

## ***Project 37-L: Advanced Engineered Coatings with Extended Die Life for Tooling***

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*Faculty: Steve Midson, Andy Korenyi-Both, Michael Kaufman (Mines)*

*Industrial Mentors: Paul Brancaleon (NADCA)*



COLORADO SCHOOL OF  
**MINES**

**IOWA STATE  
UNIVERSITY**

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# Project 7-L: Advanced Engineered Coatings with Extended Die Life for Tooling



- Student: Nelson Delfino de Campos Neto (Mines)
- Advisor(s): S. Midson; A. Korenyi-Both, M. Kaufman (Mines)

**Project Duration**  
PhD: August 2018 to July 2023

- **Problem:** Molten aluminum tends to solder to die faces in die casting process and is used a large amount of lubricant in the attempt to reduce the adhesion but reduces the parts quality.
- **Objective:** Identify PVD coatings to be applied to die casting dies to avoid the molten aluminum soldering and understand the adhesion mechanisms involved.
- **Benefit:** Increase die casting parts quality, eliminate the use of lubricants, extend the dies life and reduce cost-per-parts.

- Recent Progress**
- Literature review.
  - Development of an improved adhesion test.
  - Initial tests using the new adhesion test.
  - Initial characterization.

## Metrics

Description	% Complete	Status
1. Literature review and development of an improved adhesion test that simulates the die casting process by incorporating a mechanism to pressurize/quick fill the liquid aluminum against the coating.	20%	●
2. Identification of the mechanisms that rules the adhesion behavior.	10%	●
3. Identification of a working layer coating that is free of molten aluminum adhesion by laboratory tests	5%	●
4. Development of a coating architecture (single or multi-layer) that will add sufficient durability to the die coatings to allow them to survive for as long as the die casting die itself (□ 100,000 shots)	0%	●
5. Guidelines for depositing the coating system on die components/die tooling and in-plant trials.	0%	●

# Industrial Relevance



- Reducing or eliminating lubricant spray will:
  - Significantly **improve the quality** of the die castings
    - Reduce gas porosity and scrap
    - Used in higher performance applications
  - **Reduce costs**
    - Eliminate purchase costs for lubricants
    - Reduce effluent clean-up costs
    - Significantly extend die life
  - **Improve productivity**
    - Faster cycle rates

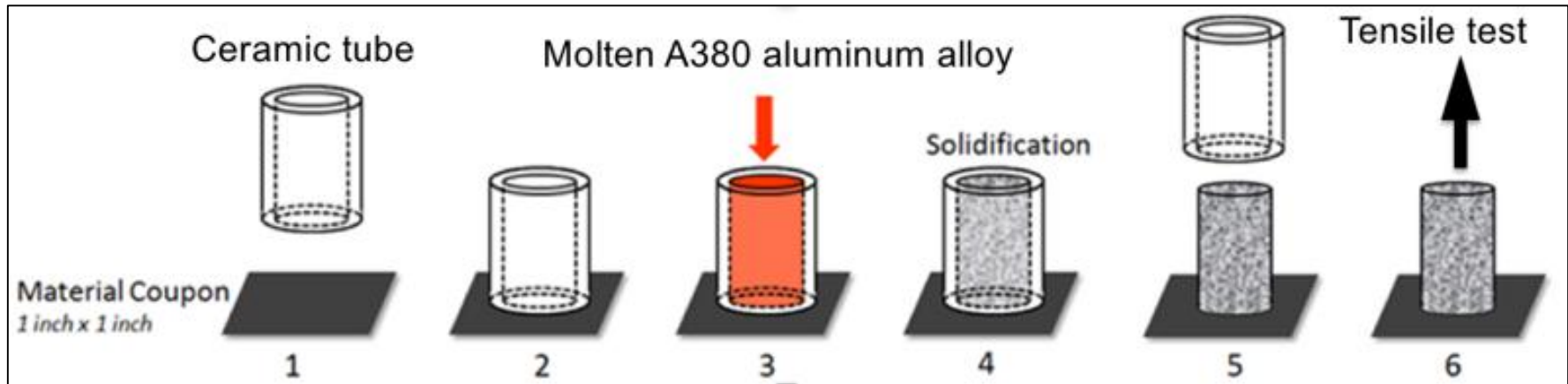
# Project Tasks



1. Develop improved adhesion test
2. Define mechanism controlling wetting and adhesion of molten aluminum to coating
3. Develop a coating architecture to provide long life
4. Conduct in-plant trials
5. Create guidelines for depositing the coating on tooling

# Previous Adhesion Test

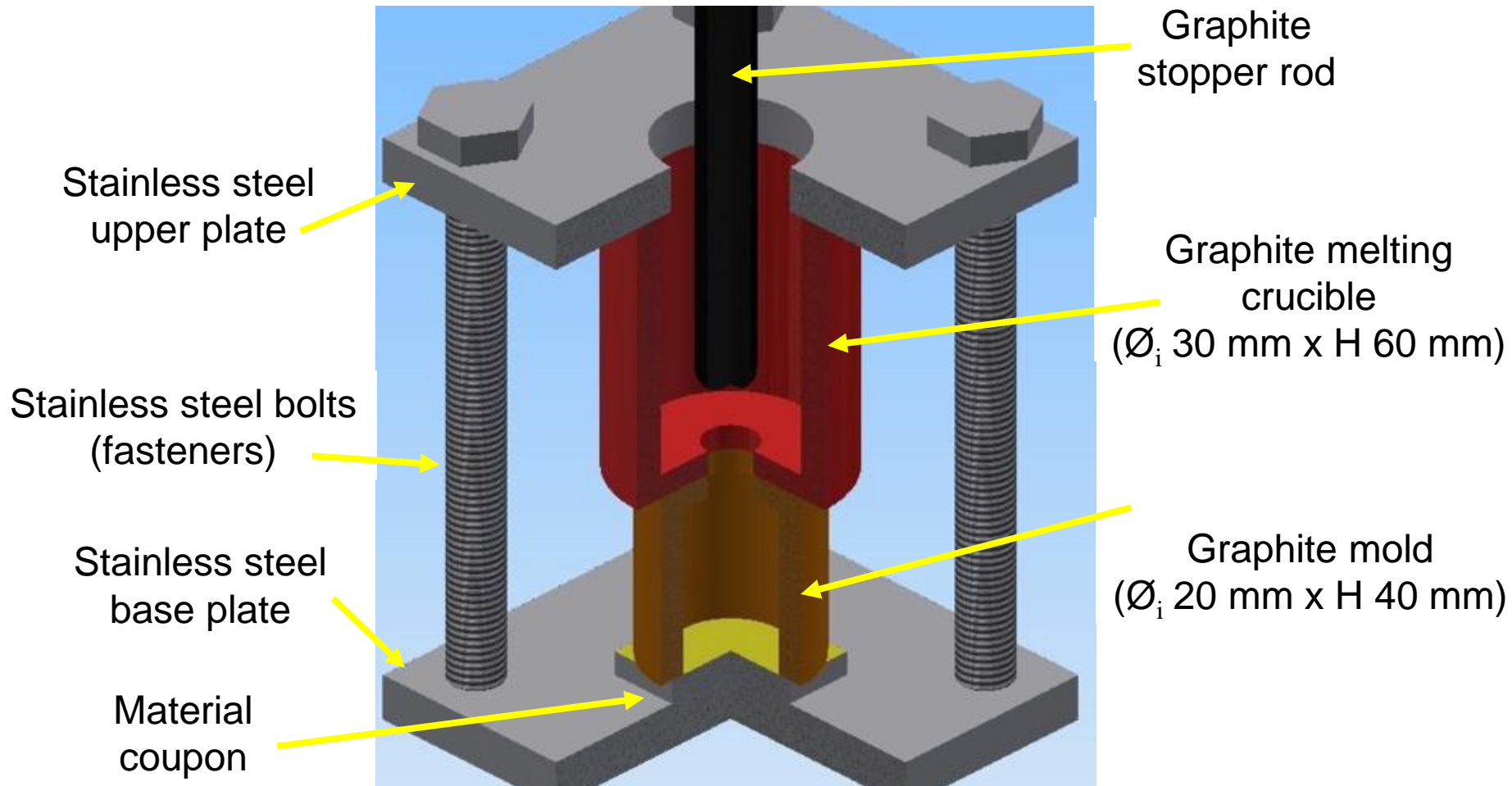
- Previous project developed a laboratory test
  - To measure adhesion of aluminum to coating



- Drawback:
  - Top pouring can carry the oxide layer from the upper surface of the molten aluminum into the crucible to contact with the material coupon

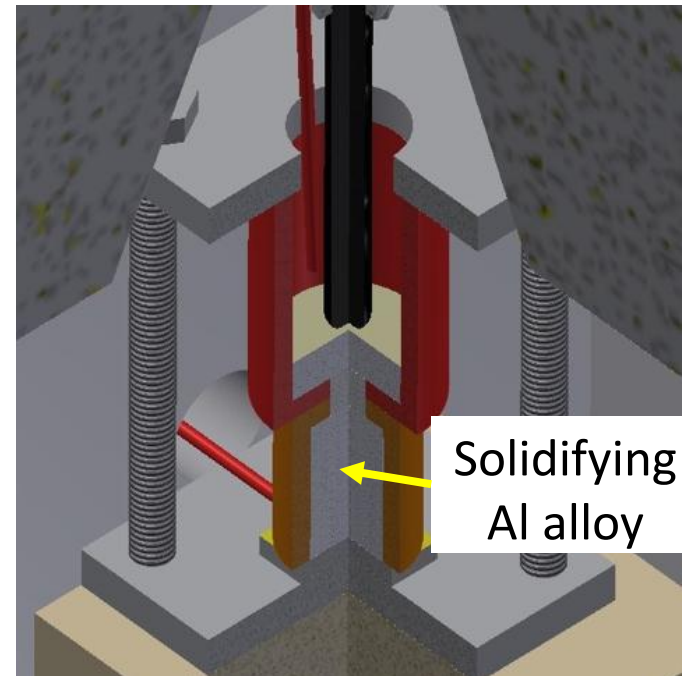
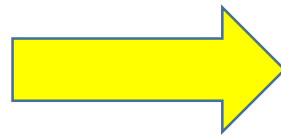
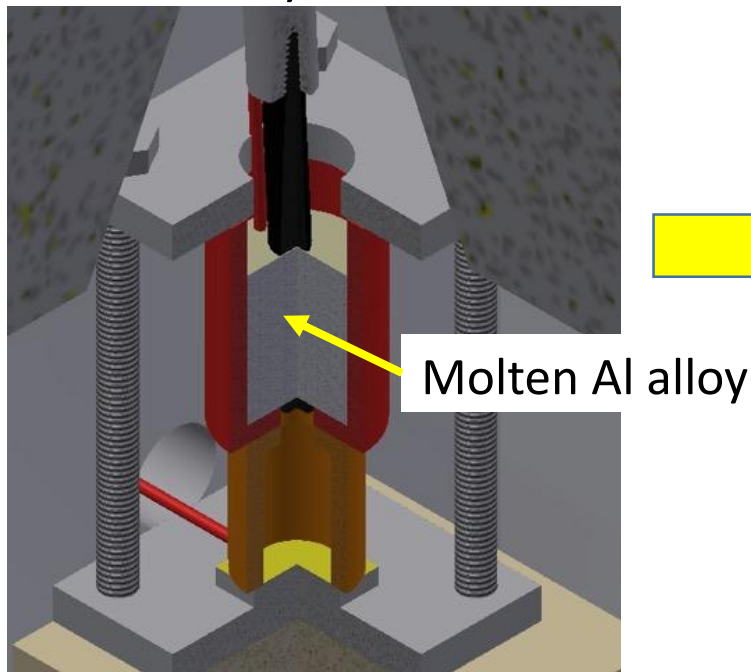
# 1st Proposed Solution

- Development of a setup to allow bottom pouring and avoid the top oxide layer from the molten alloy be in contact with material coupon



# Bottom Pouring at Resistance Furnace

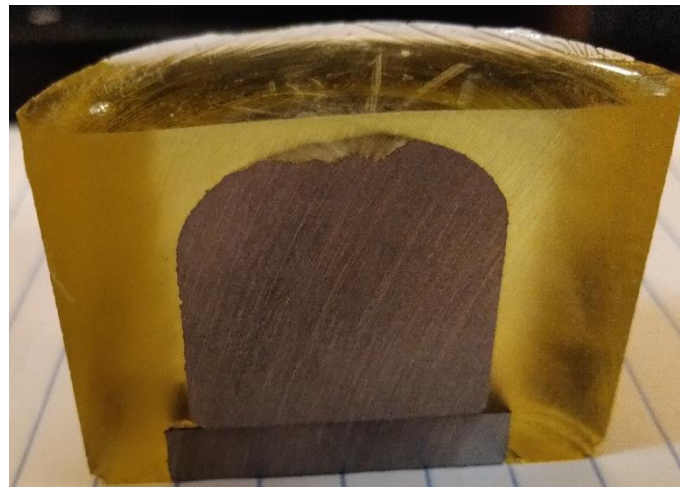
- Entire unit is placed into room temperature resistance furnace
- Aluminum pieces are placed into upper chamber
- Unit is heated to 700°C (~50 minutes)
- Stopper rod is removed
- Aluminum falls into lower chamber and contacts substrate test material
  - Surface oxide remains behind in upper chamber





# 1<sup>st</sup> Proposed Adhesion Test

- Molten aluminum is held in contact with substrate for controlled period of time
- Temperature is recorded during entire experiment
- Entire unit is slowly cooled to room temperature
- Setup is disassembled
- Sample can be tensile tested





# Drawbacks of this approach

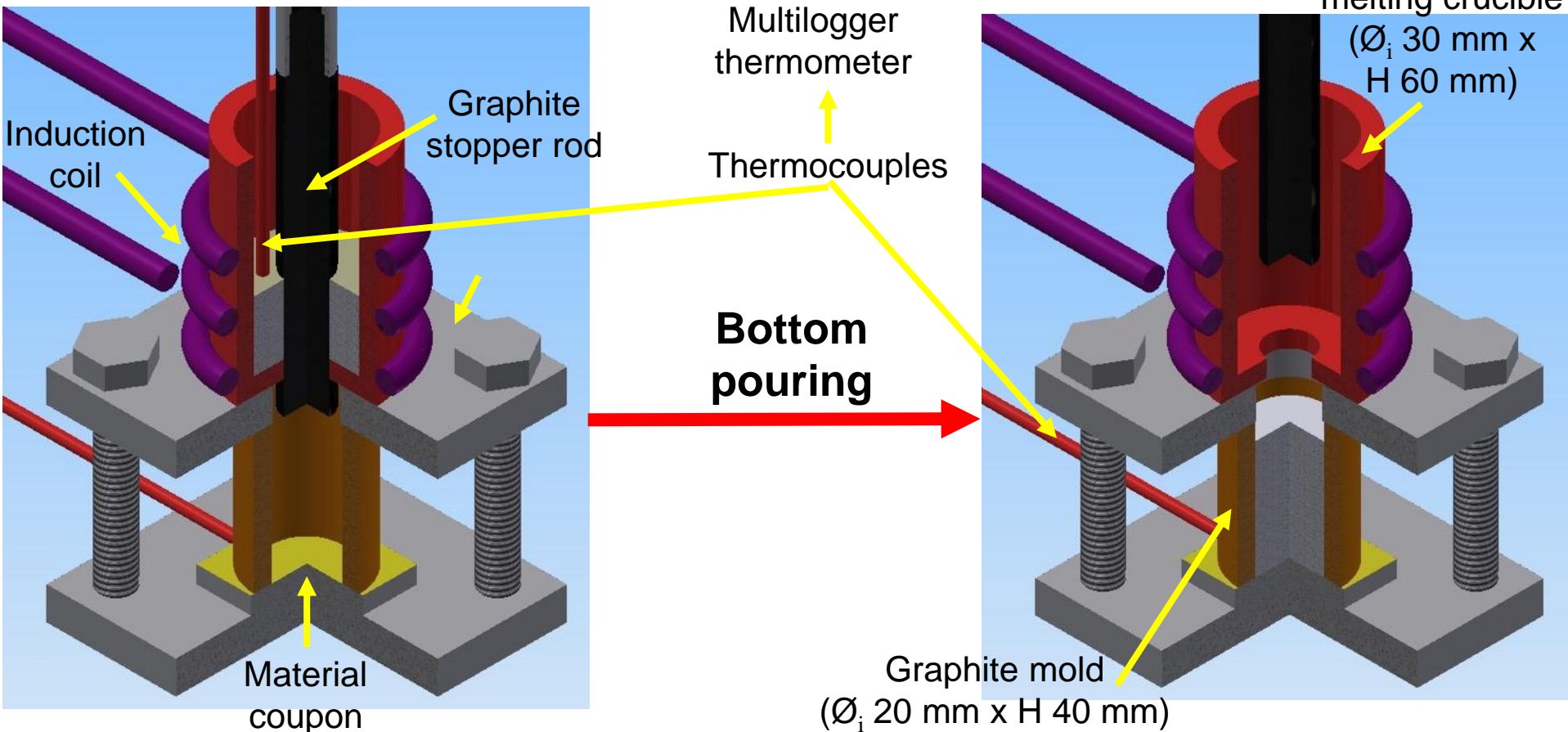


- Carbon powder was observed between solidified aluminum and steel substrate
- Most likely originated from walls of graphite crucibles
- Fell onto upper surface of steel substrate during heating
- Prevented contact between molten aluminum and substrate



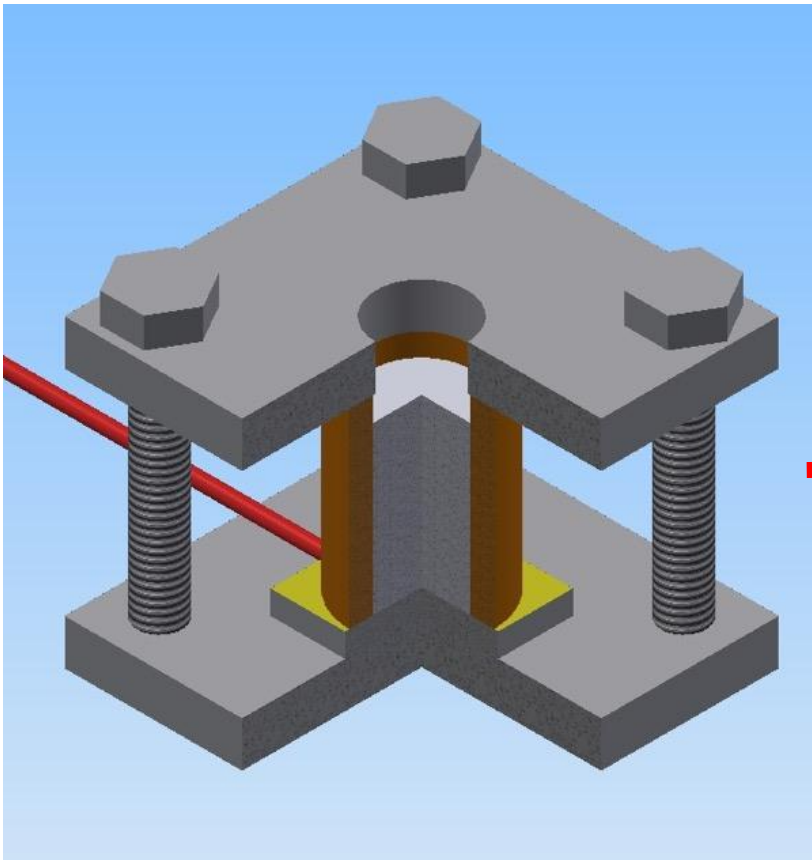
# Task 1: Improved Adhesion Test

- Use induction melting
- Rapid heating to melt aluminum (~10 minutes)
  - Less oxidation and disintegration of crucible walls



# Modified Test Apparatus

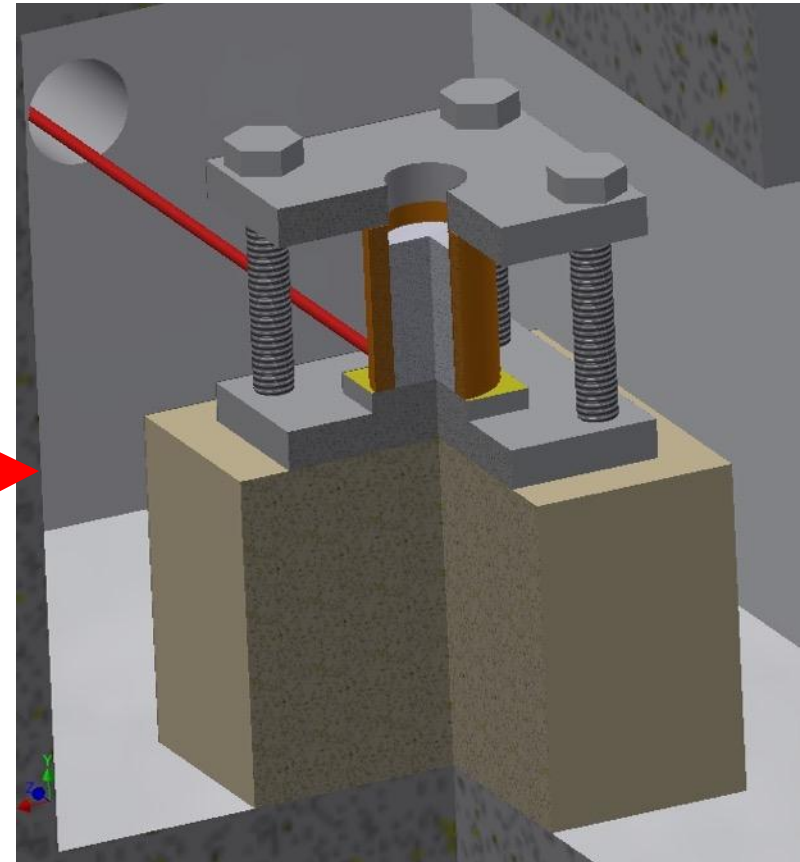
- After aluminum has been poured into lower chamber
- Lower section is placed into resistance furnace pre-heated to 700°C



Resistance  
furnace at  
700 °C



Holding  
time



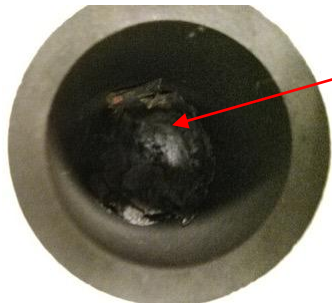


# 1<sup>st</sup> Test Using Induction Melting

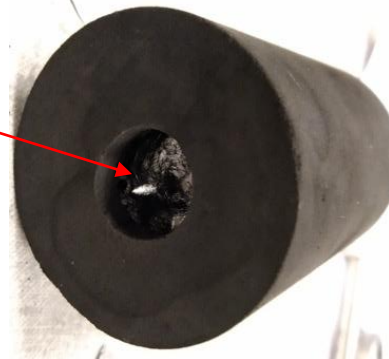
- Melted aluminum in induction coil
- Pulled stopper rod
- Molten aluminum fell onto room temperature substrate and solidified



No carbon layer



Al oxides  
stayed at the  
melting  
crucible



# Planned Initial Experiments

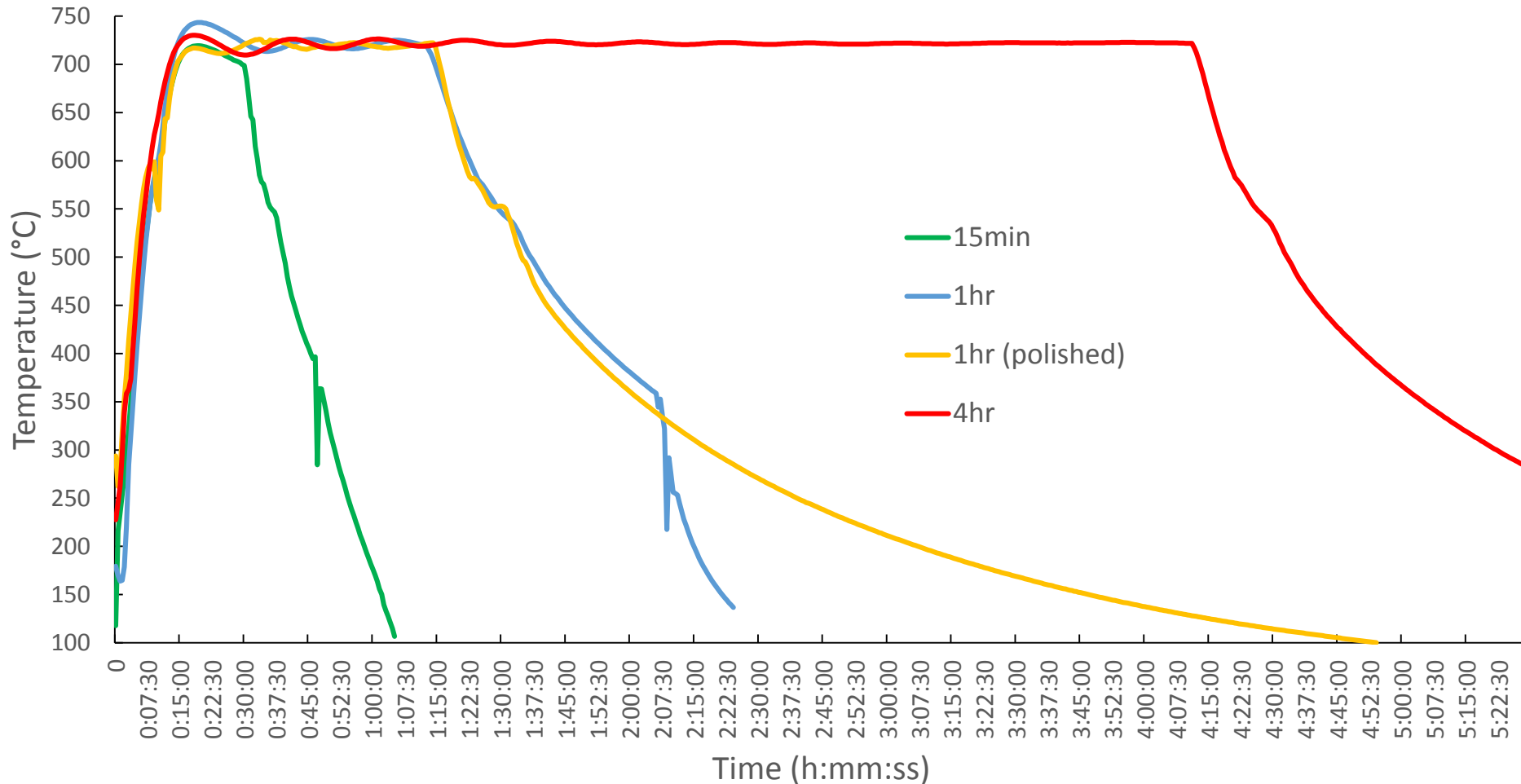


- Planned initial experiments
  - 700 °C; 3 different holding time
    - 15mins, 1 hr, 4 hrs
  - Uncoated H13 steel substrate
    - Ground to 600 mesh SiC finish ←
    - Polished to  $1\mu\text{m}$  ←
  - PVD coatings
    - ZrN

# Temperature Profiles

- Same average behavior in temperature profile for H13 steel substrate after bottom pouring and placed at 700 °C pre-heated resistance furnace

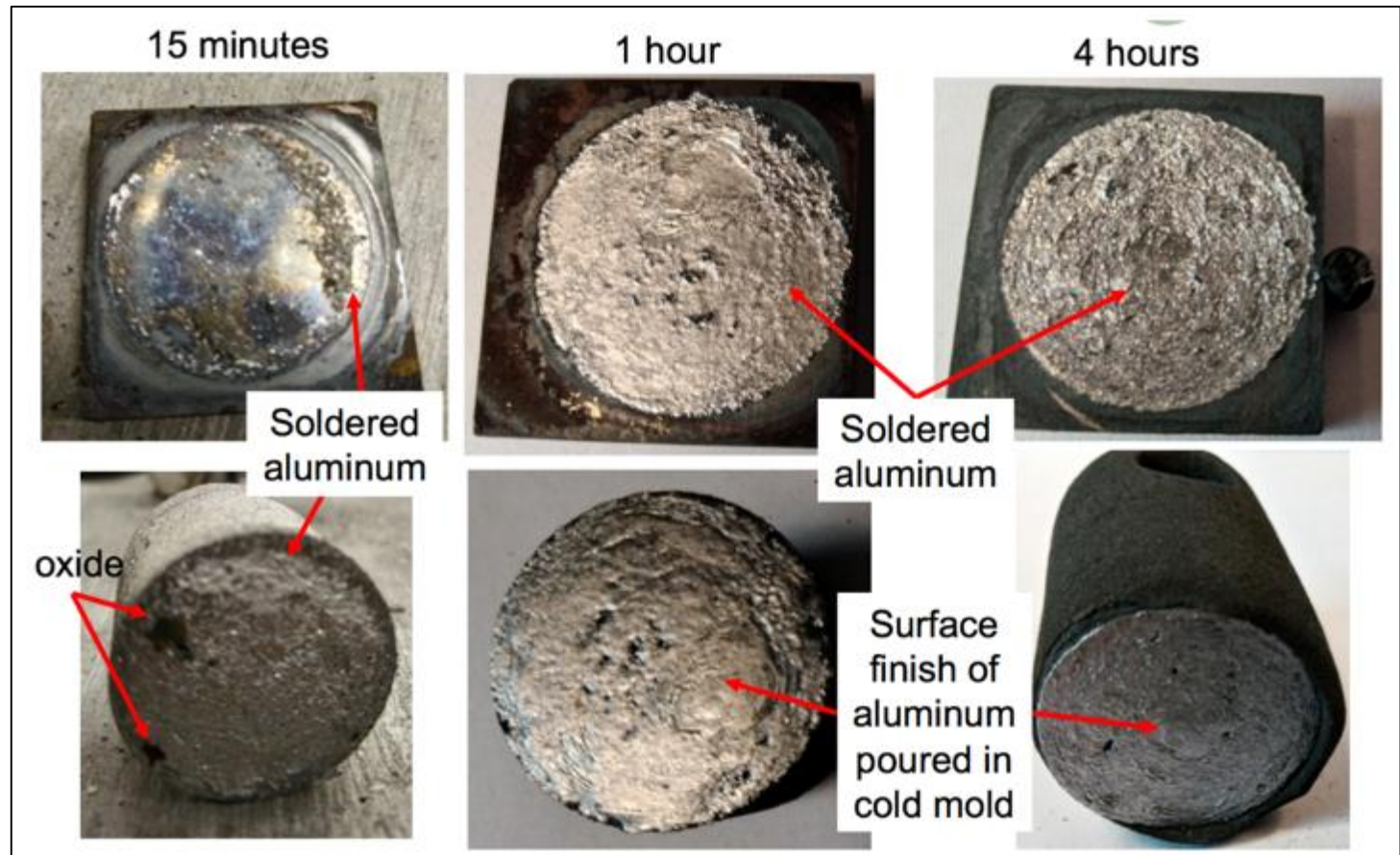
— ~13 minutes to reach 700 °C



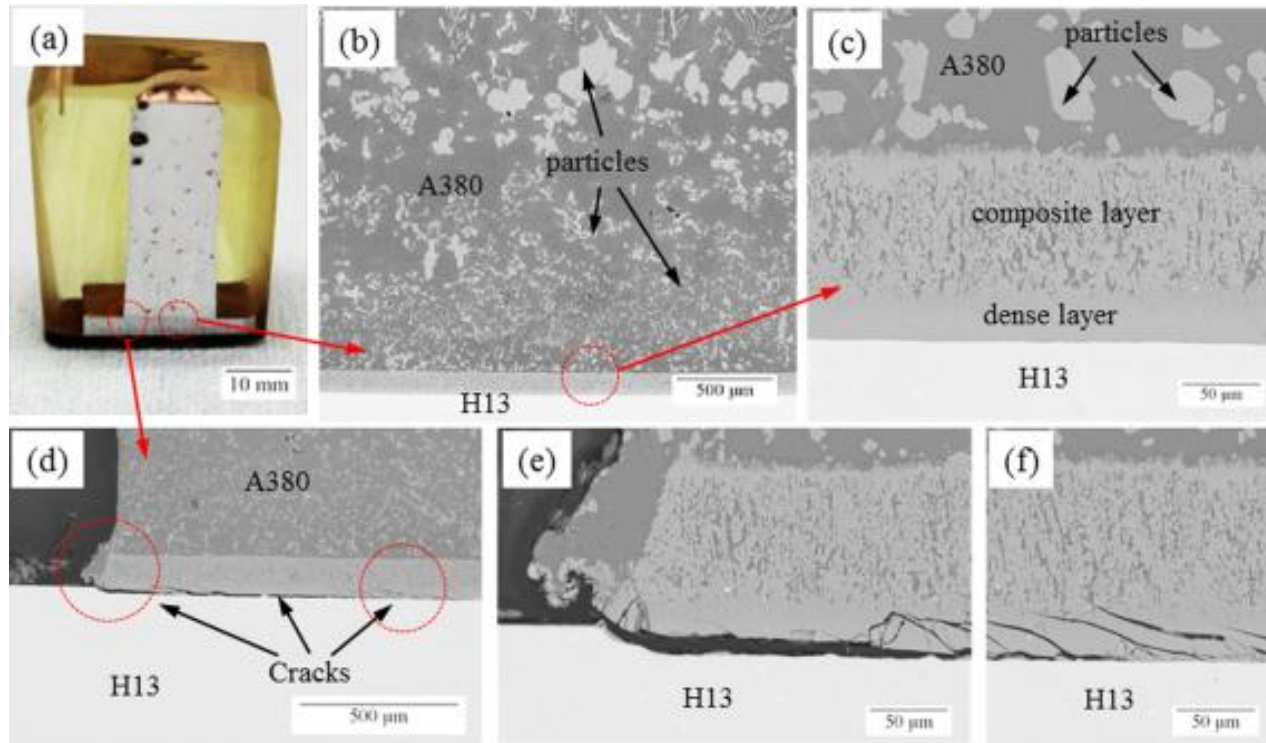


# Bare H13 (ground 600 mesh)

- Reaction occurred between molten aluminum & H13 steel substrate
  - Area of reaction was only small after 15 minutes
- Aluminum separated from steel during cooling to room temperature



# Al + Bare H13 Substrate: Results from Bo Wang



- Bo Wang saw a similar phenomena
  - Cracking between the solidified aluminum and bare H13 substrate

# Wang's Aluminum Adhesion Test Results



#	Material	Supplier	Method & Treatment	Composition	Thickness [μm]	Breaking Strength [MPa]
1	AlCrN	1	CAE	Al <sub>0.67</sub> Cr <sub>0.33</sub> N <sub>x</sub>	1.7	0
2	AlTiN	2	CAE	Al <sub>0.68</sub> Ti <sub>0.32</sub> N <sub>x</sub>	1.5	0
3	CrWN	2	Nitriding + CAE	Cr <sub>0.97</sub> W <sub>0.03</sub> N <sub>x</sub>	6.7	0
4	AlTiN	3	CAE	Al <sub>0.62</sub> Ti <sub>0.38</sub> N <sub>x</sub>	3.3	0*
12a	AlCrN	5	Nitriding + CAE	—	—	0*
5	TiAlN	3	CAE	Ti <sub>0.56</sub> Al <sub>0.44</sub> N <sub>x</sub>	1.8	0.01
12b	AlCrN	5	CAE	—	—	0.04
6	CrN	4	CAE + Fine Polish	CrN <sub>x</sub>	4.4	0.07
7	H13	—	—	—	—	0.12
8	Cr	CSM	MS	Cr	2.2	0.12
9	CrWN	4	CAE + Fine Polish	Cr <sub>0.95</sub> W <sub>0.05</sub> N <sub>x</sub>	4.2	0.26
10	CrN	5	Filtered CAE	CrN <sub>x</sub>	5.0	0.78
11	TiN	CSM	MS	TiN <sub>x</sub>	0.6	0.84
12	AlCrN	5	CAE + Fine Polish	Cr <sub>0.54</sub> Al <sub>0.46</sub> N <sub>x</sub>	5.1	1.30
13	TiB <sub>2</sub>	6	MS	TiB <sub>x</sub>	1.5	2.54

- H13 did not have the highest breaking strength
  - Possibly due to cracking at interface

Source: B. Wang, Ph.D. thesis, Colorado School of Mines, 2016



# Polished H13 ( $1\mu\text{m}$ diamond)

- Similar reaction occurred between molten aluminum & H13 steel substrate
  - Area of reaction was much larger for 15 minute sample
- Aluminum separated from steel during cooling to room temperature

15 minutes

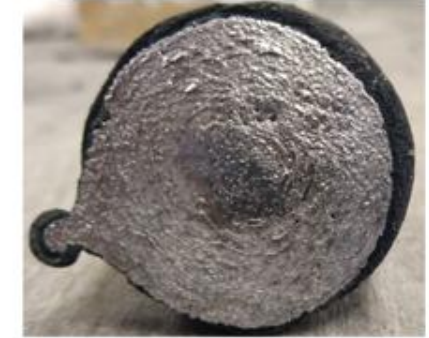
1 hour

4 hours

H13 Steel  
substrates

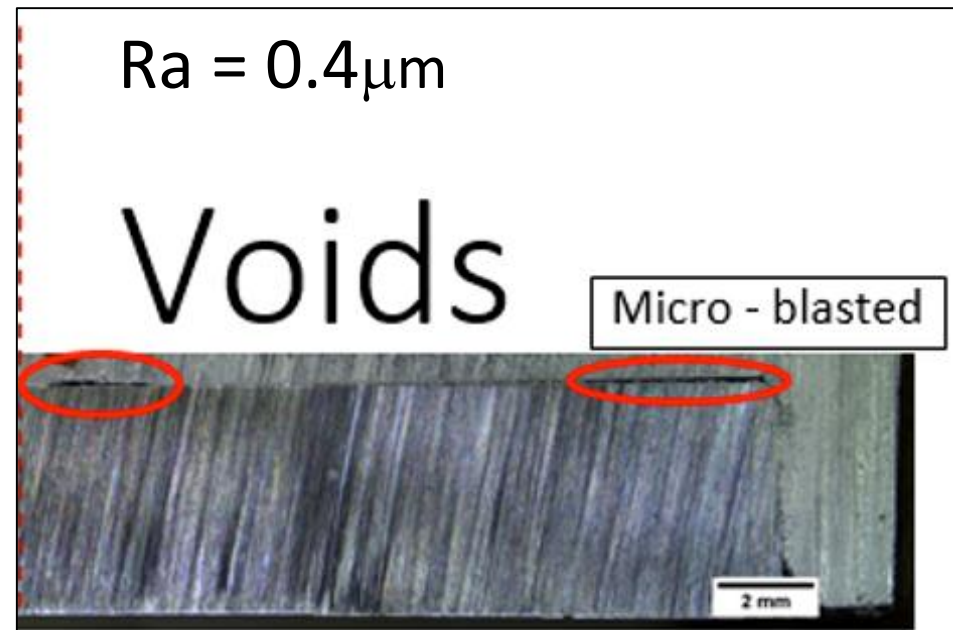
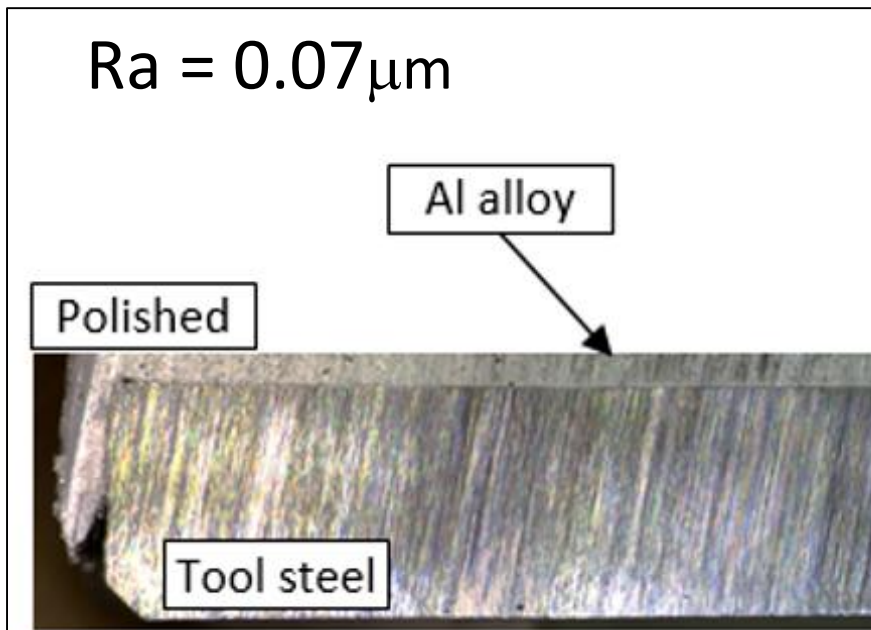


Solidified Al  
cylinders



# Influence of Surface Finish: Published Data

- Testing performed by Gobber et al. in Italy
  - Examined impact of surface roughness on adhesion of molten Al to H13 steel
  - Rougher H13 substrate resulted in less contact between solidified aluminum and steel
- Similar to our results
  - We saw less adhesion/reaction after 15 minutes for the rougher sample



# Task 2: Adhesion Mechanism

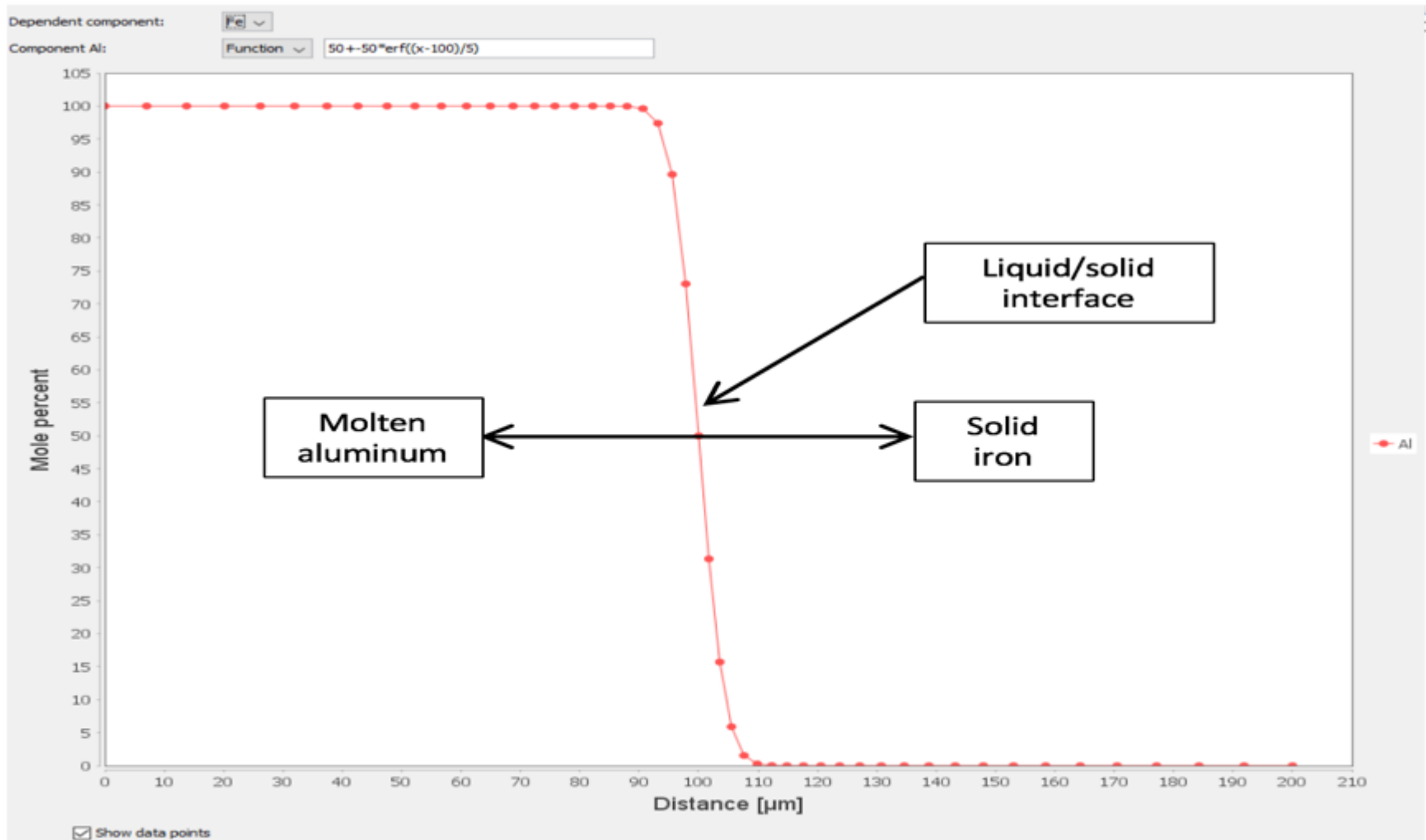


- Understand the inter-diffusion behavior between molten aluminum and steel
- Simulation packages can provide a powerful resource
- CALPHAD method
  - Using DICTRA module of Thermo-Calc
- Initially evaluated a simplified diffusion-couple model
  - Pure Al in contact with pure Fe
  - Held at 680°C for different times



# DICTRA Simulation

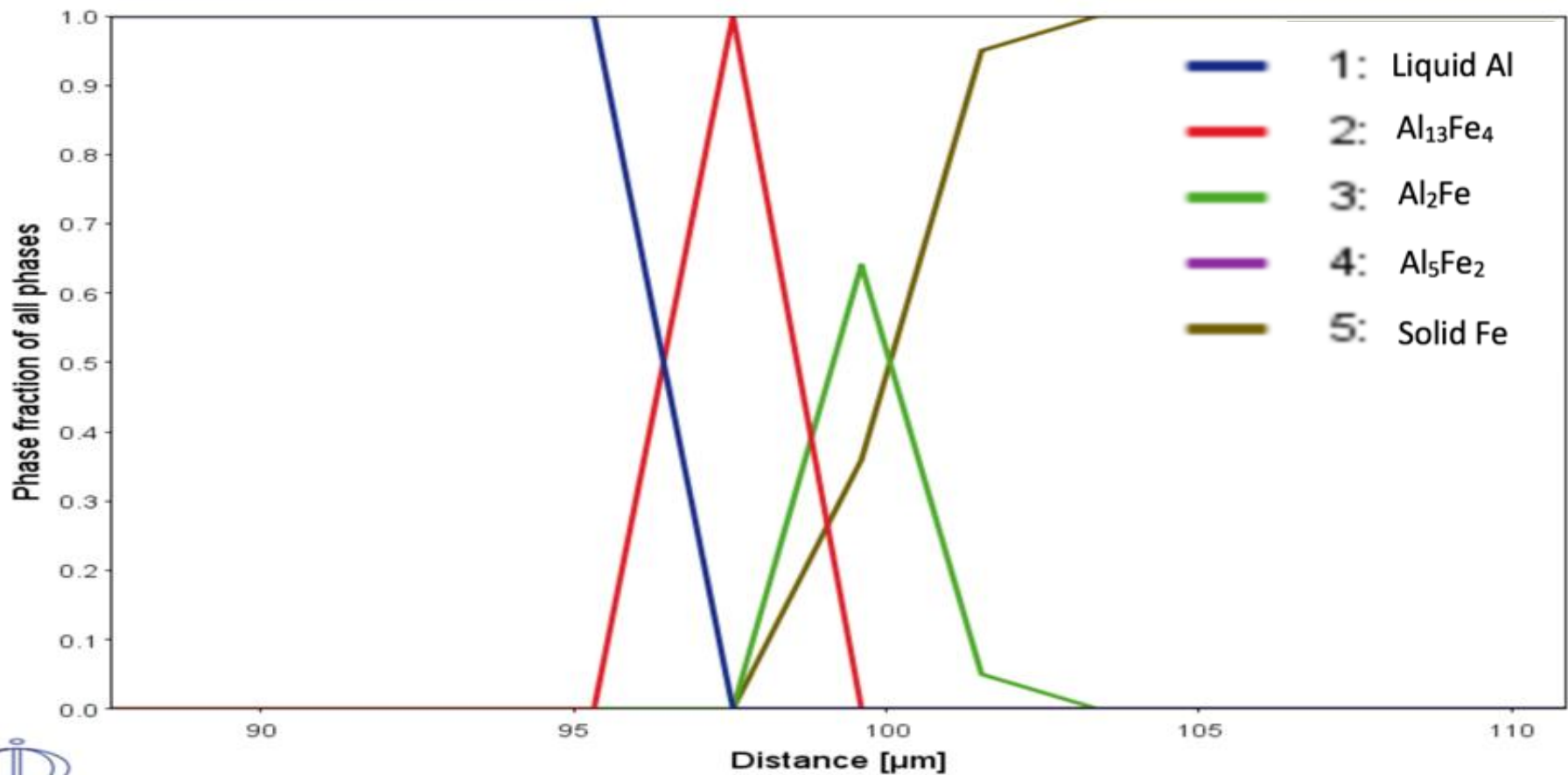
- Starting condition



# 20 seconds at 680 °C

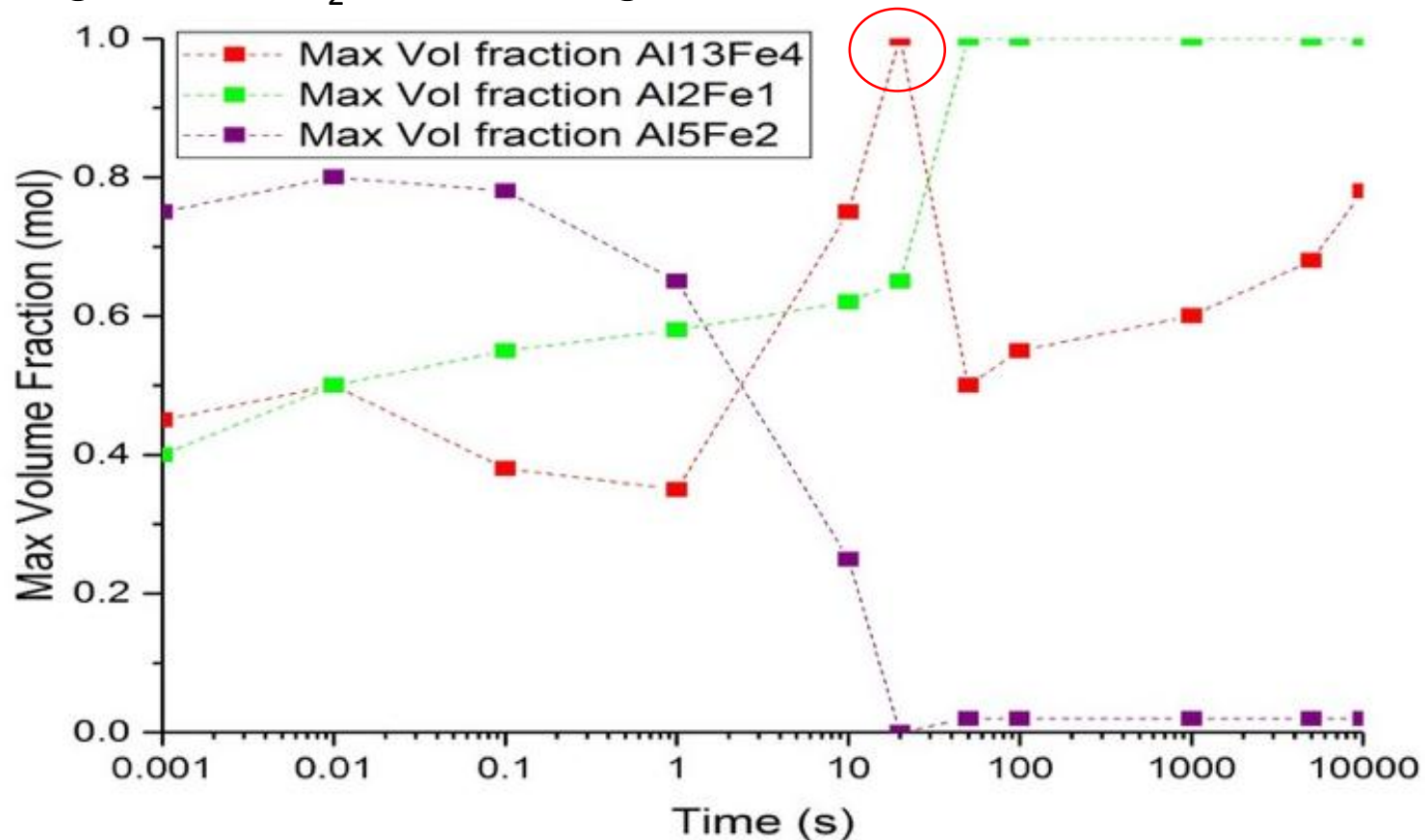
- Shows volume fraction of three phases formed at interface between liquid aluminum and solid iron

–  $\text{Al}_{13}\text{Fe}_4$ ,  $\text{Al}_2\text{Fe}$ , and  $\text{Al}_5\text{Fe}_2$



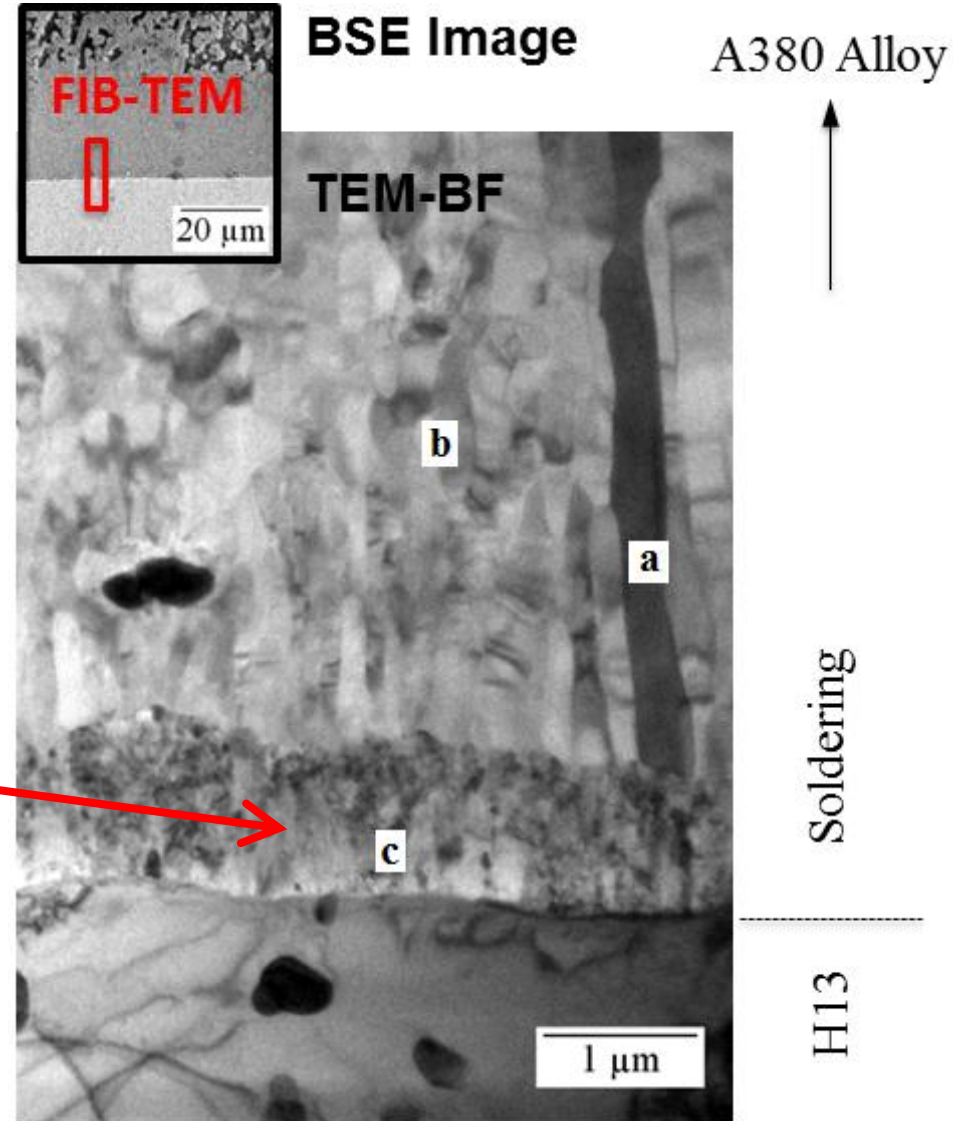
# Volume Fraction

- Shows volume fraction change of each phase with time
  - $\text{Al}_5\text{Fe}_2$  initially forms
  - At about 20 seconds,  $\text{Al}_{13}\text{Fe}_4$  had the highest volume fraction
  - Longer times,  $\text{Al}_2\text{Fe}$  had the highest volume fraction

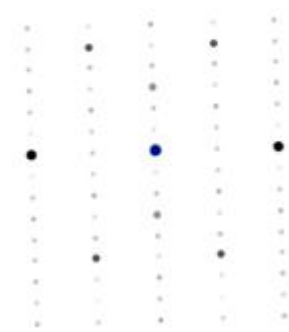
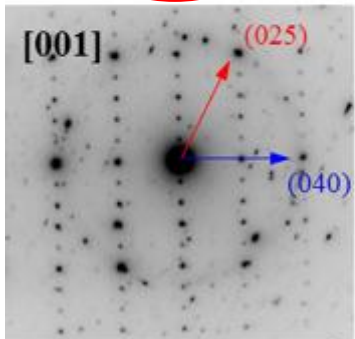


# Bo Wang's results using uncoated H13 steel

- Bo Wang detected  $\text{Al}_{13}\text{Fe}_4$
- Did not detect  $\text{Al}_2\text{Fe}$  or  $\text{Al}_5\text{Fe}_2$
- Need to increase the complexity of the DICTRA simulation



**c**  
 $\text{Al}_{13}\text{Fe}_4$   
 (C2/m)  
 JEMS simulation



# Summary & Conclusions



- Developed a modified adhesion test using induction heating: initial tests
  - 600 mesh ground H13: aluminum soldering occurred, but the interface cracked separating the solidified aluminum and the steel
  - 1  $\mu\text{m}$  polished H13: same results, but more aluminum soldered with the 15 minutes test

# Summary & Conclusions



- Adhesion mechanism: Thermo-Calc simulations
  - Simplified model predicted one of the phases experimentally observed in the project performed by Bo Wang
    - Use DICTRA to predict diffusion profiles
  - Use the Property Model Calculation module to evaluate wetting of coatings by molten aluminum
  - Simulation can be a powerful resource to predict suitable coatings



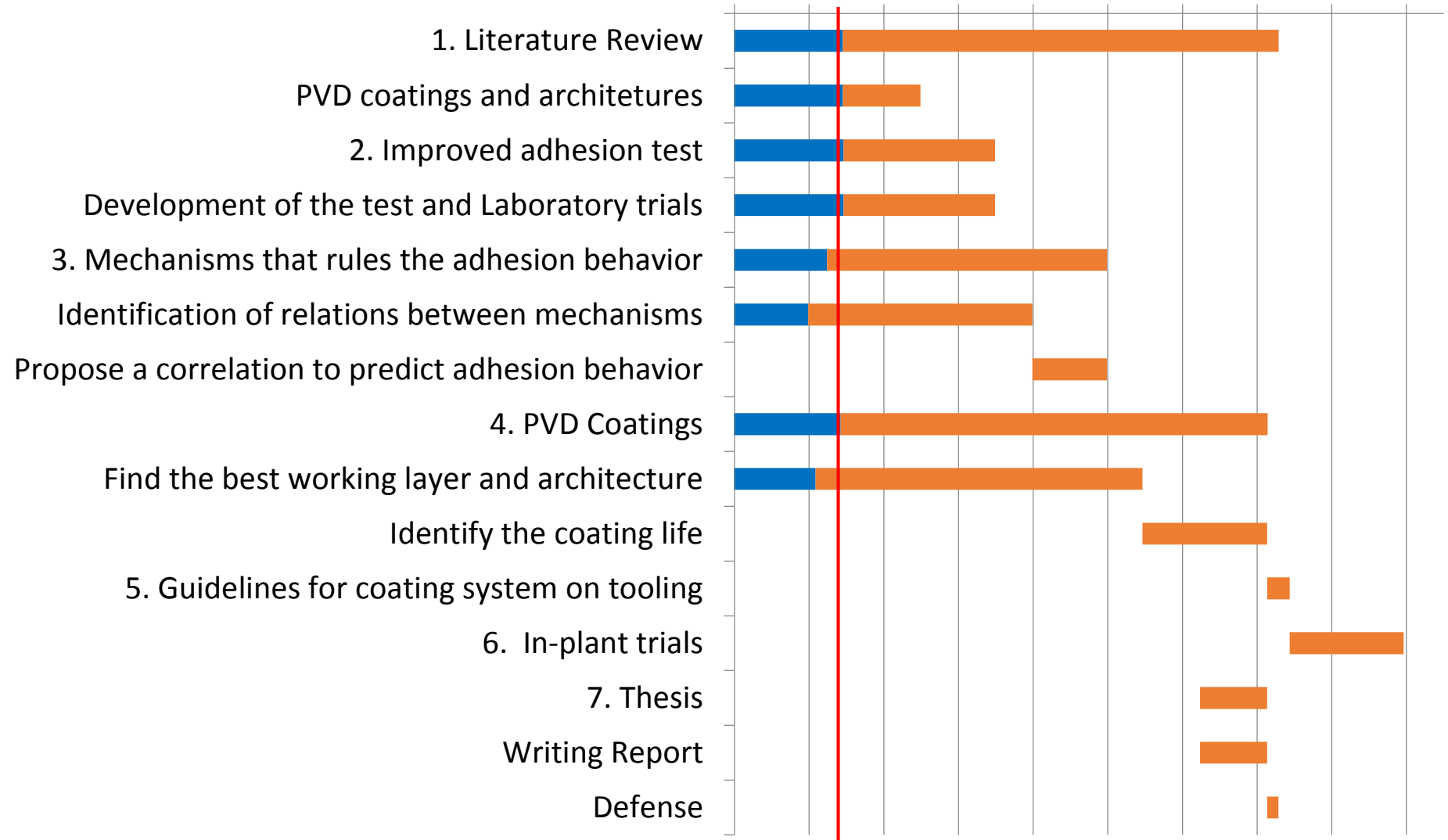
# Future Work



- Literature review
  - PVD coatings currently used by die casters and other industries
  - Chemical interactions between liquid metals and solid materials
  - Wetting of solids by liquid metals
  - Brazing
- Experimental work
  - Uncoated H13 with rougher surface (ground 80 mesh SiC)
  - PVD coated samples: ZrN, carbides
- Characterization
  - Examine the phases formed at the interface between the solidified aluminum and H13 steel substrate

# Progress (Gantt chart)

8/18 2/19 9/19 3/20 10/20 4/21 11/21 6/22 12/22 7/23



# Acknowledgement



- This research is sponsored by the DLA – Troop Support, Philadelphia, PA and the Defense Logistics Agency Information Operations, J62LB, Research & Development, Ft. Belvoir, VA

*Thank you!*

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**Industrial Partners:** *Paul Bracaleon (NADCA)*

**Project Duration:** *Aug. 2018 – July 2023*

#### Achievement

- Identify PVD coatings to be applied to die casting dies to avoid the molten aluminum soldering and understand the adhesion mechanisms involved.

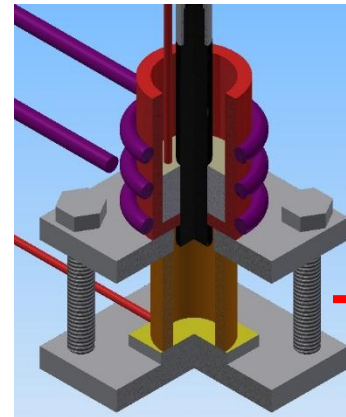
#### Significance and Impact

- Increase die casting parts quality, eliminate the use of lubricants, extend the dies life and reduce cost-per-parts.

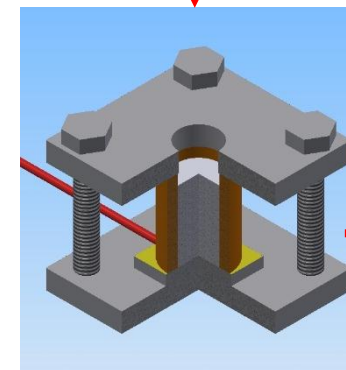
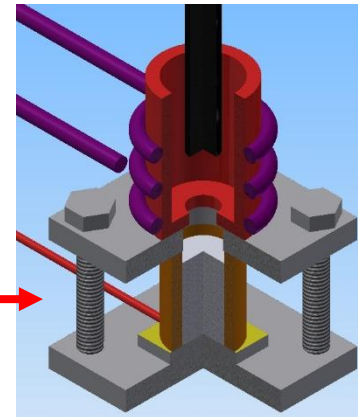
#### Research Details

- Development of an advanced laboratory test to simulate the aluminum die cast process in order to find the best PVD coatings and understand the adhesion mechanisms involved.

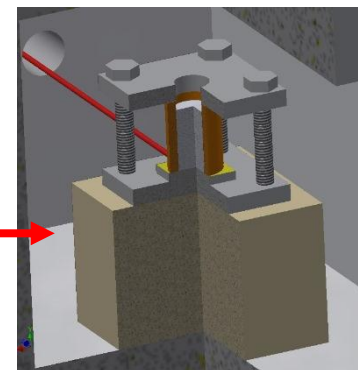
Induction Melting



Bottom Pouring



Place in a  
furnace



Holding time  
at 700 °C

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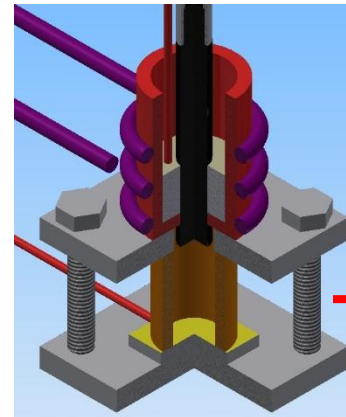
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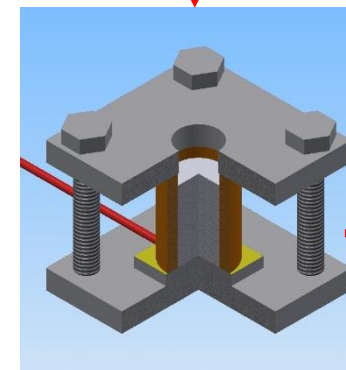
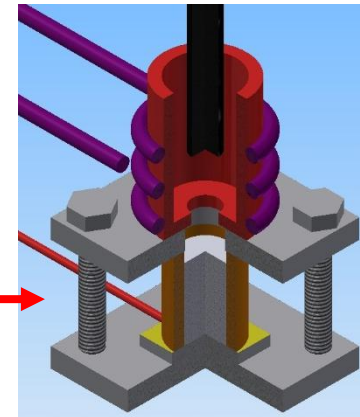
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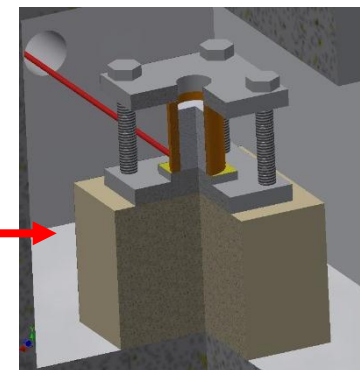
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## Program Goal

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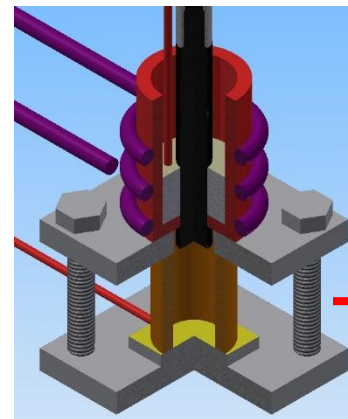
## Approach

- Develop an advanced laboratory test to simulate the aluminum die cast process in order to find the best PVD coatings and understand the adhesion mechanisms involved.

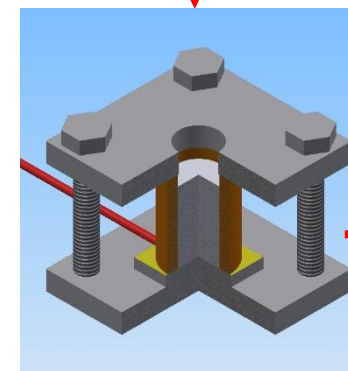
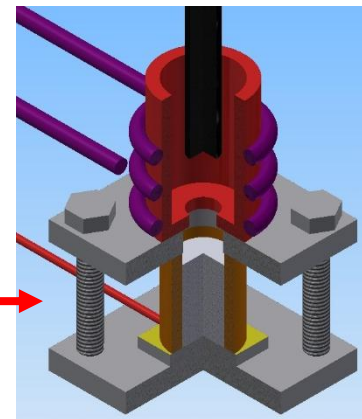
## Benefits

- Increase die casting parts quality, eliminate the use of lubricants, extend the dies life and reduce cost-per-parts.

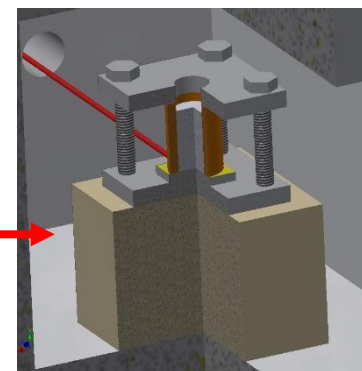
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Bottom Pouring



Place in a furnace



Holding time at 700 °C