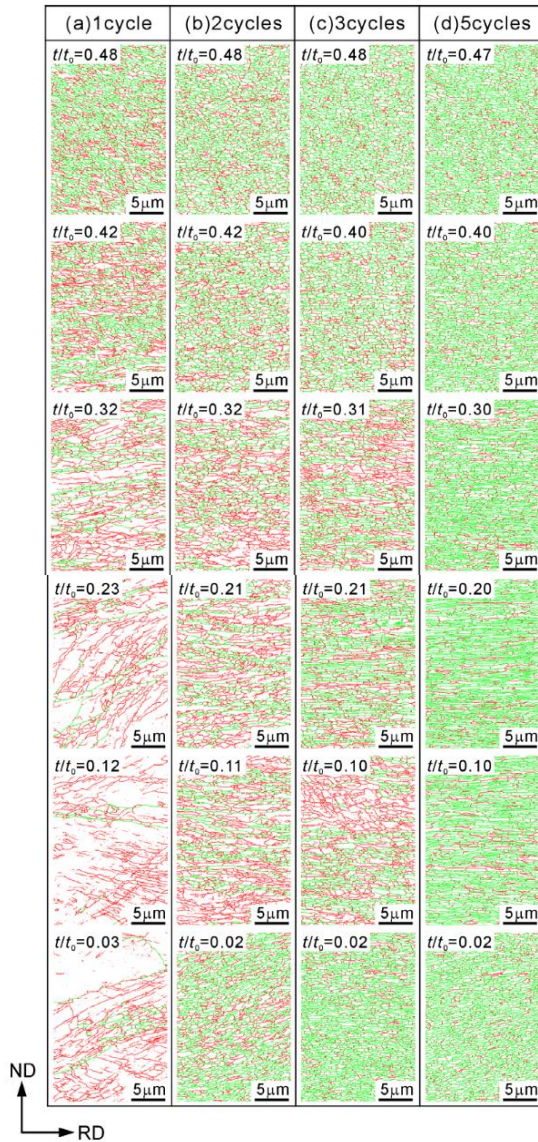
Unlubricated – high friction



ND
↑
RD
→

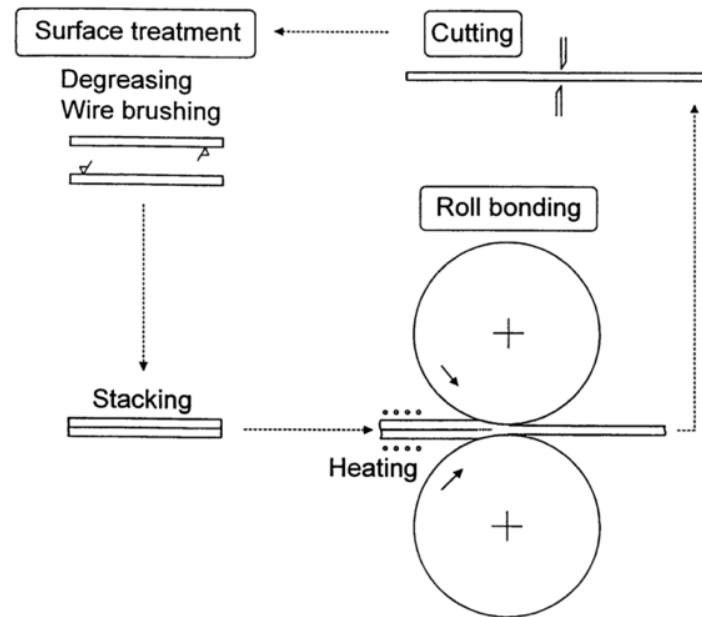
1mm

Role of Redundant Shear



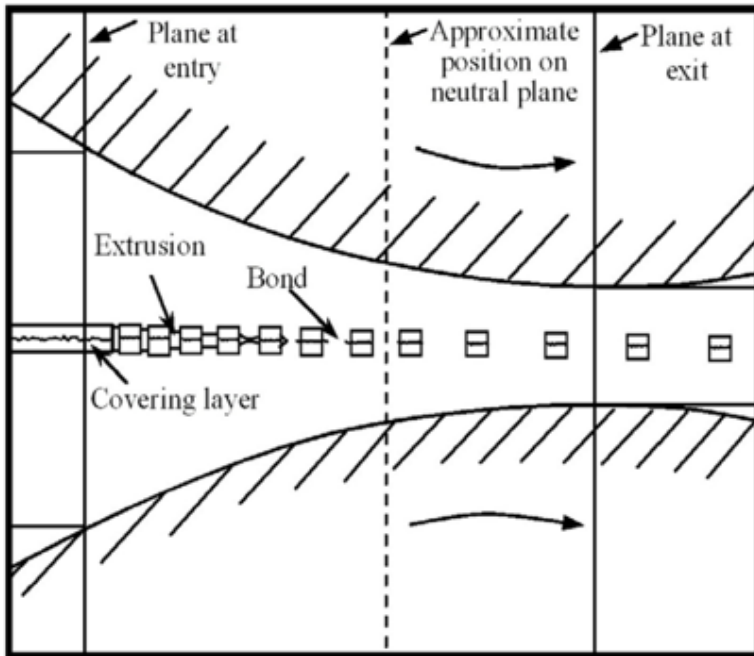
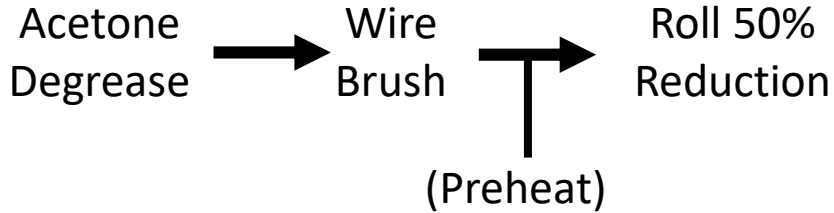
— $\theta \geq 15^\circ$

— $2^\circ \leq \theta < 15^\circ$

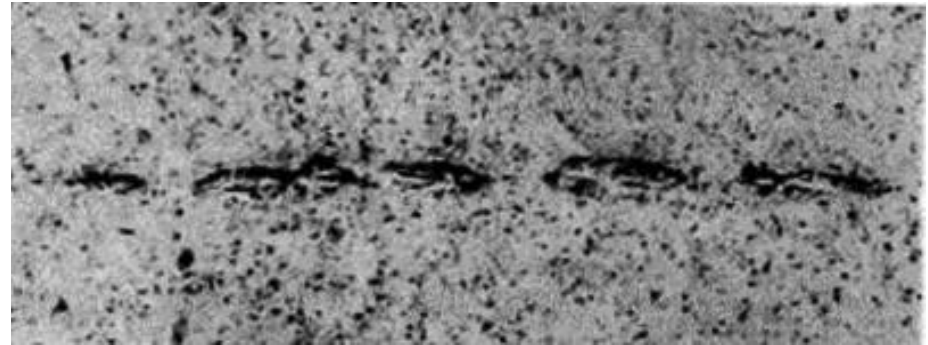


Homogenous microstructure through thickness after 5 ARB cycles in 1mm thick samples

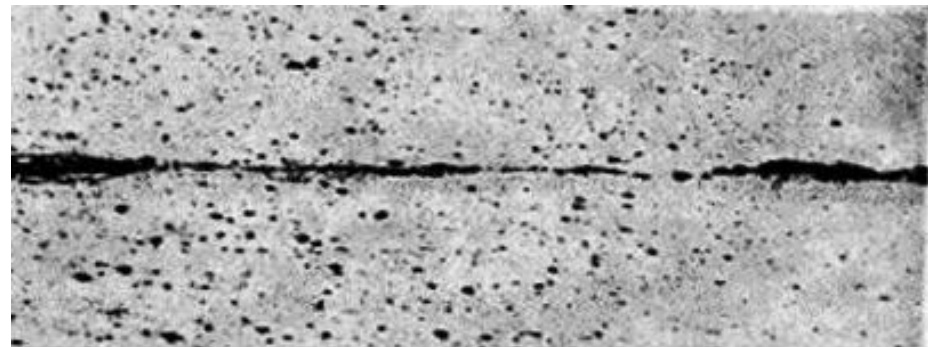
Surface Preparation



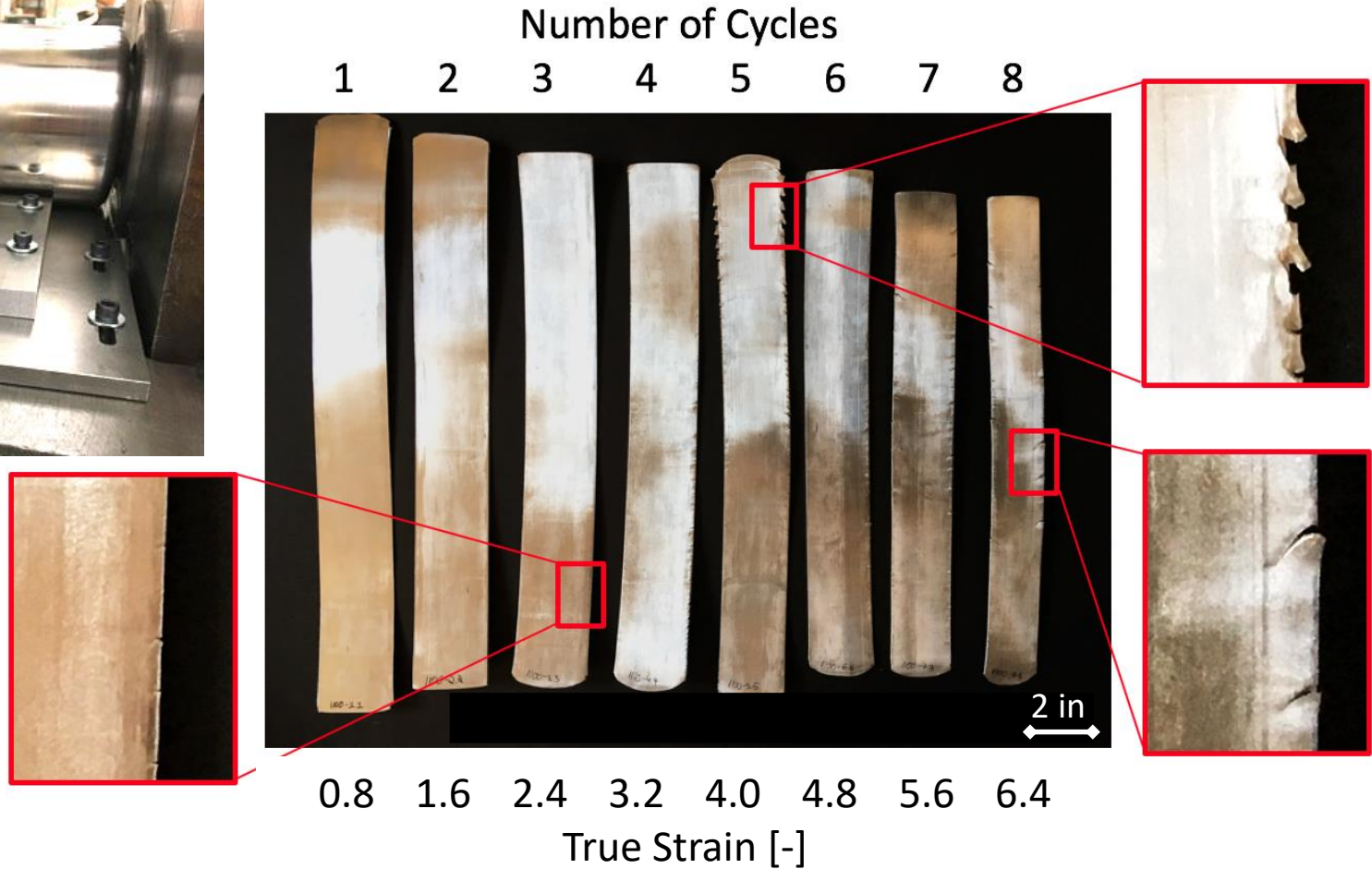
Room Temperature



100 μm
> 300 °C



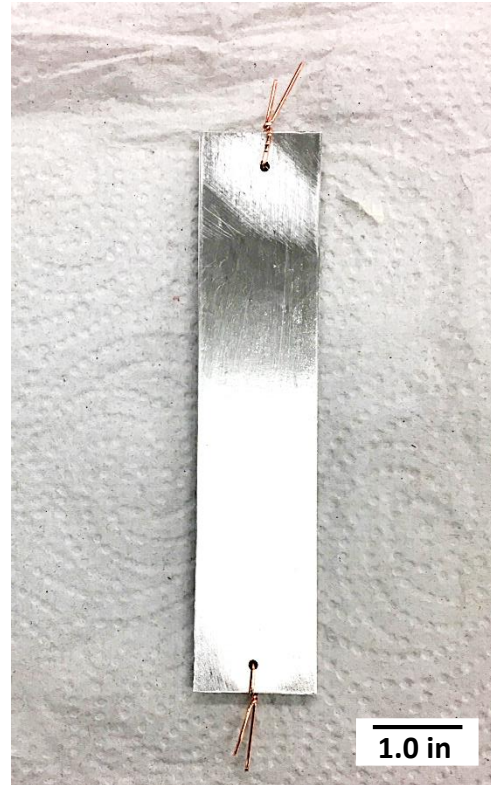
Al 1100 ARBed Samples



Edge Crack Mitigation



Material Overhang
Al 2024 – 2 ARB cycles



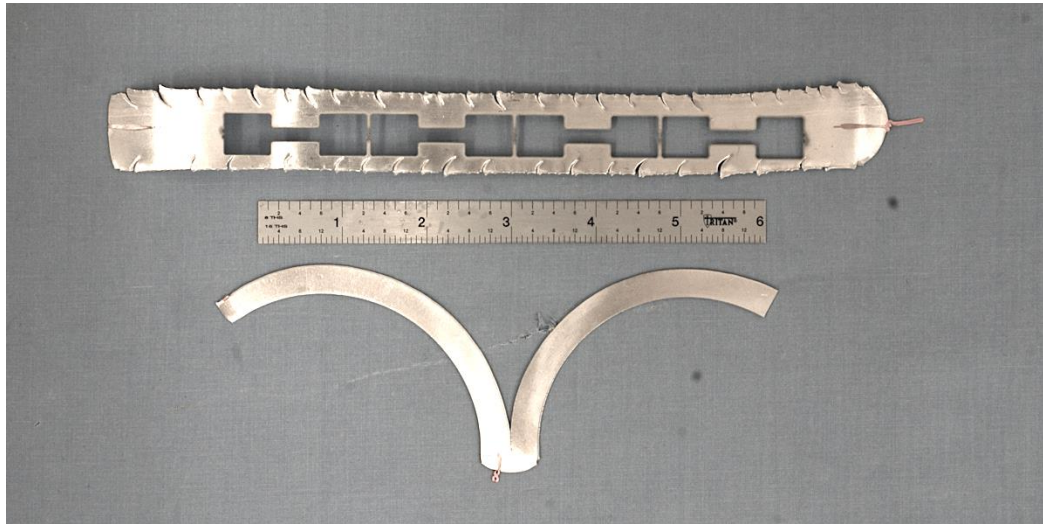
Wire Binding



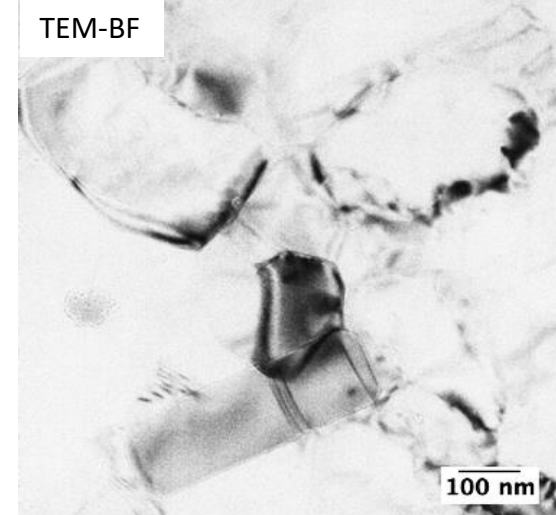
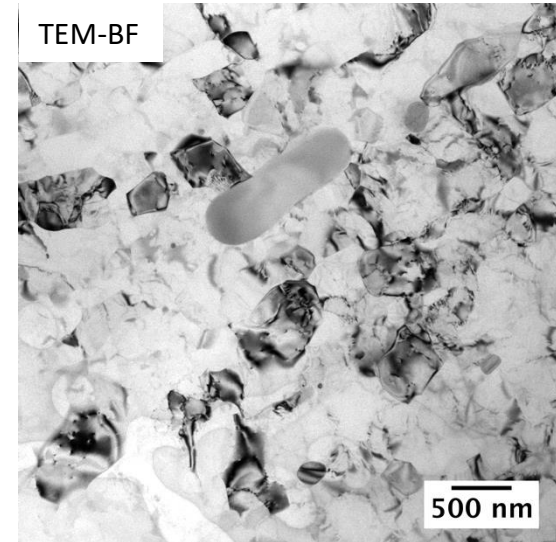
Lateral Spreading
Al 5083 – 4 ARB Cycles



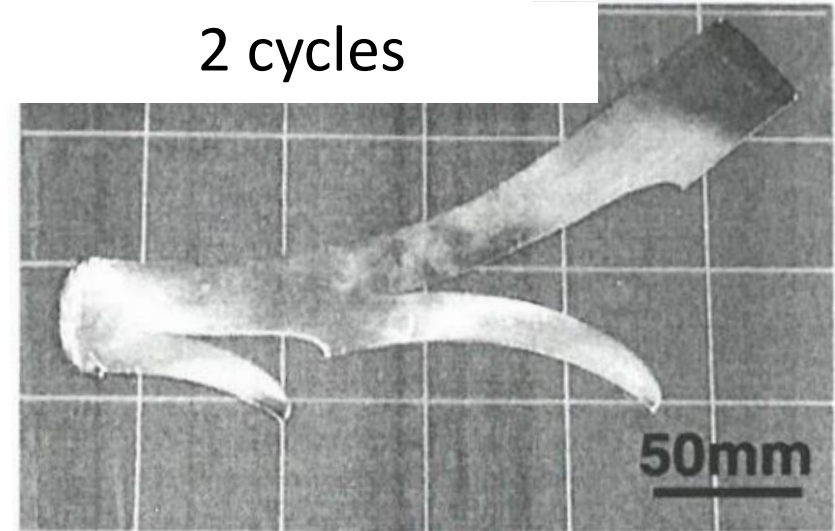
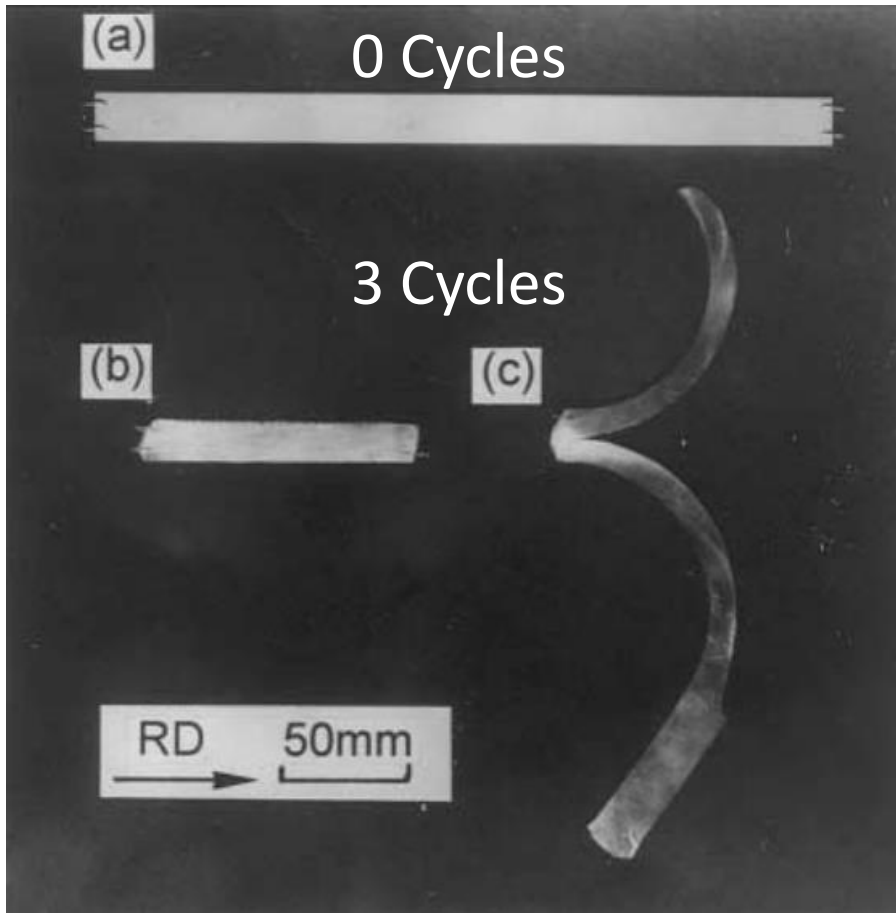
5 Cycles of Al 5083



ARB Cycles:	5
Individual layers:	32
True Strain:	~4.0
Effective reduction:	~96.9%
Grain size:	~500 nm

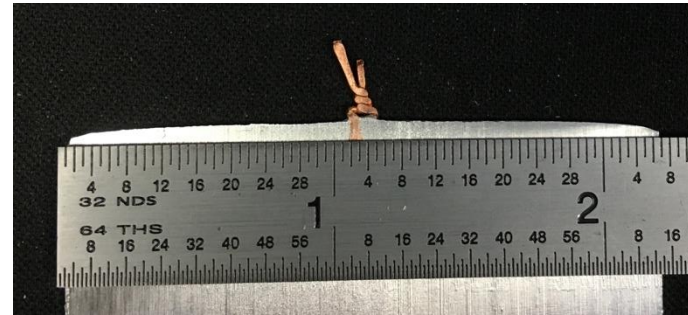
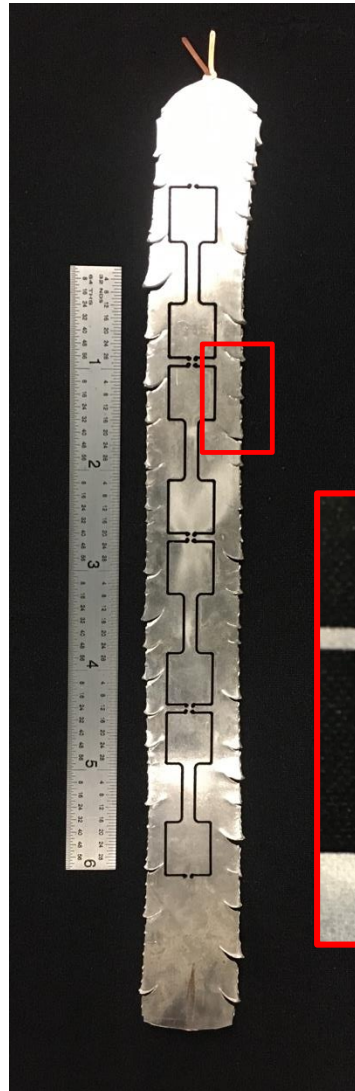


Edge Cracking in Literature



Al 5083 rolled at 200 °C

Edge Crack Mitigation



2 ARB Cycles



4 ARB Cycles

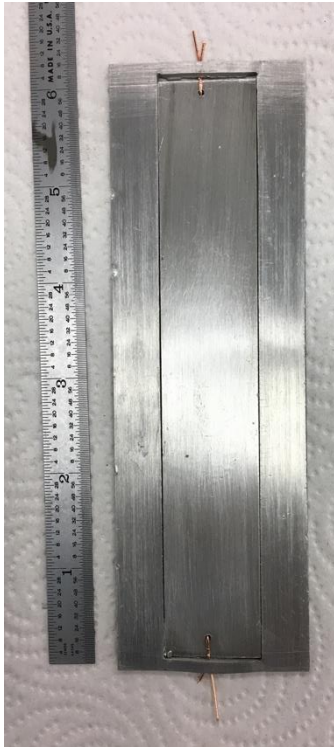


5 ARB Cycles

Edges elongate less than centerline due to **lateral spreading**, leading to edge cracking

Imposing Lateral Constraint

0.080" Al 1100 window



Constrained



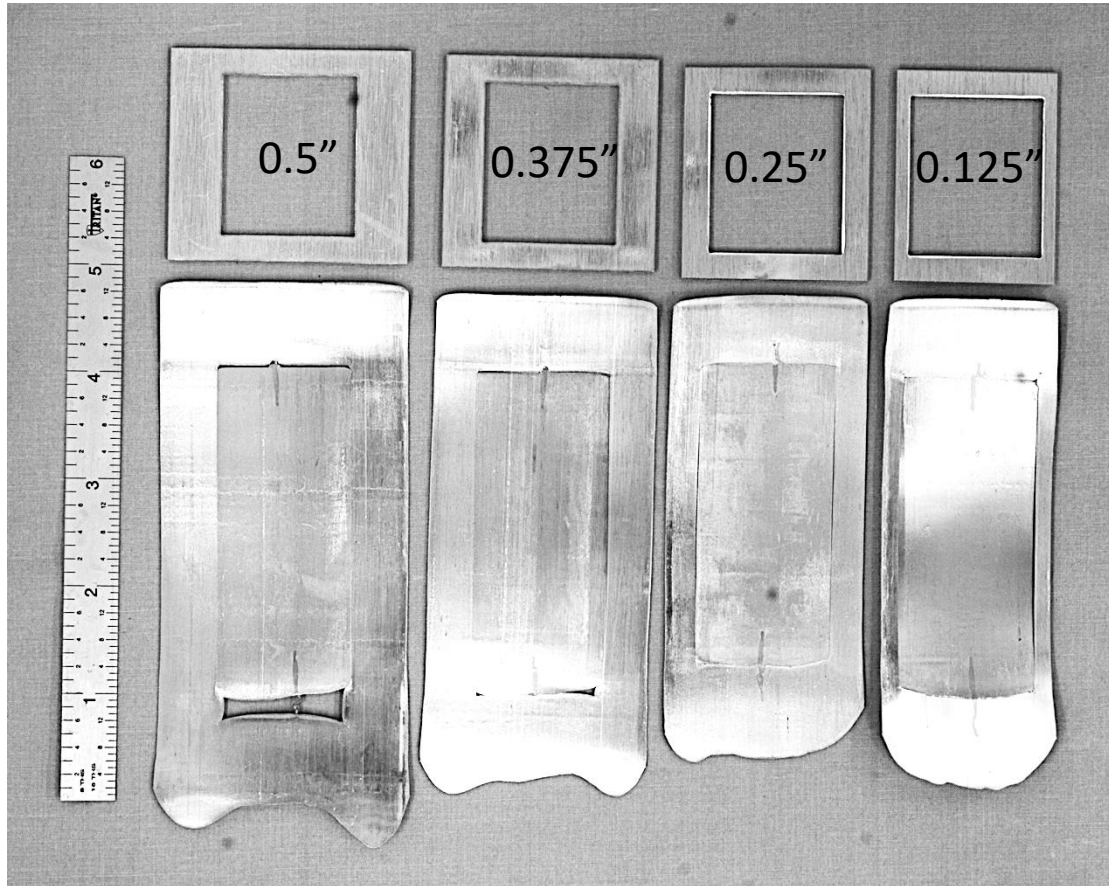
4 ARB Cycles
~0.035" spread

Unconstrained



2 ARB Cycles
~0.060" spread

Imposing Lateral Constraint



Lateral constraint
keeps spreading
below 0.040"

0.030"

0.027"

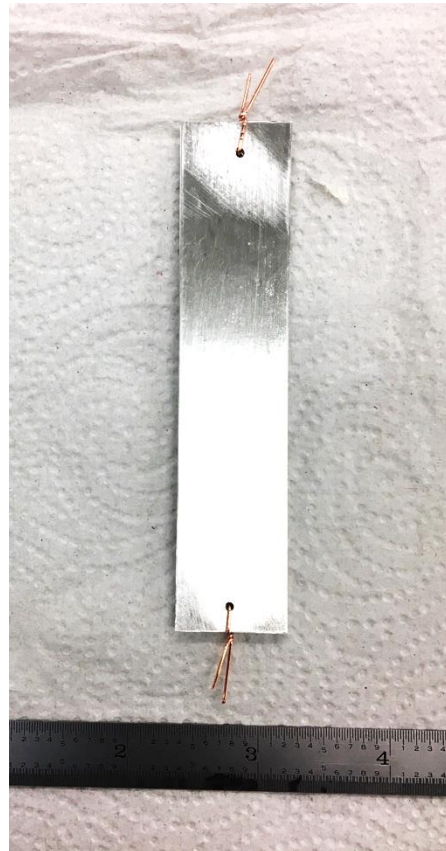
0.039"

0.030"

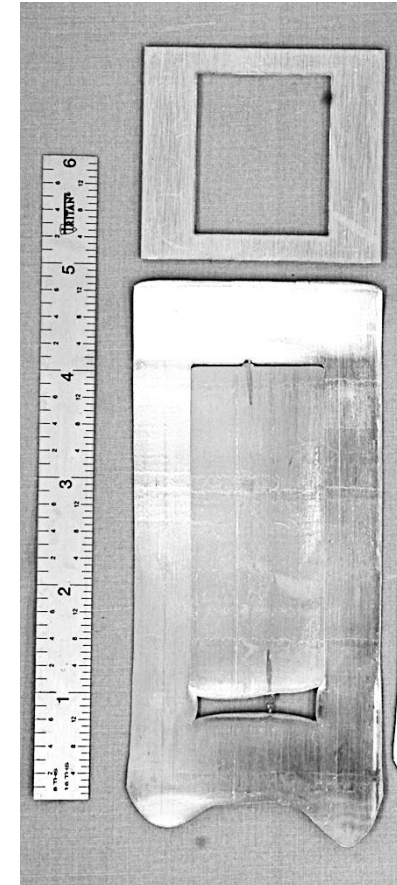
3 Constraints Needed



Edge Guides
Align Material to Mill



Wire Binding
Prevent relative movement



Lateral Constraint
Prevent lateral spreading

Superplastic Tensile Design

Temperatures: 200 – 500 °C

Strain Rates: $10^{-2} - 10^{-4} \text{ s}^{-1}$

Anticipated loads: 10 – 100 lbs

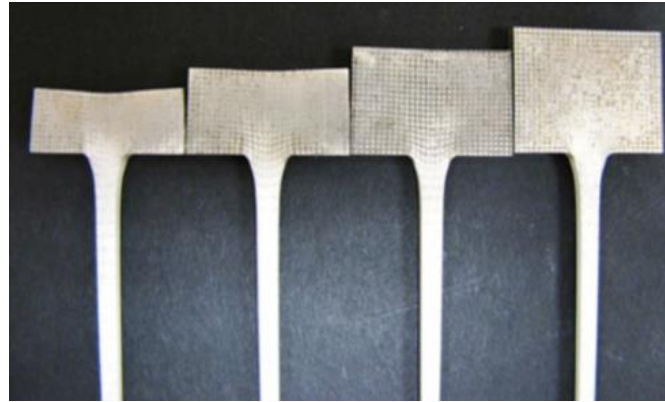
Control modes: Constant crosshead
Constant strain rate



Superplastic Tensile Design

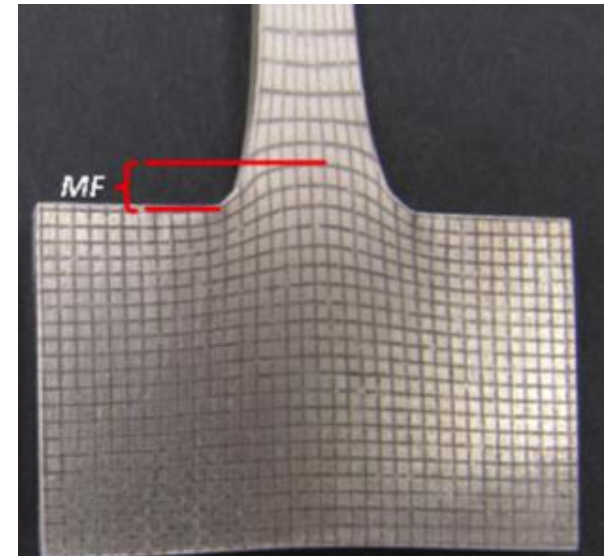


Variation in
gauge aspect ratio

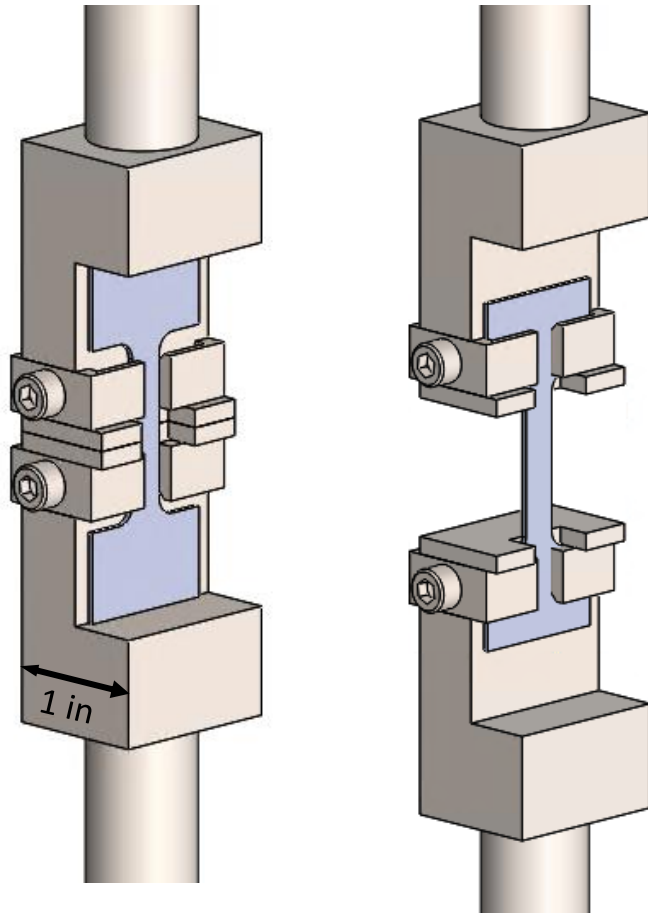


Variation in
grip aspect ratio

- Material flow leads to:
- elevated flow stress
 - elevated strain
 - inaccurate strain rates

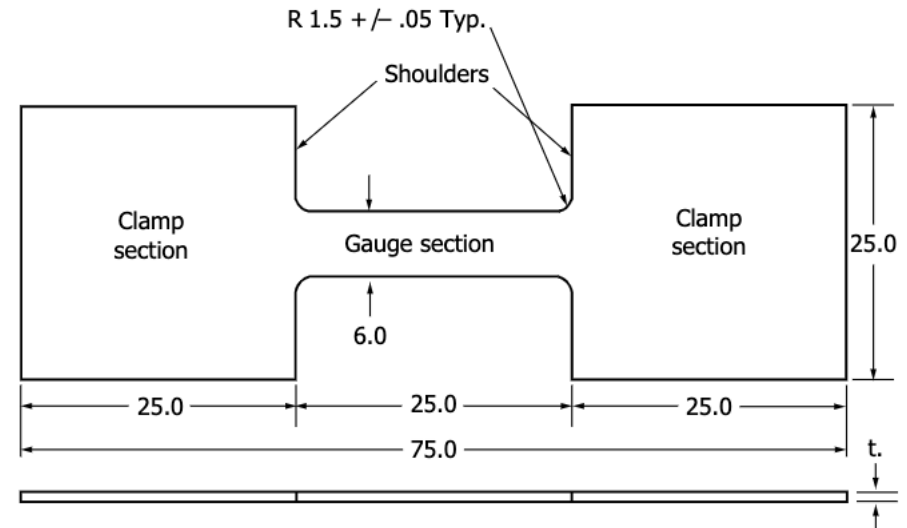


Superplastic Tensile Design



Drop-in placement

During testing



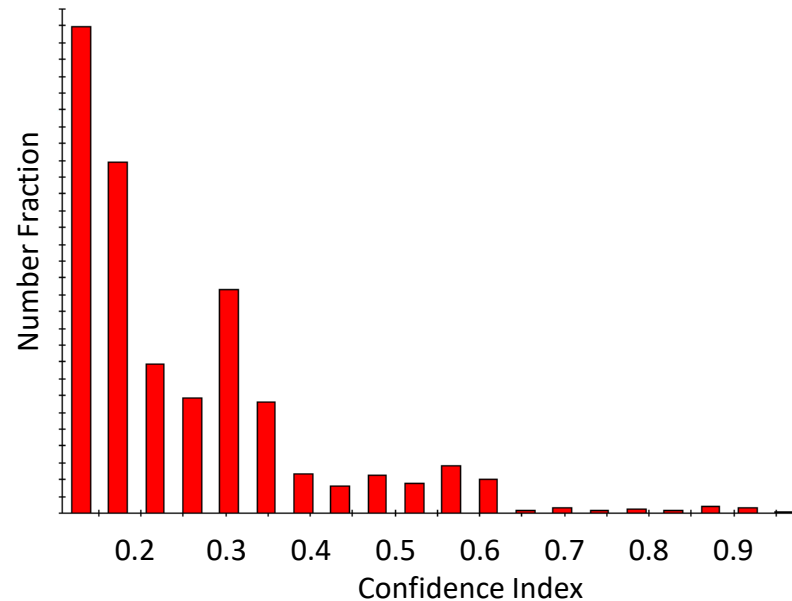
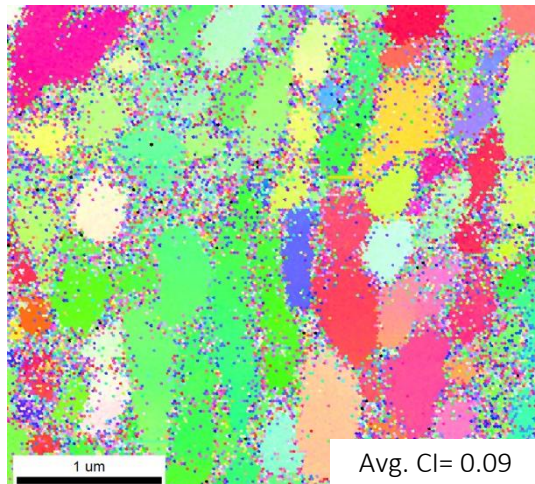
From ASTM E2448, dimensions in mm

Features:

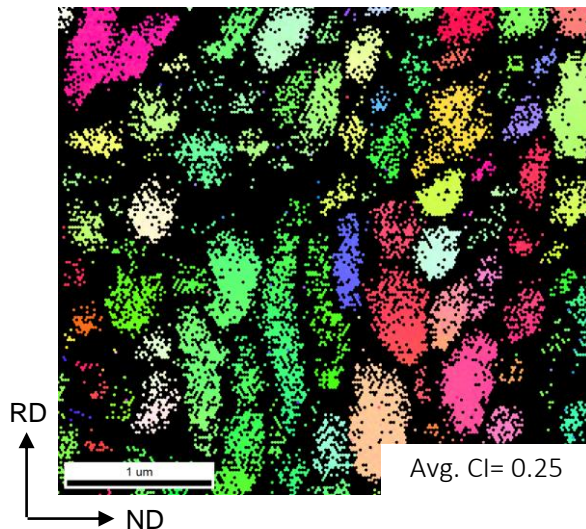
- drop-in specimen placement
- all load distributed through shoulder

Microstructural Characterization: Electron Backscatter Diffraction (EBSD)

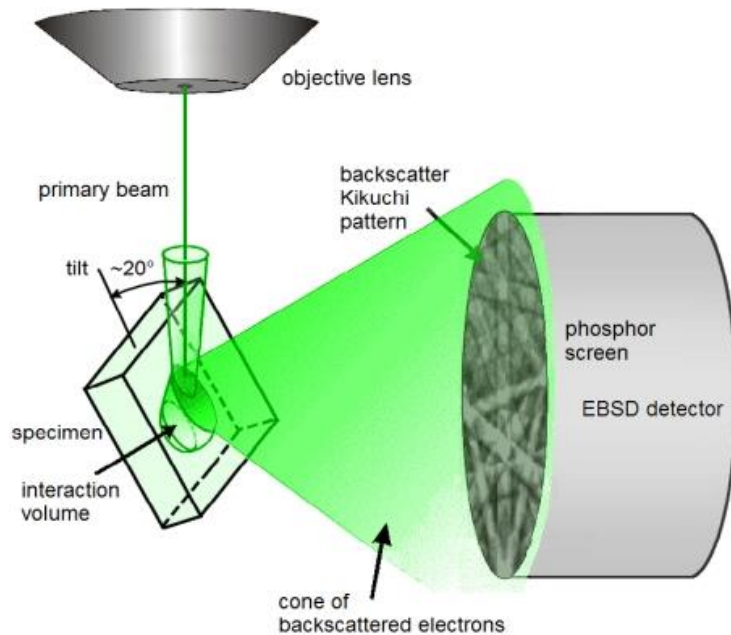
Al 1100 6 ARB



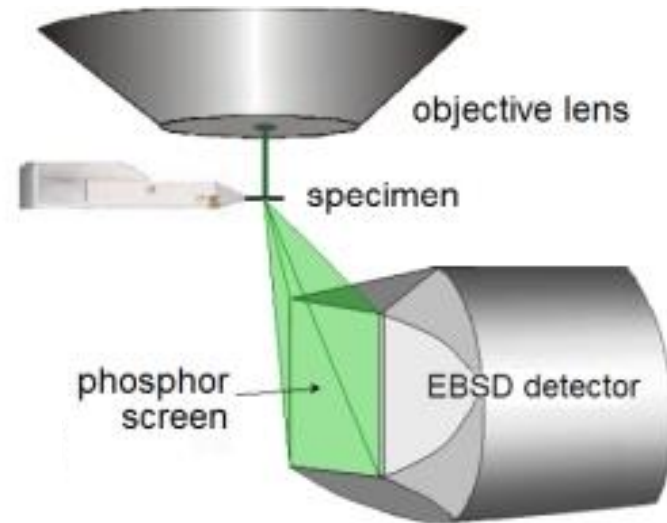
EBSD to quantify grain size and
study subgrain development



Microstructural Characterization: Transmission Kikuchi Diffraction (TKD)



EBSD



TKD

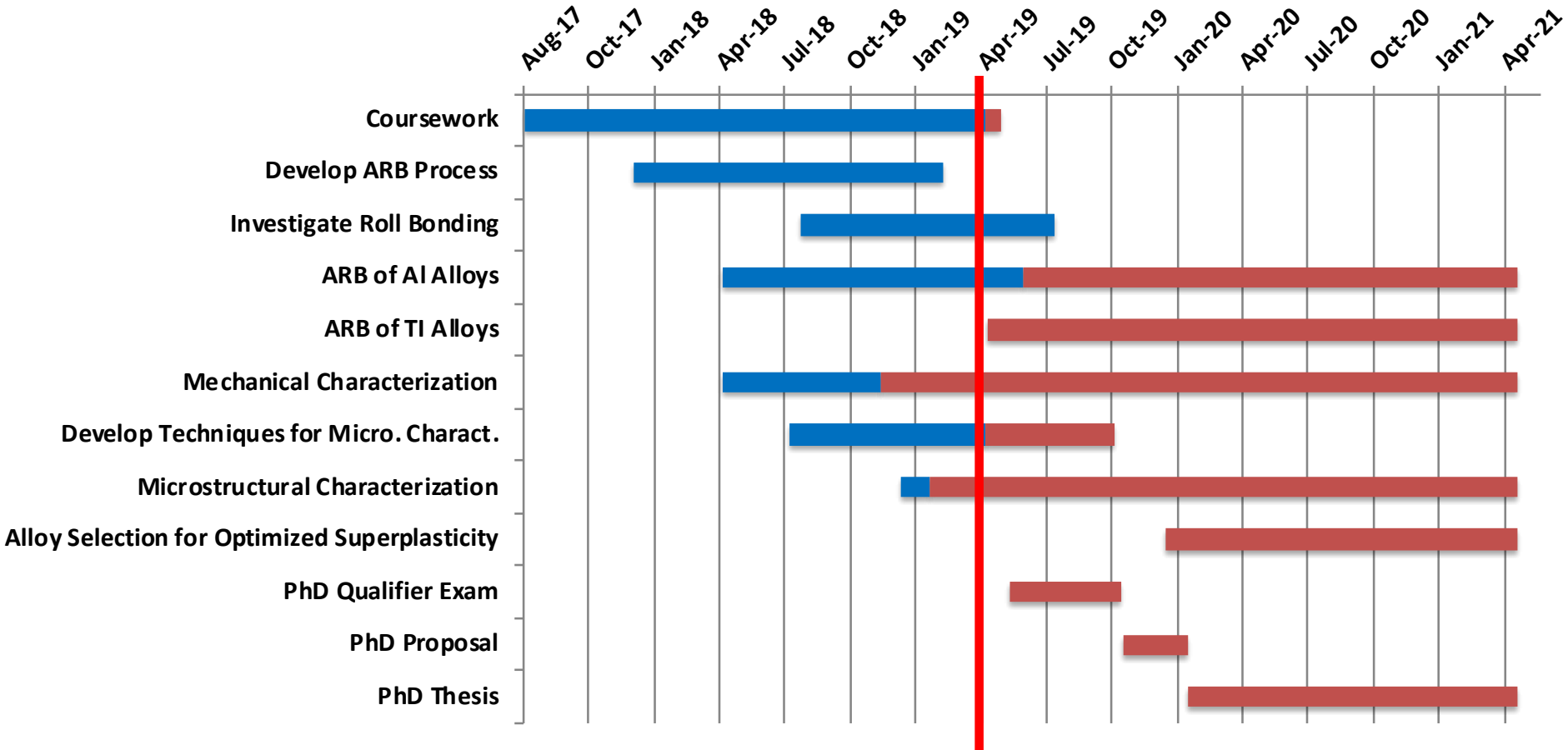
TKD: Less through-thickness interaction, ideal for submicron grains

Next Steps



1. Utilize knowledge of edge cracking to produce bulk material
→ Aluminum alloys 5083, 5182, 5754
2. Finalize and test superplasticity tensile setup
3. Continue to develop techniques for microstructural analysis
→ focused ion beam (FIB) and transmission Kikuchi diffraction (TKD)
4. Transition to titanium alloys (CP Ti)

Progress



Thank you!

Brady McBride
bmcbride@mines.edu

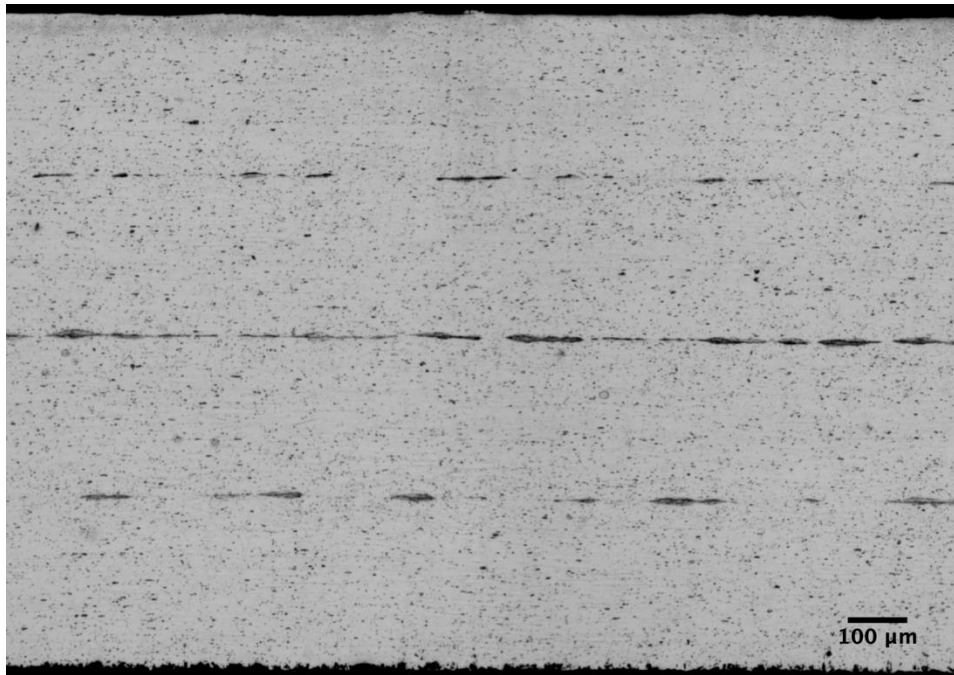
References



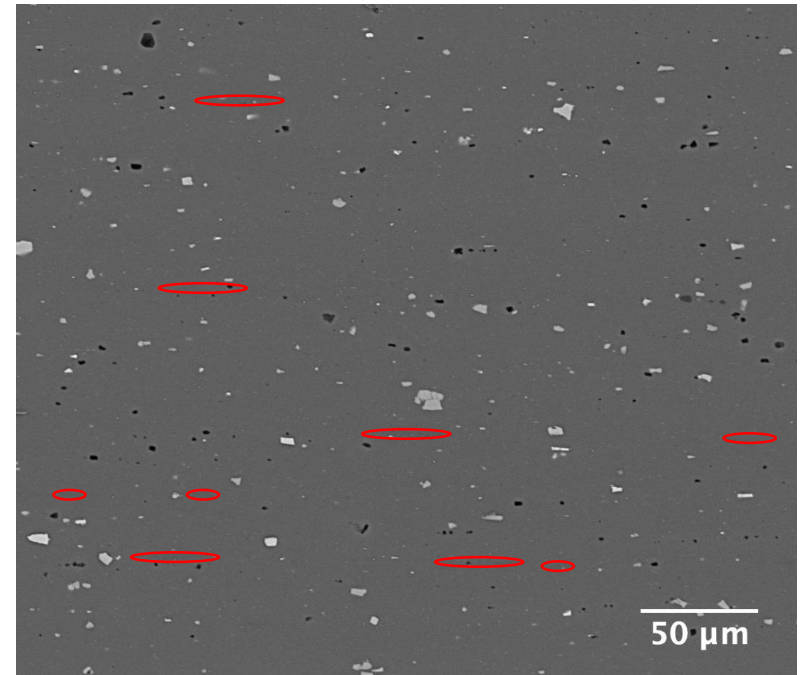
- [1] Y. Saito, H. Utsunomiya, N. Tsuji, and T. Sakai, “Novel ultra-high straining process for bulk materials—development of the accumulative roll-bonding (ARB) process,” *Acta Materialia*, vol. 47, no. 2, pp. 579–583, 1999.
- [2] R. M. Cleveland, A. K. Ghosh, and J. R. Bradley, “Comparison of superplastic behavior in two 5083 aluminum alloys,” *Materials Science and Engineering A*, vol. 351, no. 1-2, pp. 228–236, 2003.
- [3] N. Tsuji, K. Shiotsuki, and Y. Saito, “Superplasticity of ultra-fine grained Al-Mg Alloy by ARB,” *Materials Transactions*, vol. 40, no. 8, pp. 765–771, 1999.
- [4] N. Kamikawa, T. Sakai, and N. Tsuji, “Effect of redundant shear strain on microstructure and texture evolution during accumulative roll-bonding in ultralow carbon IF steel,” *Acta Materialia*, vol. 55, pp. 5873-5888, 2007.
- [5] M.G. Nicholas, D.R. Milner, Pressure Welding at Elevated Temperatures, *British Welding Journal*. 8 (1961) 375–383.
- [6] N. Tsuji, “Production of Bulk Nanostructured Metals by Accumulative Roll Bonding (ARB) Process,” in *Severe Plastic Deformation: Toward Bulk Production of Nanostructured Materials*, B. Altan, Nova Science, 2006, pp. 545-565.
- [7] F. Abu-Farha, M. Nazzal, and R. Curtis, “Optimum specimen geometry for accurate tensile testing of superplastic metallic materials,” *Experimental Mechanics*, vol. 51, pp. 903-917, 2010.

Bonding Interfaces

Etching exaggerates bonded interfaces



Al 1100
2 ARB Cycles
OIM, Keller's Reagent



Al 5083
5 ARB Cycles
BEI, As-Polished

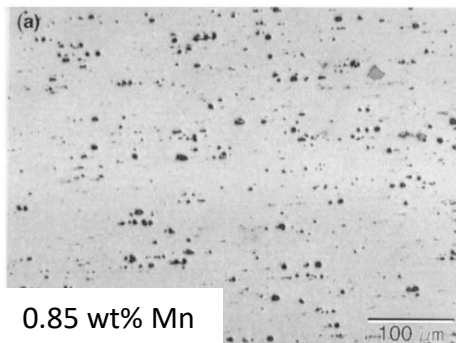
Fenn Rolling Mill



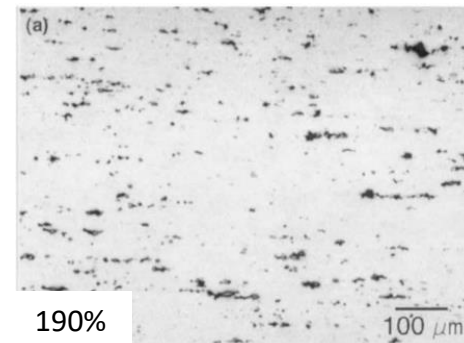
5.25" cold/hot rolls
100,000 lb capacity
37 RPM
50 SFPM

5XXX Aluminum

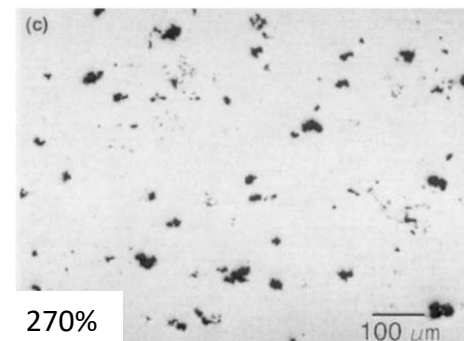
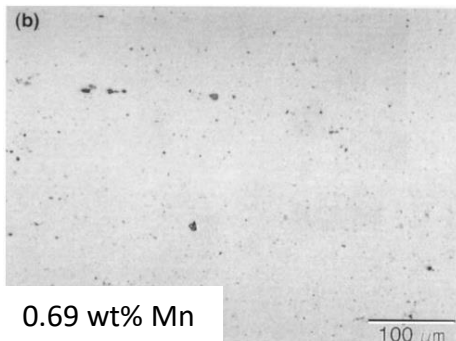
Alloy	Mg	Mn	Cr	Uses
5083	4.4	0.7	0.15	Marine, auto, aircraft applications
5182	4.5	0.35	<0.1	Automotive body panels, brackets
5754	3.5	<0.1	0.25	Storage tanks, pressure vessels, welded structures



500°C, 10⁻³ s⁻¹

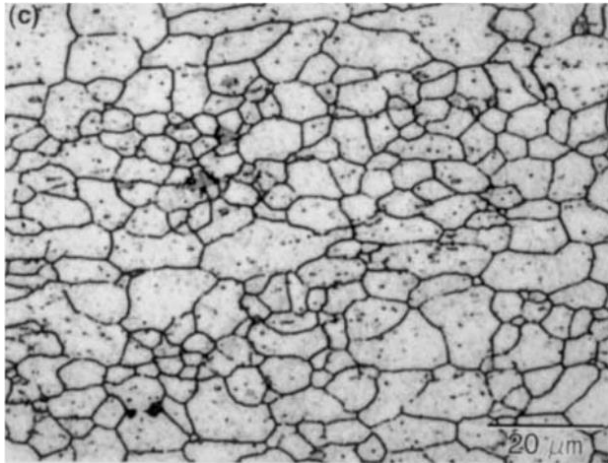


2nd phase particles → Cavity nucleation → Less superplastic ductility



Microstructural Characterization: Anodizing for LOM

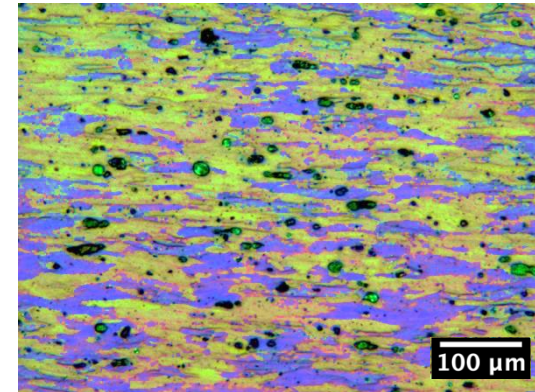
Precipitation Grain Contrast
16 hr at 120 C



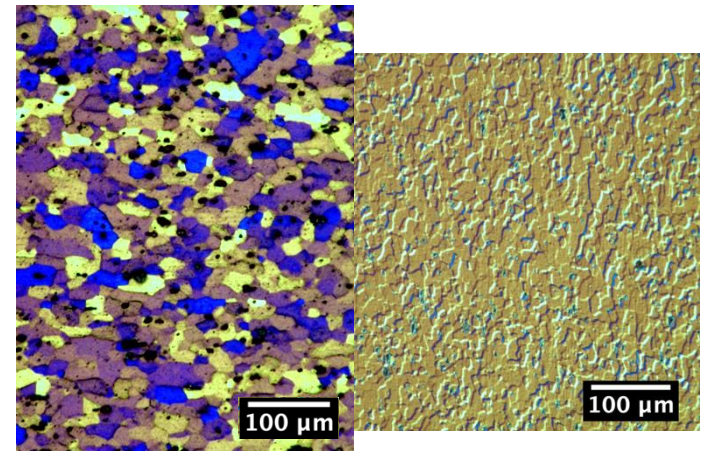
Cleveland et al., *Materials Science and Engineering A*, 2003.

Anodizing for quick analysis of
grain and deformation structures
without
thermally affecting microstructure

Anodizing with Barker's Reagent



Al 5083, 68% reduction



Recrystallized Al 5083

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Project Duration: *August 2017 – May 2021*

Achievement

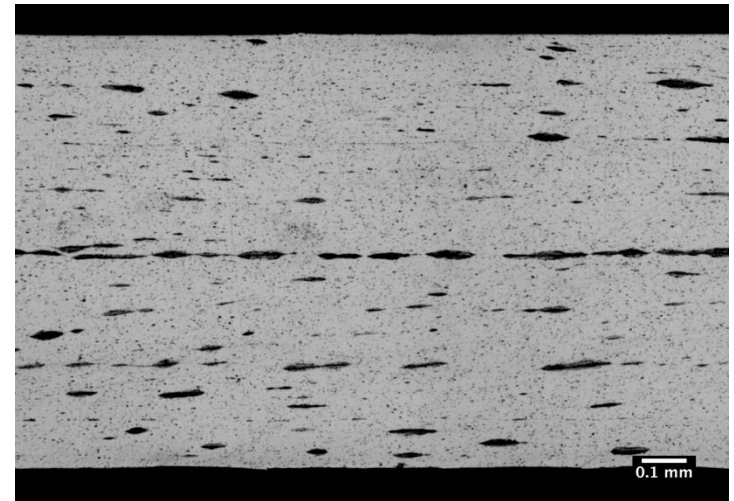
- Development of a process capable of producing ultra-fine grained microstructures in Al and Ti alloys that exhibit superplasticity at lower temperatures than conventional processing methods.

Significance and Impact

- Low temperature superplasticity would enhance superplastic forming operations by reducing cycle time as well as reducing costs related to heating and die wear.

Research Details

- Improved superplastic formability by means of reduced temperature and increased forming strain rates will reduce operating costs and prolong die life.



Cross-section of roll bonded Al 1100 showing interfaces between 128 individual layers of material.

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Program Goal

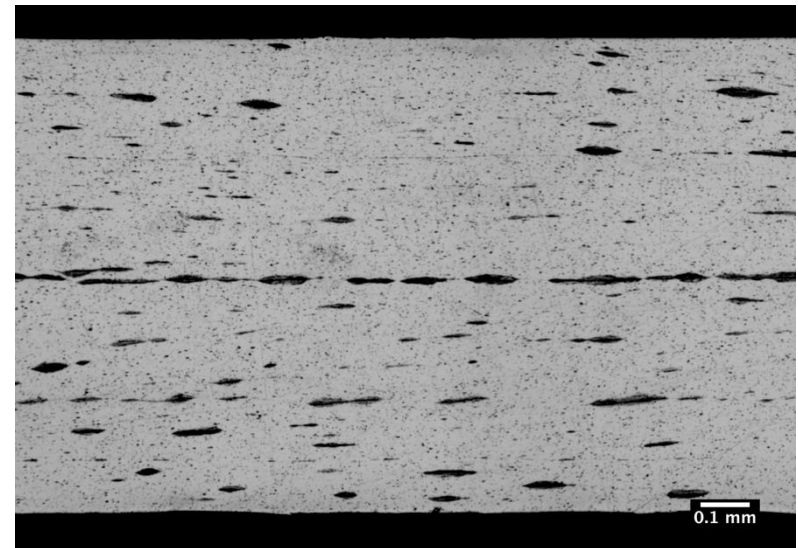
- Investigate enhanced superplasticity of ultra fine grained materials produced by accumulative roll bonding

Approach

- Develop a process for accumulative roll bonding and determine microstructural mechanisms related to superplasticity

Benefits

- Improved superplastic formability by means of reduced temperature and increased forming strain rates will reduce operating costs and prolong die life



Cross-section of roll bonded Al 1100 showing interfaces between 128 individual layers of material.