

Project 14: Characterization of Regions in Ti-6Al-4V Forgings with Diminished Ultrasonic Inspectability

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Industrial Mentor: Tony Yao (Weber Metals)

Project 14: Characterization of Regions in Ti-6Al-4V Forgings with Diminished Ultrasonic Inspectability



- Student: Connor Campbell (Mines)
- Advisors: Terry Lowe and Kester Clarke (Mines)

Project Duration
MS: January 2016 to May 2019

- **Problem:** Regions of microstructural heterogeneity cause high ultrasonic noise in alpha/beta Ti alloys and limit inspectability via nondestructive methods.
- **Objective:** Extend understanding of how microstructural heterogeneity evolves during forging; characterize and quantify deformed samples, correlate to ultrasonic scattering.
- **Benefit:** Observations of features that increase noise may provide insight into how to optimize processes for homogeneity.

- Recent Progress**
- Microstructural characterization of forged ($\alpha+\beta$) Ti
 - Data Analysis
 - Thesis Writing

| Metrics | | |
|--|------------|--------|
| Description | % Complete | Status |
| 1. Survey of current knowledge | 95% | ● |
| 2. Extraction of regions of low ultrasonic quality | 100% | ● |
| 3. Sample preparation and characterization of regions of high ultrasonic quality | 90% | ● |
| 4. Characterization of regions of low ultrasonic quality | 80% | ● |
| 5. Quantification of microstructures and data analysis | 20% | ● |

Presentation Outline



- Industrial relevance
- Background information
 - Ultrasonic testing of ($\alpha+\beta$) titanium alloys
- Current progress
 - Characterization of regions with high ultrasonic noise
- Future work
 - Characterization of regions with low ultrasonic noise for comparison
 - Quantification of microstructures and data analysis
 - Thesis writing
- Summary

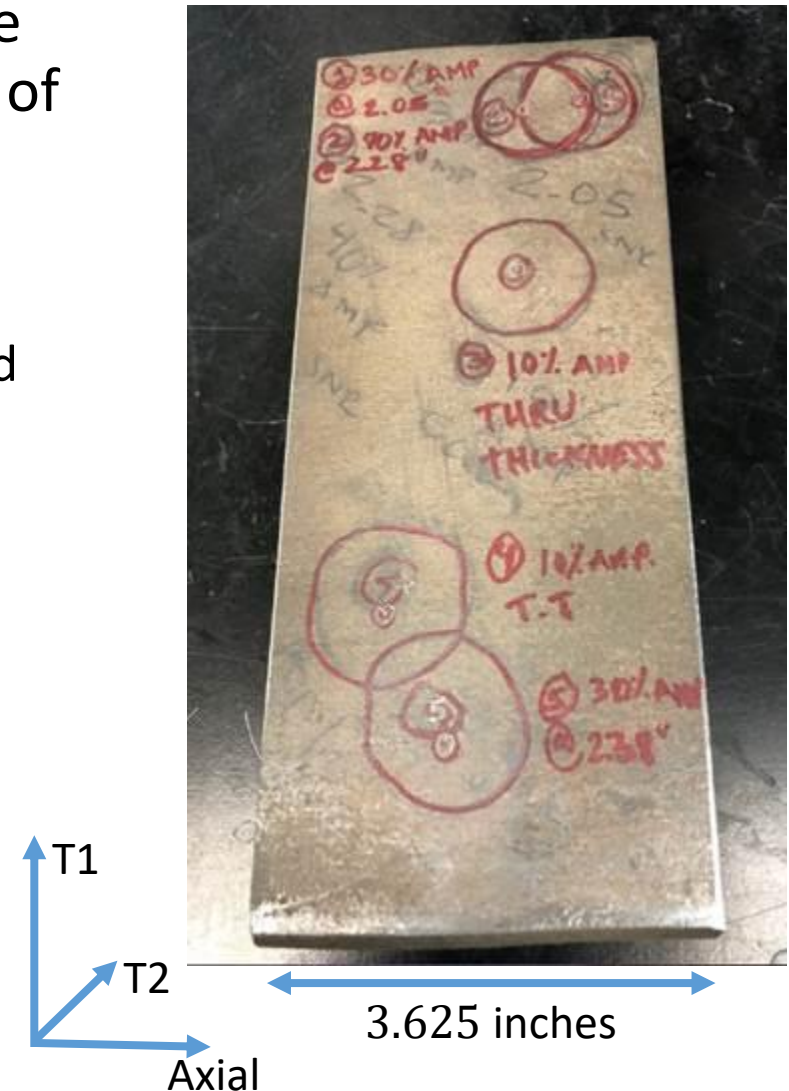
Industrial Relevance



- Ti-6Al-4V is widely used in many industries
- Properties of ($\alpha+\beta$) Ti-alloys can vary greatly
 - Dependent on α morphology and orientation
 - Necessitates rigorous inspection
 - Commonly done via ultrasonic testing (UT)
- Prone to heterogeneous deformation and localized texture during thermomechanical processing (TMP)
 - Scatter ultrasonic signals used for inspection
 - Can cause parts to be rejected (\$\$\$\$)
 - Hard to predict where localized texture will form, and how severe it will be even in simple forgings!

Project Goal

- Investigate microstructure of simple forging (on right), determine origin of features that impeded ultrasonic inspection
 - 5 areas were tested, increased noise observed in three of them at indicated depths
- Extend understanding of microstructural features that contribute to uncertainty in UT of Ti-64 forgings
 - Electron microscopy and orientation mapping via electron backscatter diffraction (EBSD)

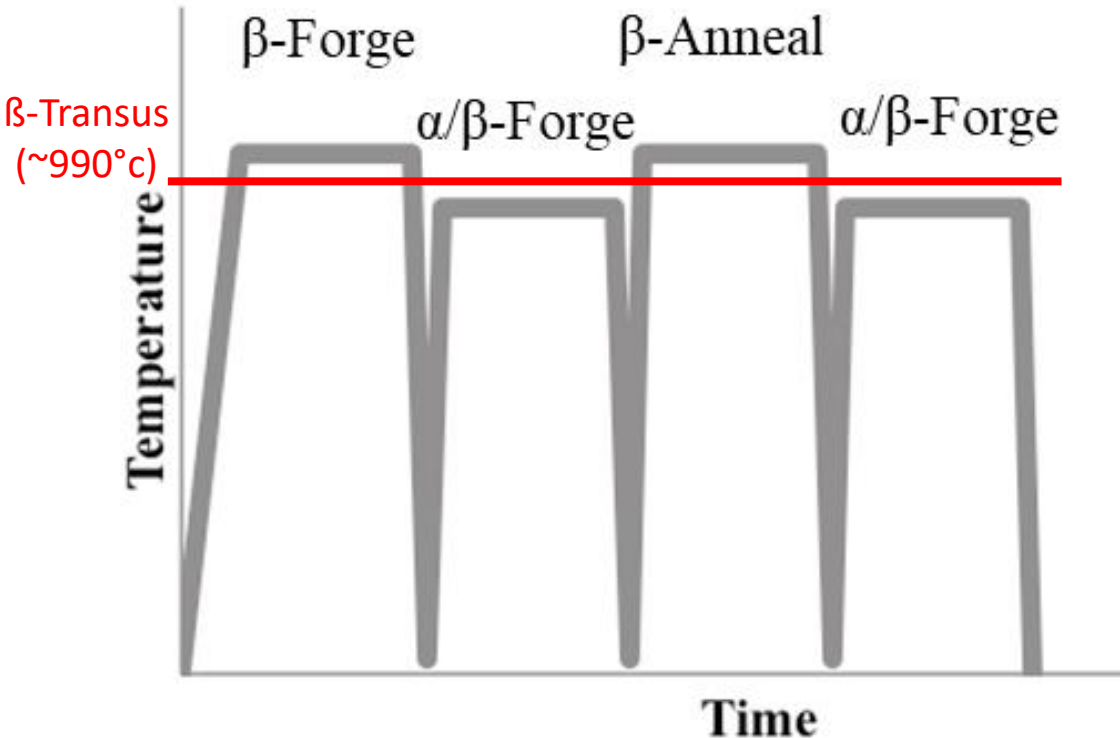


Background Information



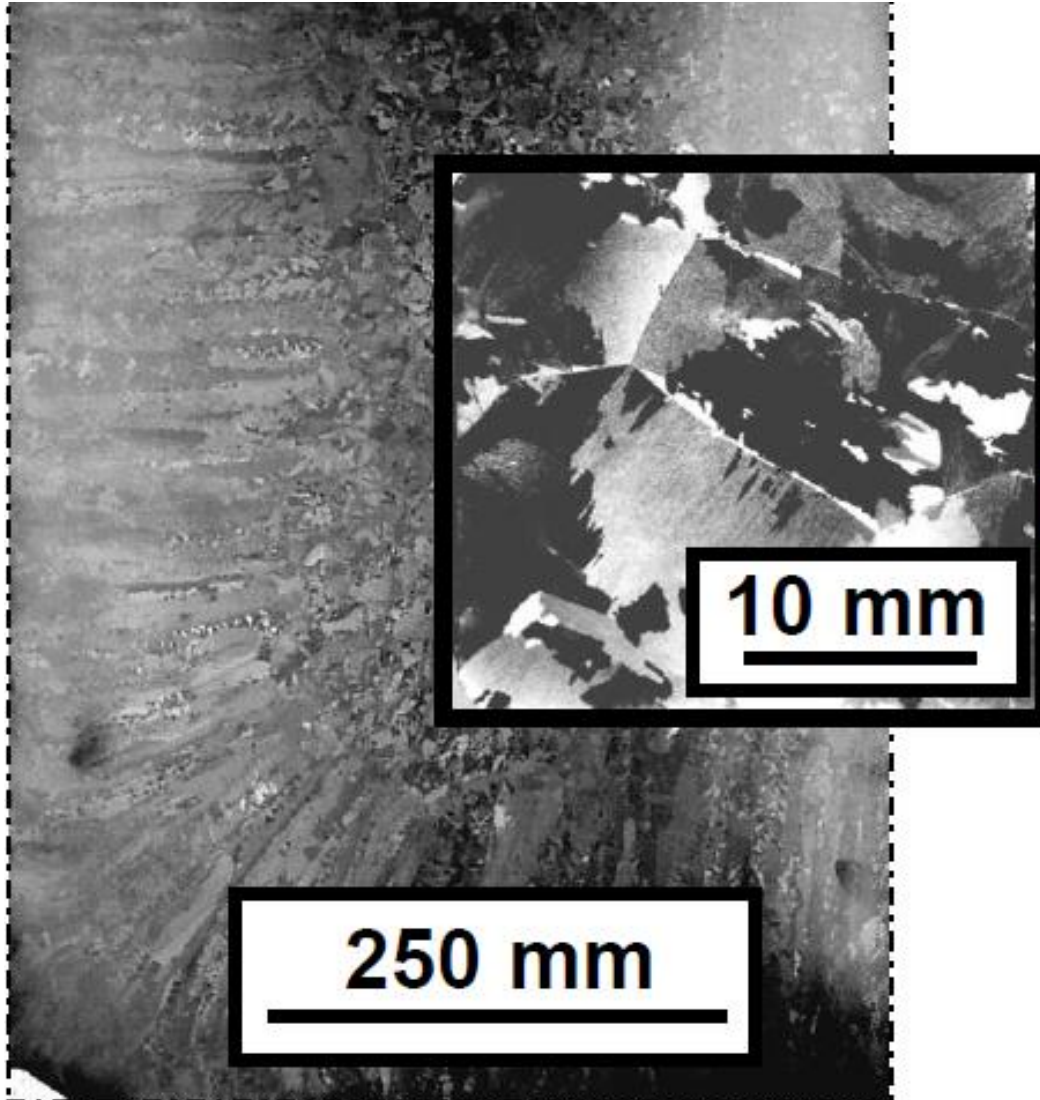
- How are $(\alpha+\beta)$ Ti-forgings typically processed?
- How are forgings ultrasonically inspected?
- What complicates ultrasonic inspection of alpha/beta Ti-alloys?
- What are microstructural aspects that contribute to noise?

Background Information: (α + β) Titanium Alloy Processing



1. β -forging homogenizes as-cast microstructure
2. α + β forging introduces hot work that drives β recrystallization
3. β anneal generates finer β grains, rapid cooling produces fine α colonies that are easily broken up
4. Final α + β work to net-shape creates equiaxed, fine grained α in a matrix of transformed β

Step 0: Ingot Solidification

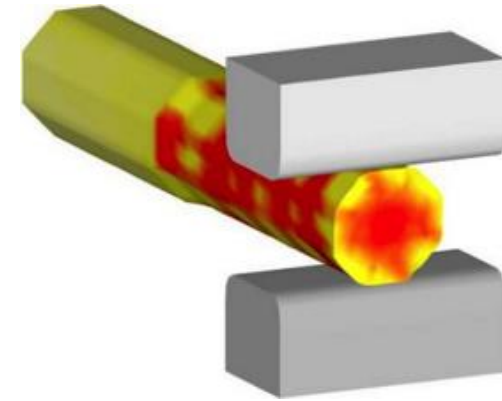


- β -grains solidify, can be equiaxed or columnar
 - Can be ~cms in size
- α colonies grow from β grain boundaries during cooling
 - Will be related to parent β by Burgers orientation relationship:
 $\{110\}_{\beta} // (0001)_{\alpha}$
 $\langle 111 \rangle_{\beta} // [2\bar{1}\bar{1}0]_{\alpha}$
 - 12 possible variants, usually between 3 and 5 will form

Figure Credit: S.L. Semiatin, 2018

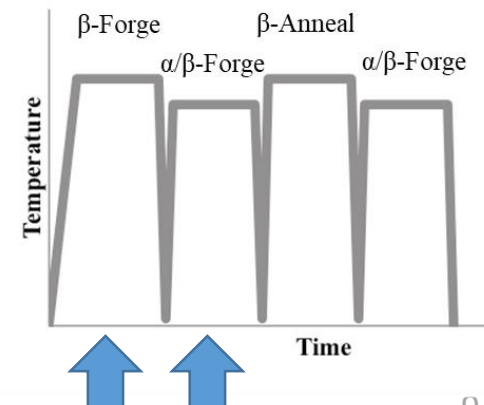
Steps 1+2: β and Initial ($\alpha+\beta$) Hot Working of Ingot

- Ingot is cogged, elongating longitudinal axis
- β -worked initially because β is softer than α
 - $T > 1050^\circ\text{C}$
 - Produces β grains \sim mms in size
- ($\alpha+\beta$) worked to introduce hot work used to fuel recrystallization during β anneal
 - $900^\circ\text{C} < T < 990^\circ\text{C}$
 - α colonies will deform, albeit less than β
 - Strain partitioning b/t phases is hard to predict
 - “Hard” vs. “Soft” oriented α colonies
 - Temperature- and rate-dependence of β



DEFORM-3D simulation
of cogging

<http://wildeanalysis.co.uk/fea/software/deform/deform-3d-suite/deform-cogging>



Step 3: β -Anneal and Quenching

- β grains recrystallize during brief hold above β -transus
 - Grains grow rapidly until ~ 1 - 2 mm
- Rapidly quenched in water
 - Suppresses grain-boundary α
 - Produces fine α colonies that are easily deformed and recrystallized

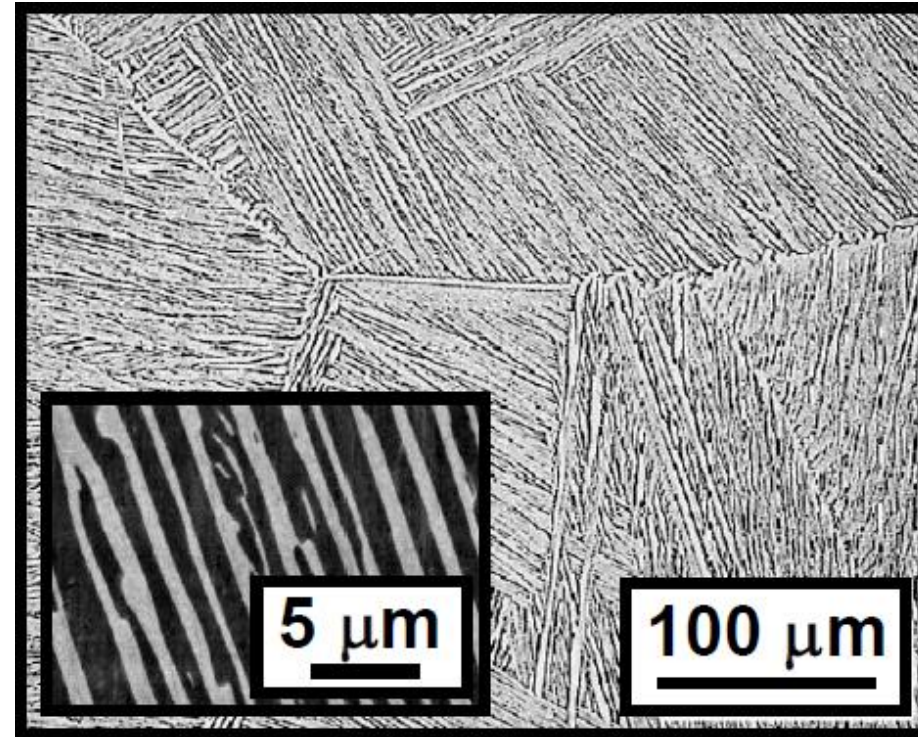
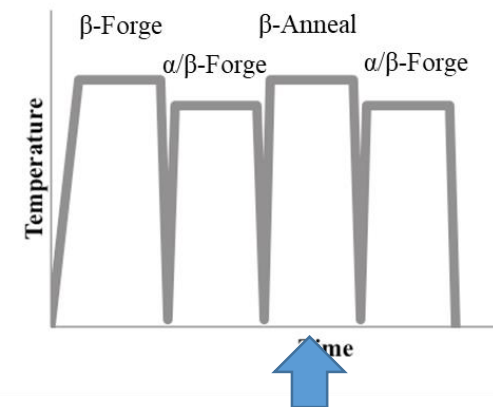


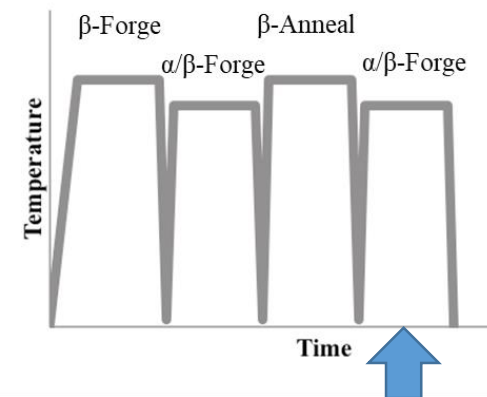
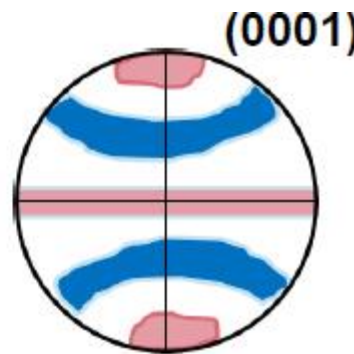
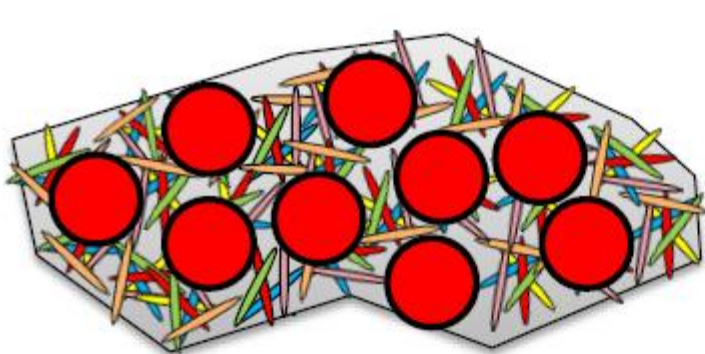
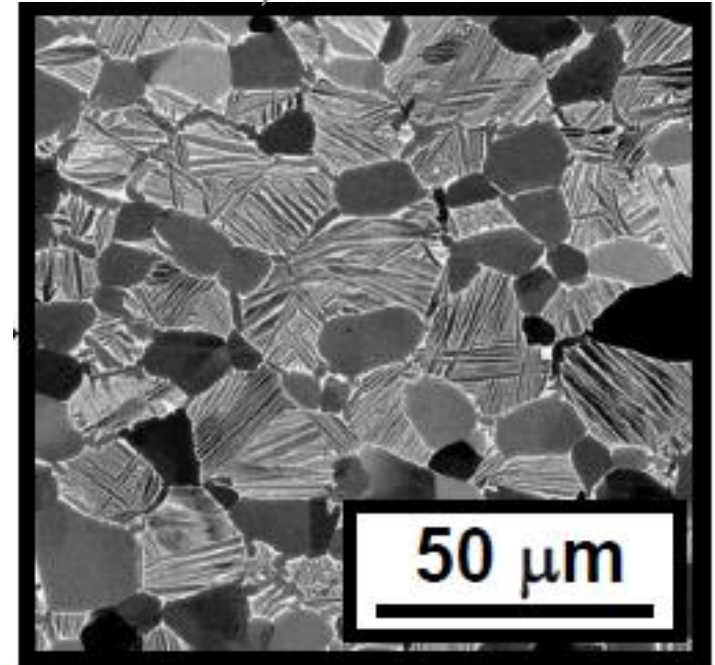
Figure Credit:
S.L. Semiatin, 2018



Step 4: ($\alpha+\beta$) Forging

S.L. Semiatin, 2018

- Produces equiaxed primary α grains in a matrix of transformed β (secondary α platelets and remnant β at boundaries)
 - Average grain size usually $\sim 15\text{-}20\mu\text{m}$ following heat treatment
- Ideal: Any primary α texture is insulated by randomly oriented secondary α \rightarrow homogeneity!
 - ...*ideally*



A. L. Pilchak, 2018

Background Information

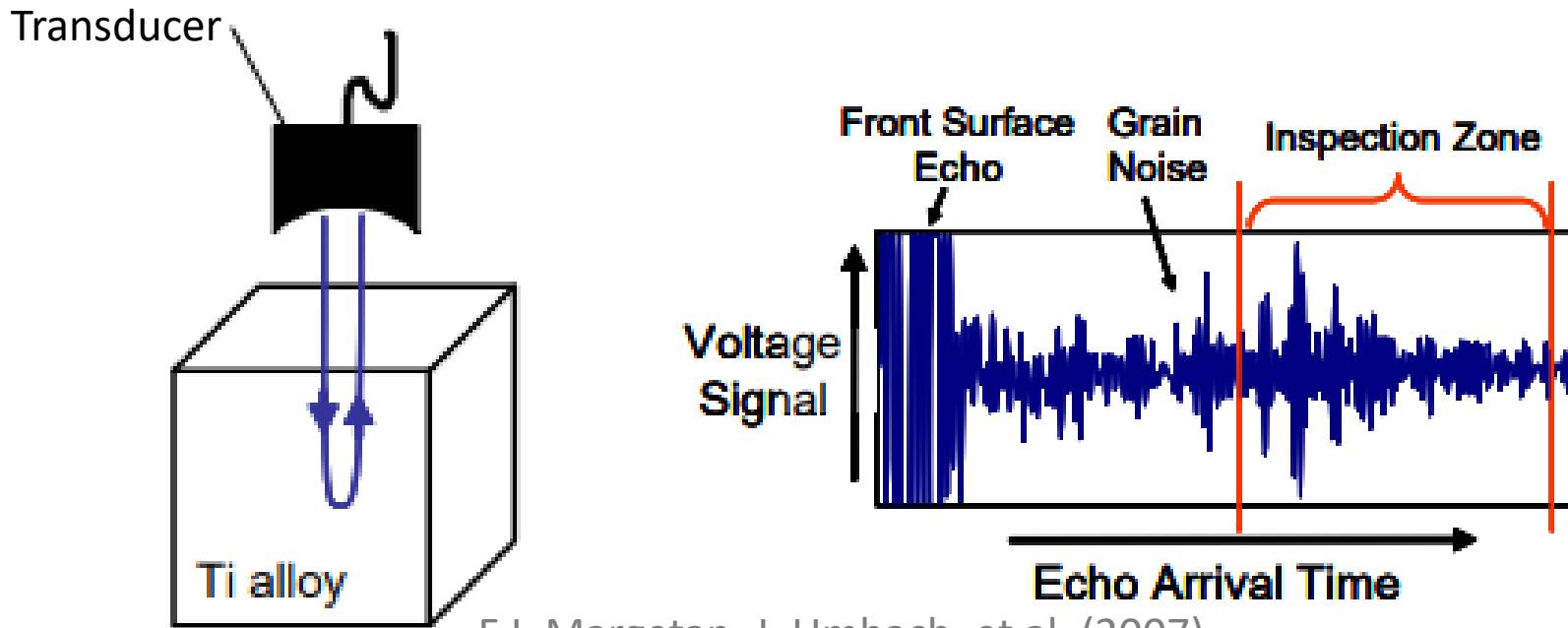


- How are ($\alpha+\beta$) Ti-forgings typically processed?
 - ~4 step process with intent of producing uniform, fine grains
- How are forgings ultrasonically inspected?
- What complicates ultrasonic inspection of alpha/beta Ti-alloys?
- What are microstructural aspects that contribute to noise?

How are Forgings Ultrasonically Inspected?

- “Pulse/Echo” Inspection

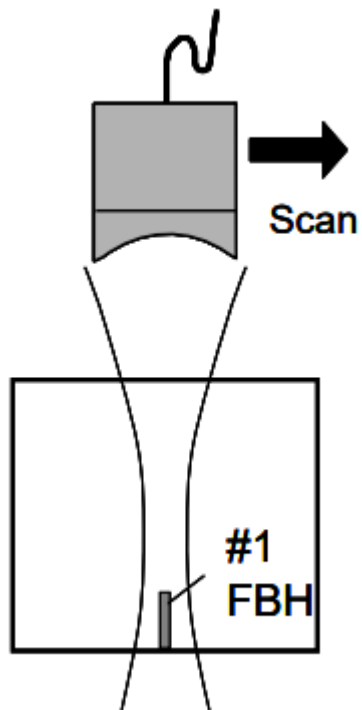
- Immersed transducer supplies an ultrasonic **pulse** into the material
- The **echo** is then recorded as a voltage signal
 - Reflections occur wherever there is a difference in density
- Initially developed to detect cracks, pores, and voids, has been refined to determine more about microstructure



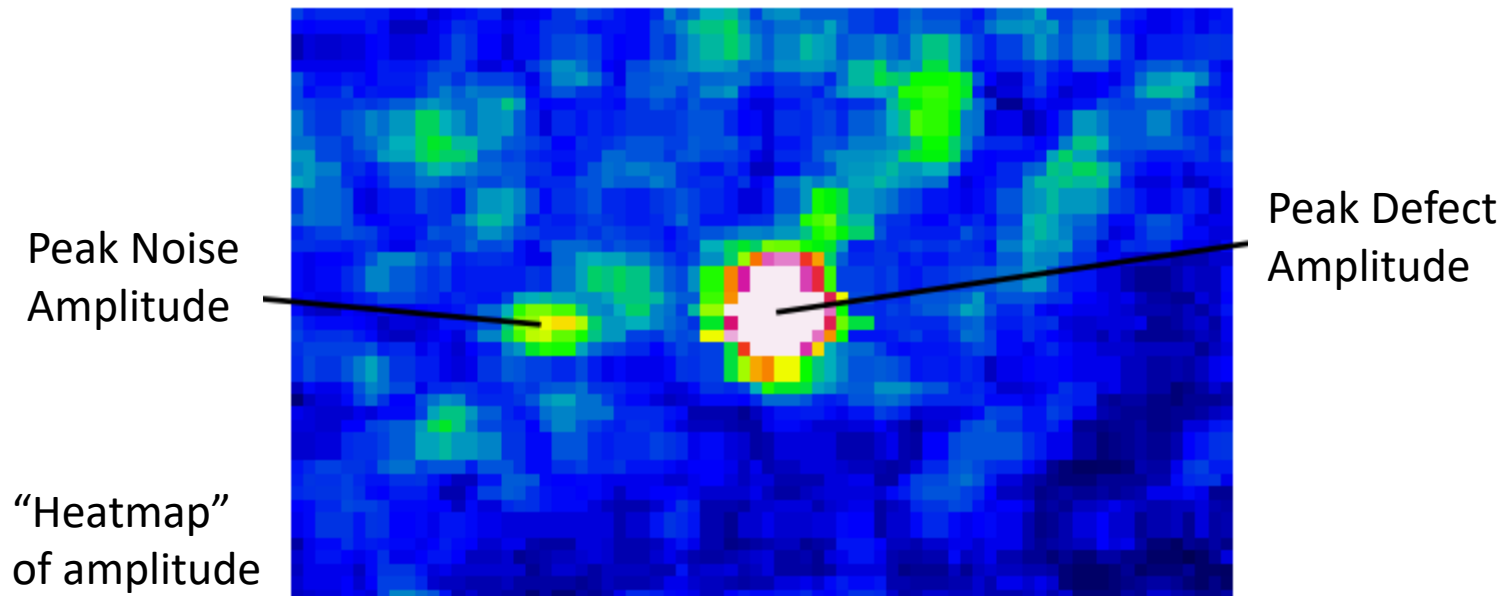
F.J. Margetan, J. Umbach, et al. (2007)

How are Forgings Ultrasonically Inspected? (Cont.)

- Calibrated using a flat-bottom hole (FBH) standard
 - Machined flaw serves as a reflector in a known location to ensure accuracy of measurements
 - Permits calculation of a signal-to-noise ratio (SNR)



$$\frac{S}{N} = \frac{\text{Peak Defect Amplitude}}{\text{Peak Noise Amplitude}}$$



Background Information

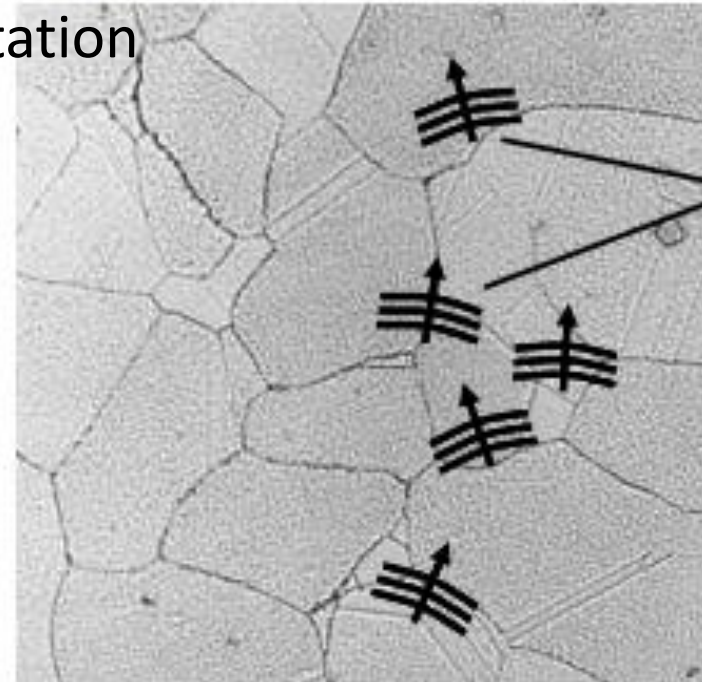


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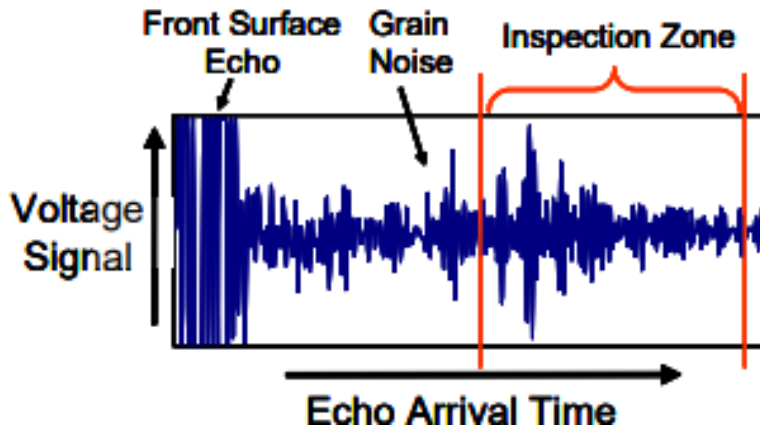
What Complicates Ultrasonic Inspection of Ti-Forgings?

- Complex ultrasound-microstructure interactions
- Difficult-to-interpret readings near surfaces
 - Dents and scratches serve as reflectors
- Reflections at grain boundaries
 - Difference in (c) and (a) plane density and elastic modulus
- Localized preferred crystallographic orientation

Incident Sound Pulse



Schematic of grain boundary scattering



F.J. Margetan, J. Umbach, et al. (2007)

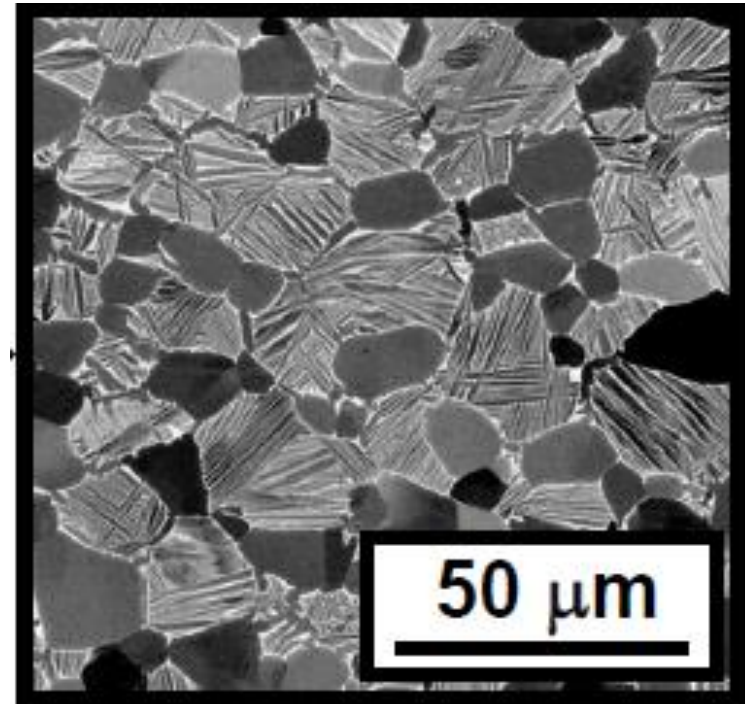
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- What complicates ultrasonic inspection of alpha/beta Ti-alloys?
 - Complex ultrasound-microstructure interactions
 - Surface defects, variations in grain noise, and localized texture
- What are microstructural aspects that contribute to noise?

What Aspects of Microstructure Contribute to Noise?

- Backscattering at grain boundaries due to acoustic mismatch
 - Grain morphology (particularly elongation)
 - Grain orientation (relative to incident beam)
- Wavelength of ultrasonic pulse relative to average grain size
 - If $\lambda > 2\pi D$, “Rayleigh” scattering occurs
 - Improves inspectability
 - If $\lambda < 2\pi D$, “Stochastic” scattering occurs
 - Increases attenuation (energy loss)
- With sufficient attenuation, dangerous defects can appear to be less dangerous



S.L. Semiatin, 2018

Background Information



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 - Complex ultrasound-microstructure interactions
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- What are microstructural aspects that contribute to noise?
 - Grain elongation and preferred orientation
 - Grains that are larger than expected ($>15-20\mu\text{m}$)

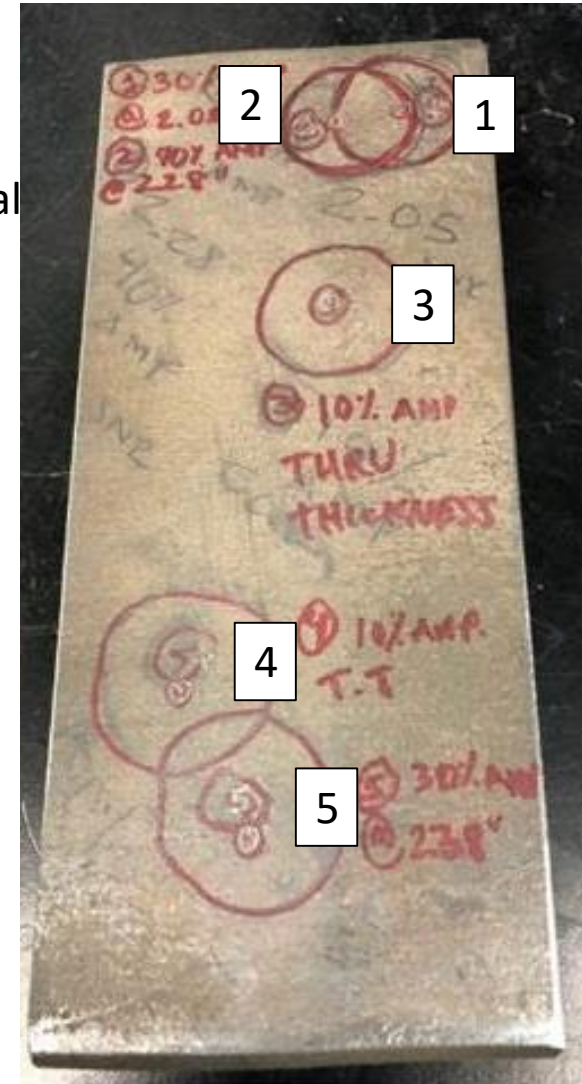
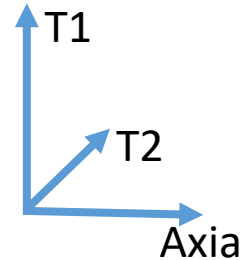
Recent Progress



- Removal of regions of interest via wire EDM
- Bulk texture measurement via x-ray diffraction
- Scanning electron microscopy of samples

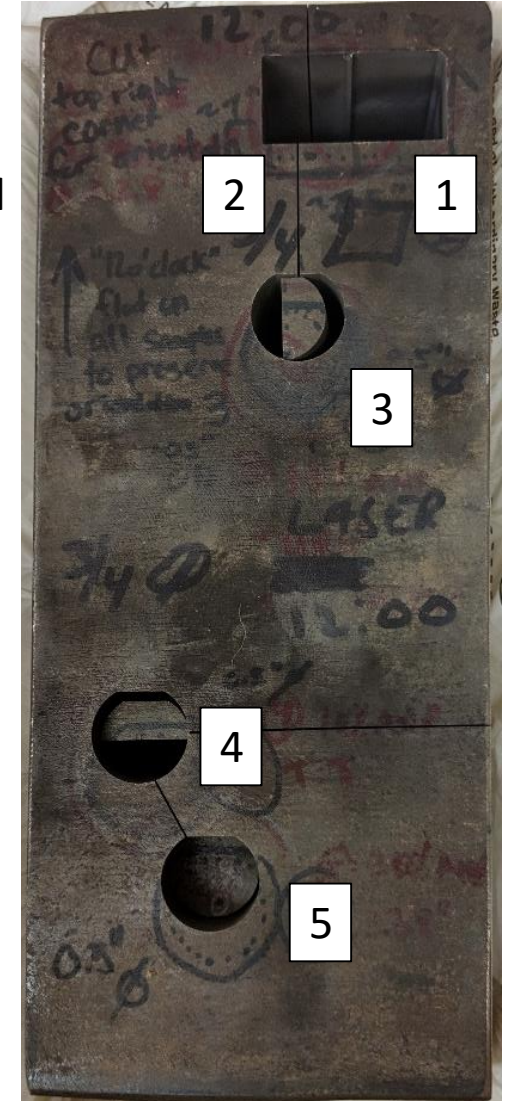
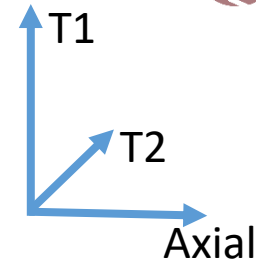
Removal of Regions of Interest

- 5 regions scanned by Weber Metals:
 1. 30% SNR, 2.05" depth
 2. 40% SNR, 2.28" depth
 3. 10% SNR through thickness (control)
 4. 10% SNR through thickness (control)
 5. 30% SNR, 2.38" depth
- Regions were extracted via wire EDM
- 1 and 2 were cut to indicated depths
 - Referred to as “Square 1” and “Square 2,” respectively
- 5 was cut into “coins” parallel to the top surface at depths of 2.23”, 2.38”, and 2.53” for XRD and BSE analysis
 - Referred to as “Coin 1,” “2,” and “3,”



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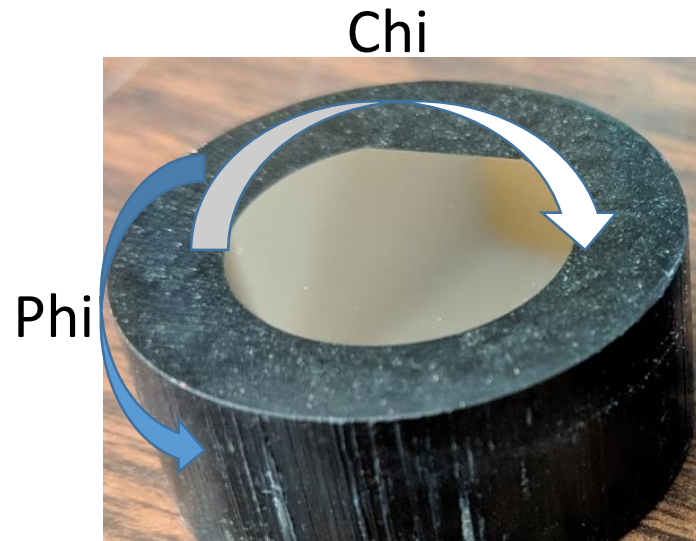
Recent Progress



- Removal of regions of interest via wire EDM
 - Samples were β -forged, β -annealed, and $(\alpha+\beta)$ -forged
 - Were not $(\alpha+\beta)$ annealed
- Bulk texture measurement via x-ray diffraction
- Scanning electron microscopy of samples

Texture Measurements via XRD

- Coin 2 was mounted and polished for XRD analysis
 - Recall that coin 2 was cut @ depth of ultrasonic indication
- Full texture scan was conducted:
 - Scan for Bragg condition for (a), (c), and (a+c) planes ($hkl-\alpha$)
 - Set condition, rotate samples through $\phi = 0^\circ-359^\circ$ and $\chi = 0^\circ-80^\circ$
 - Higher intensity = more planes aligned with that orientation
 - Defocusing and background scans were also performed



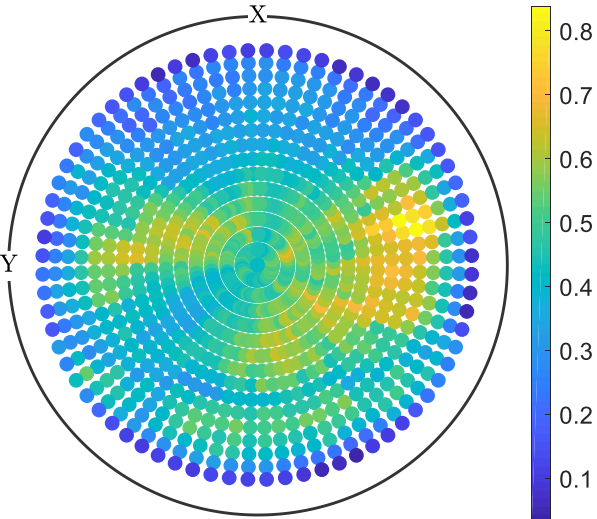
“Coin 2” Bulk Texture XRD

- Pole figure results show evidence of weak texture
 - Max intensity of 1.2x random is weak, expected values of at least 2x
 - Scan area = $\sim 1\text{cm}^2$, not detecting “localized” texture

(C) Planes

(0002)

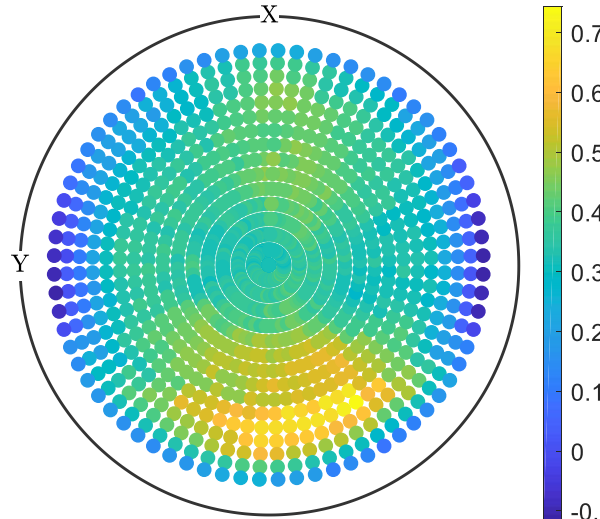
X



(A) Planes

(10 $\bar{1}$ 0)

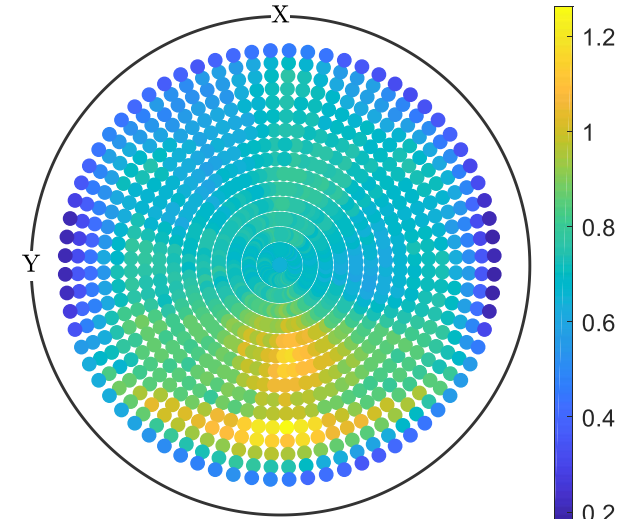
X



(C+A) Planes

(10 $\bar{1}$ 1)

X



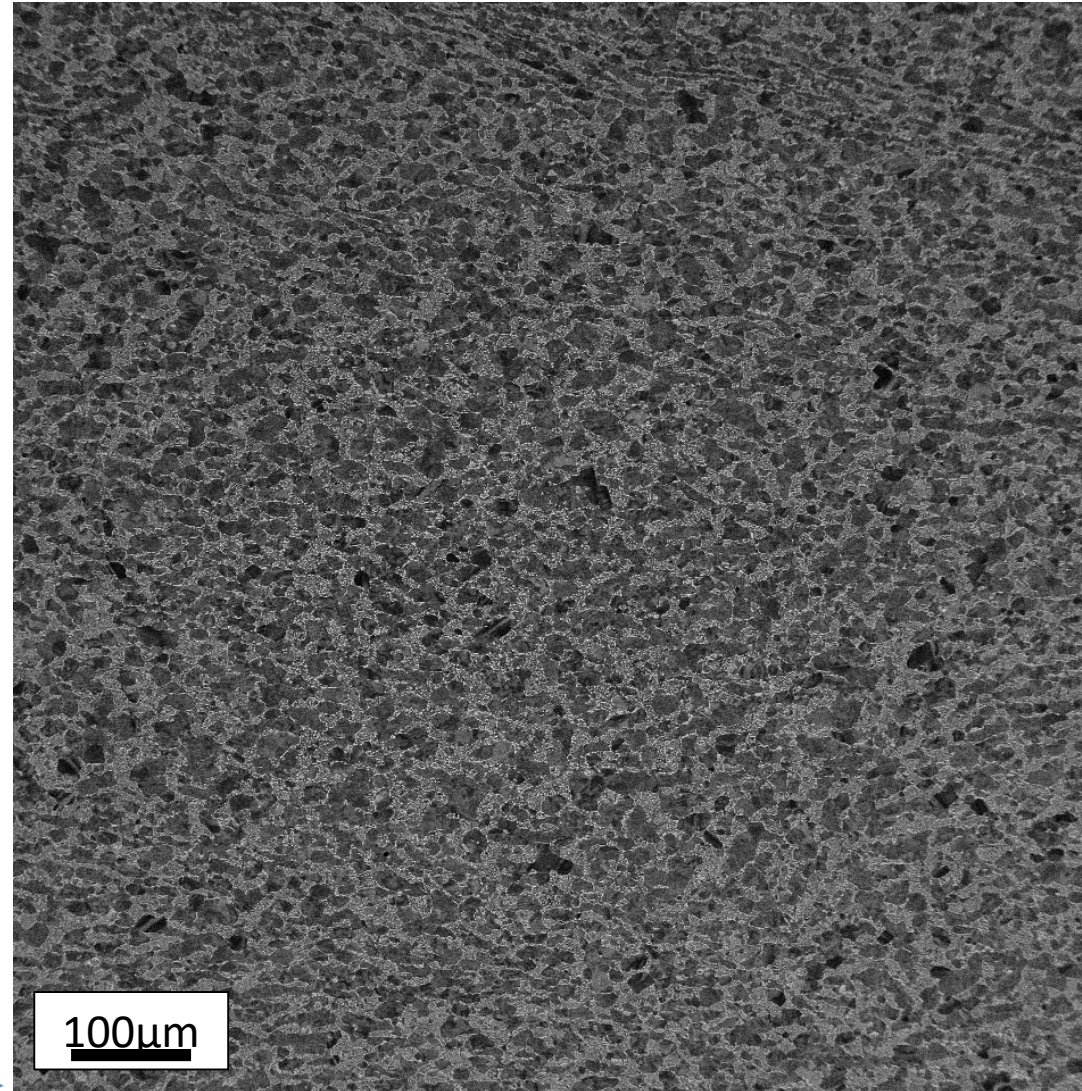
Recent Progress



- Removal of regions of interest via wire EDM
 - Samples were β -forged, β -annealed, and $(\alpha+\beta)$ -forged
 - Were not $(\alpha+\beta)$ annealed
- Bulk texture measurement via x-ray diffraction
 - Bulk texture was very weak (1.2x random for pyramidal planes)
- Scanning electron microscopy of samples

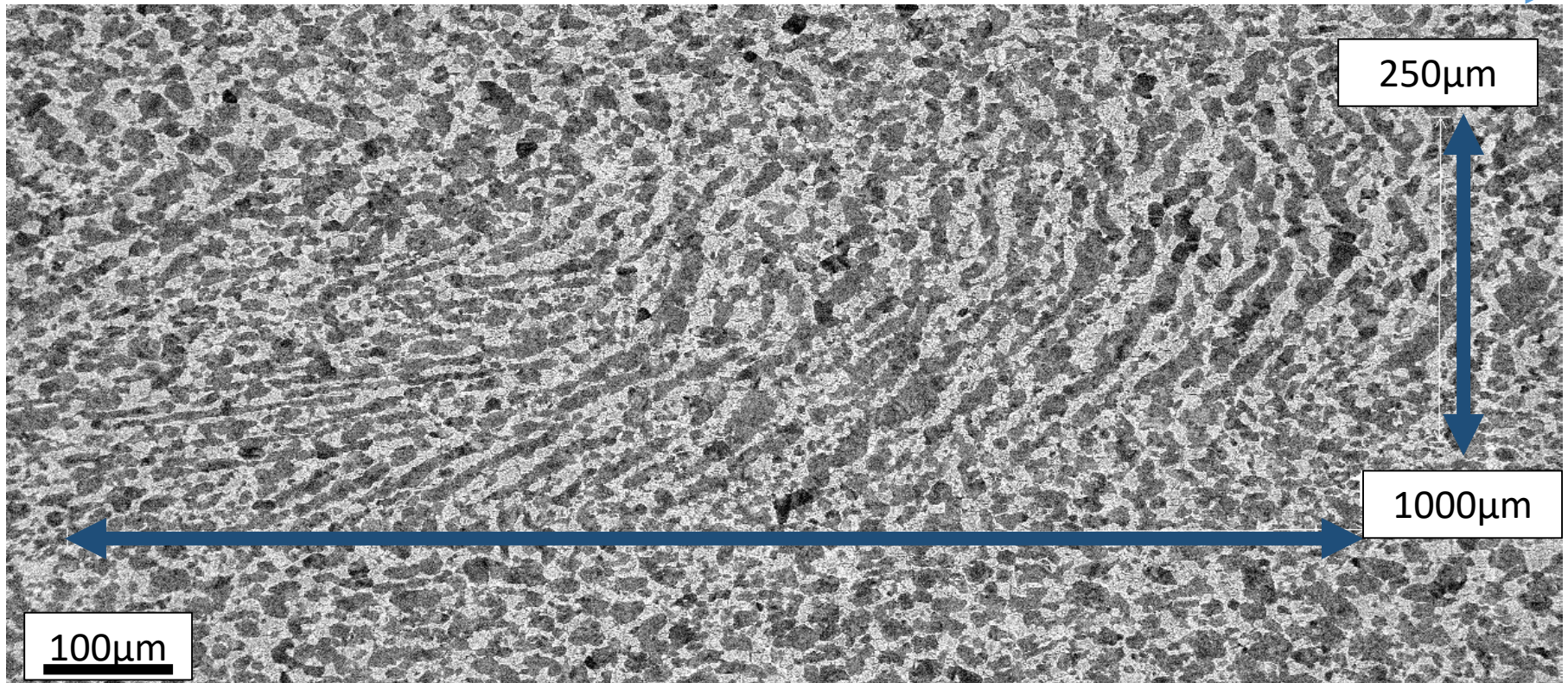
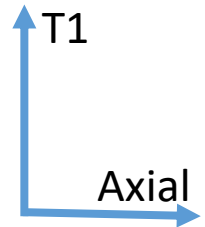
SEM of Coin 1 (above location with 30% SNR)

- “Control” samples above/below indication
- Expected for non-heat treated microstructure
 - Nominally equiaxed α
 - Nothing too coarse
 - Small amount of elongated α



SEM of Coin 2 (30% SNR)

- Large, bent α colony remnants observed
 - Evidence of poor recrystallization
 - Cannot observe crystallographic orientation via SEM
 - Proceeded to perform EBSD

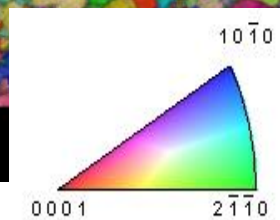
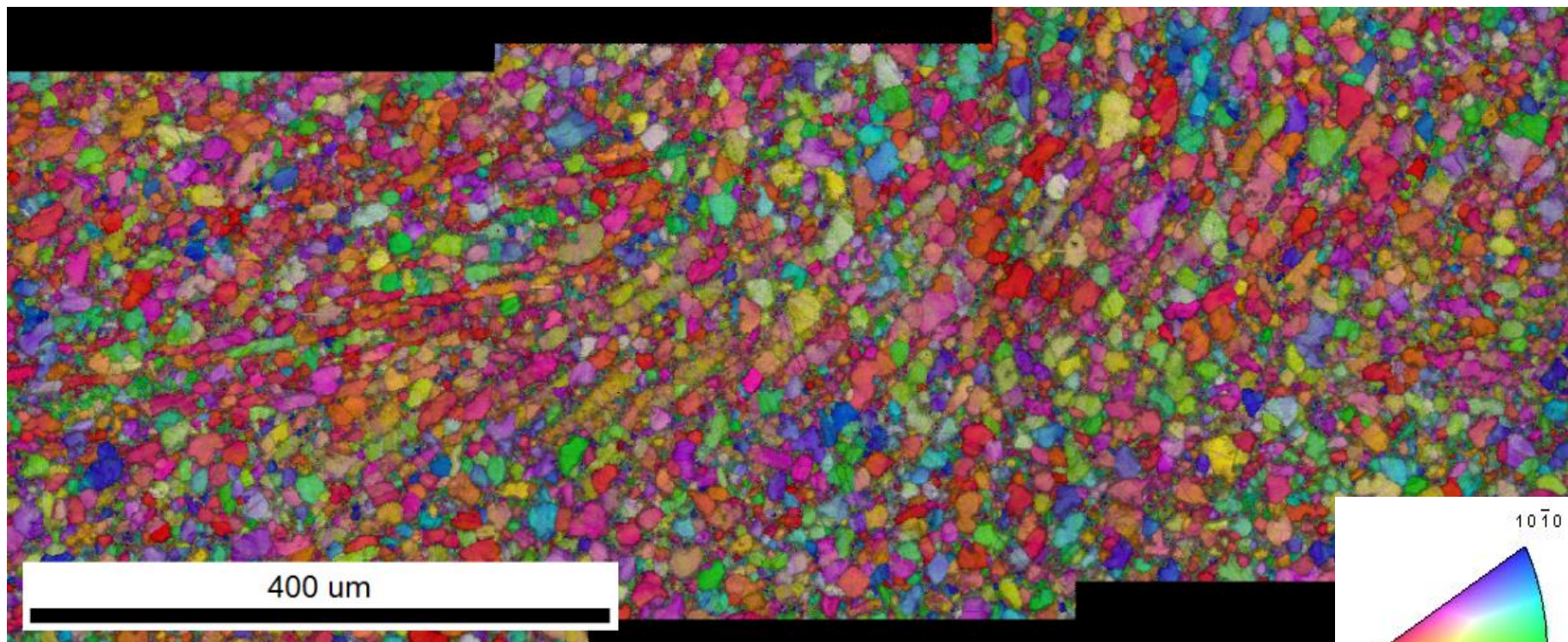
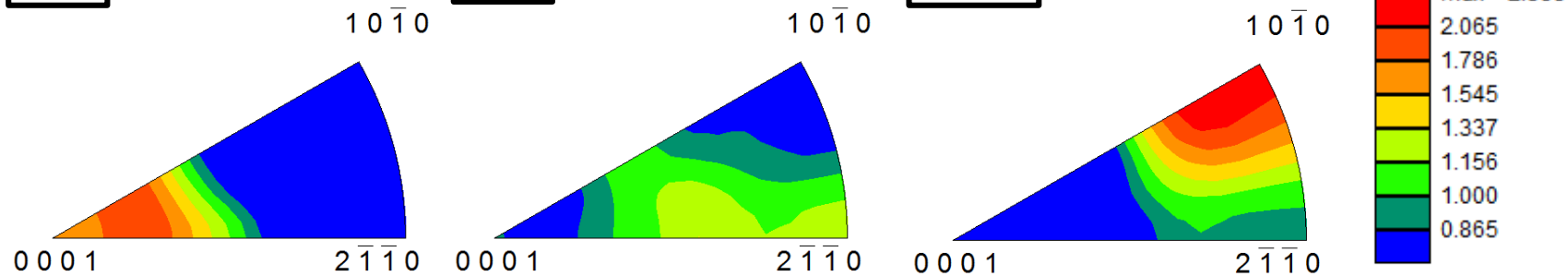


EBSD of Coin 2

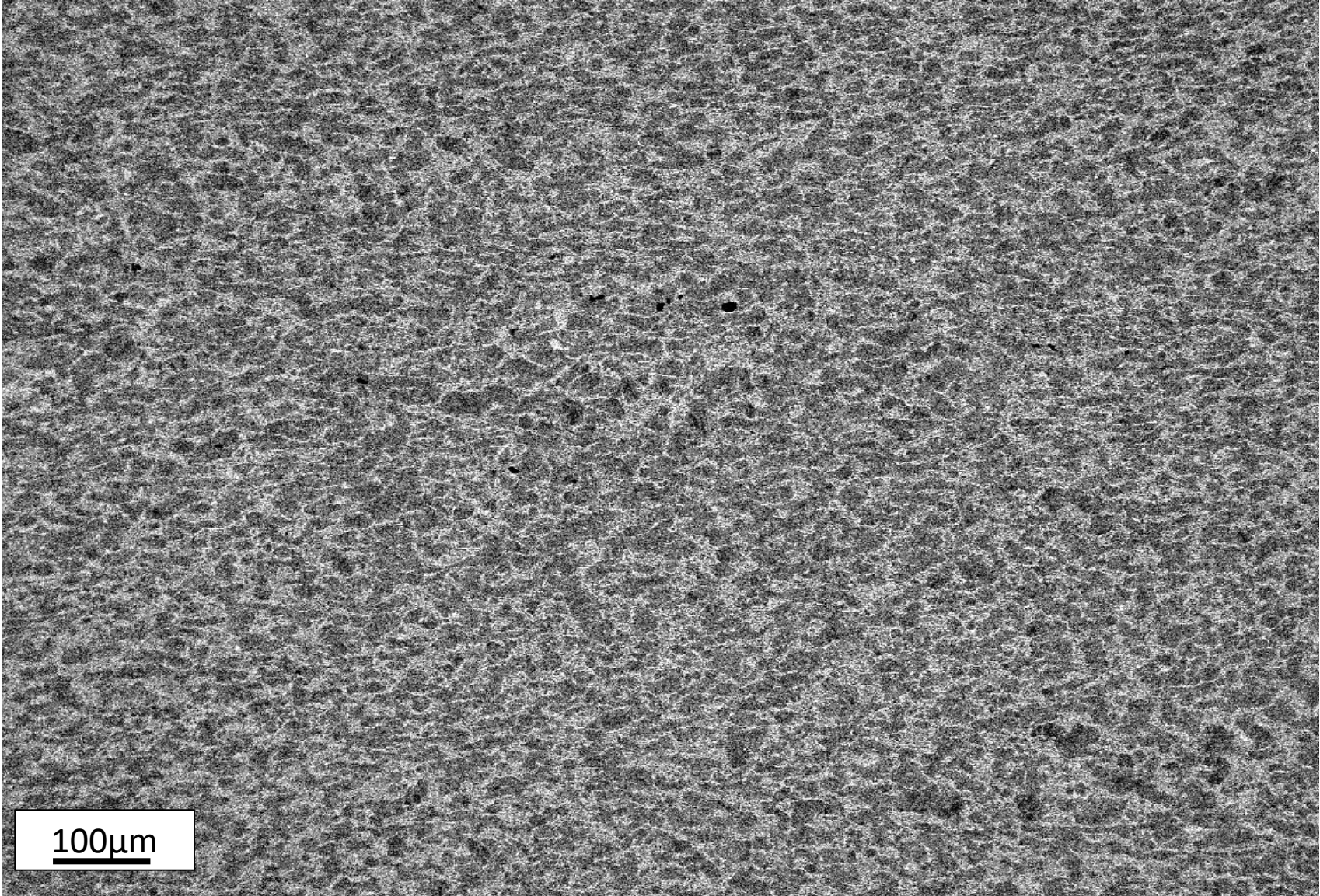
T1

T2

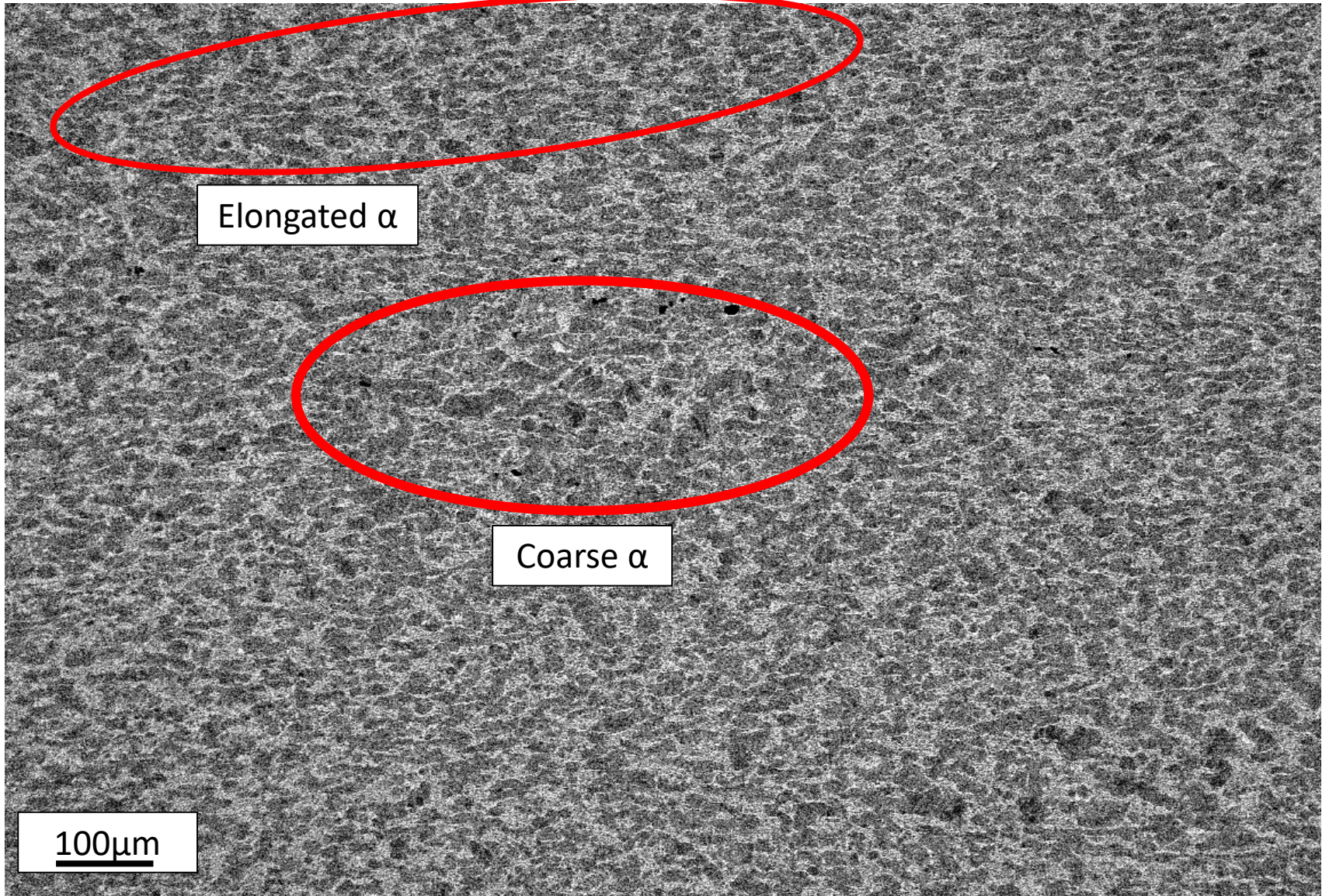
Axial



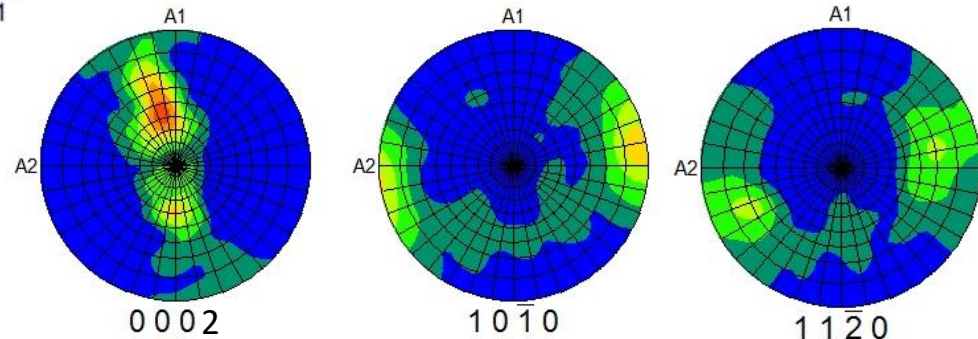
SEM of Square 2



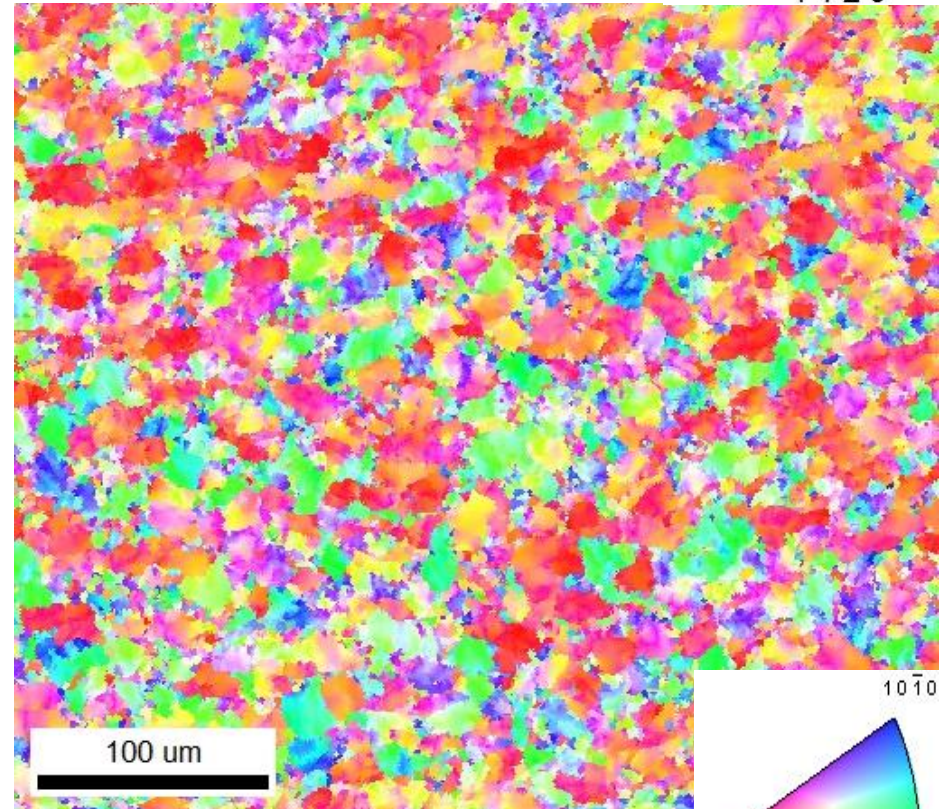
SEM of Square 2 - Annotated



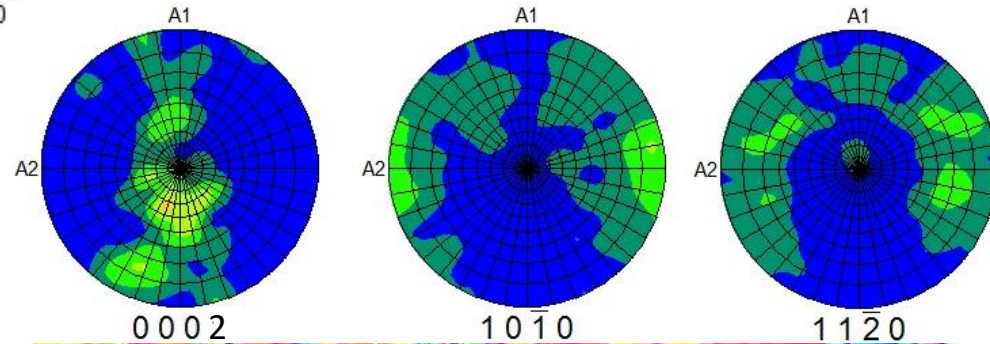
EBSD of Square 2 (40% SNR)



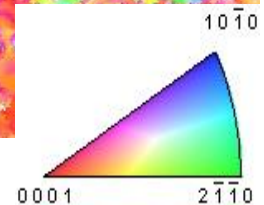
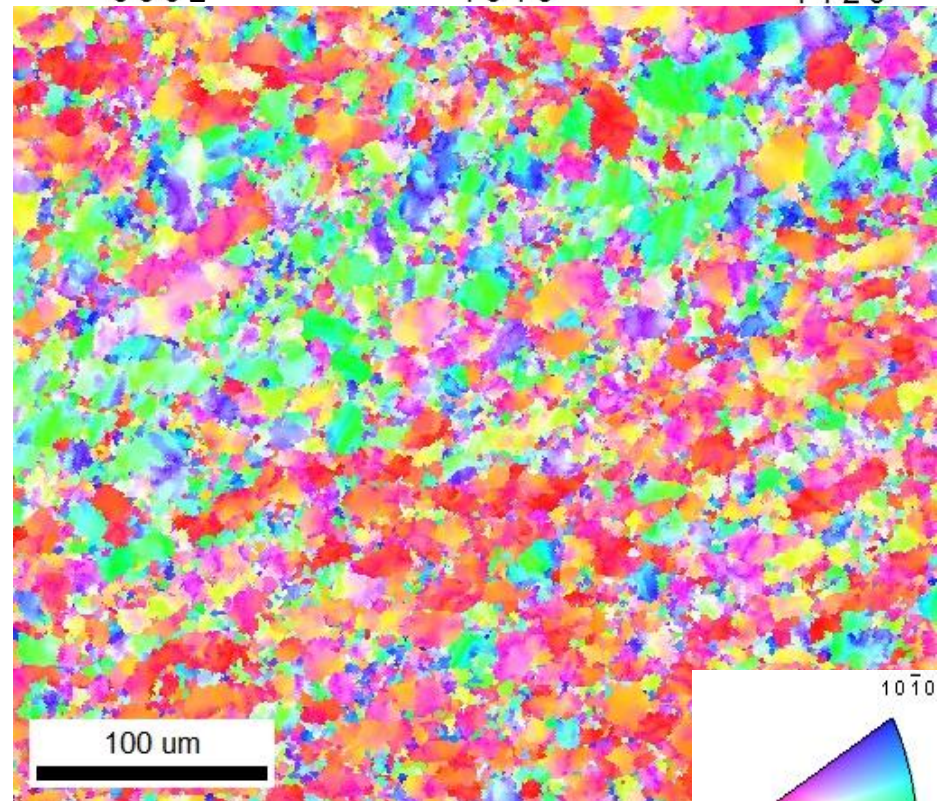
- Locally, texture intensities measured of 3.9x random
- Two dominant preferred orientations in this location
 - Red more dominant in this case
- Locations scanned were approximately below the transducer location



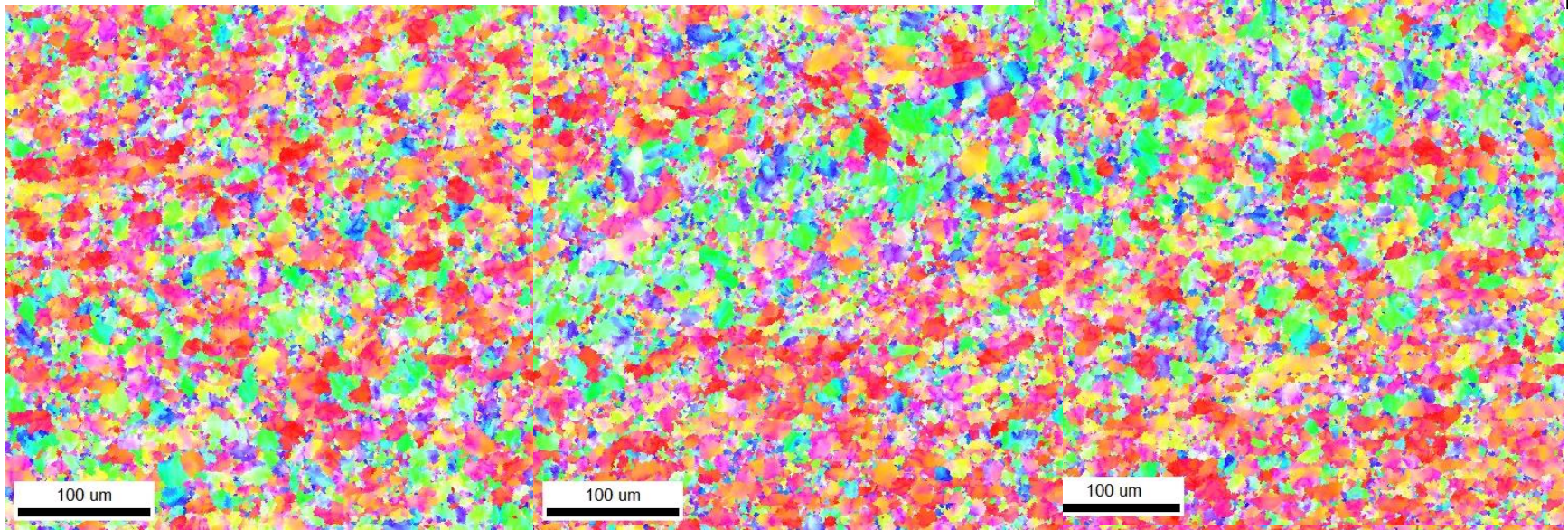
EBSD of Square 2 (40% SNR)



- Two dominant orientations more apparent here
- Appear to be looking within a microtextured region!

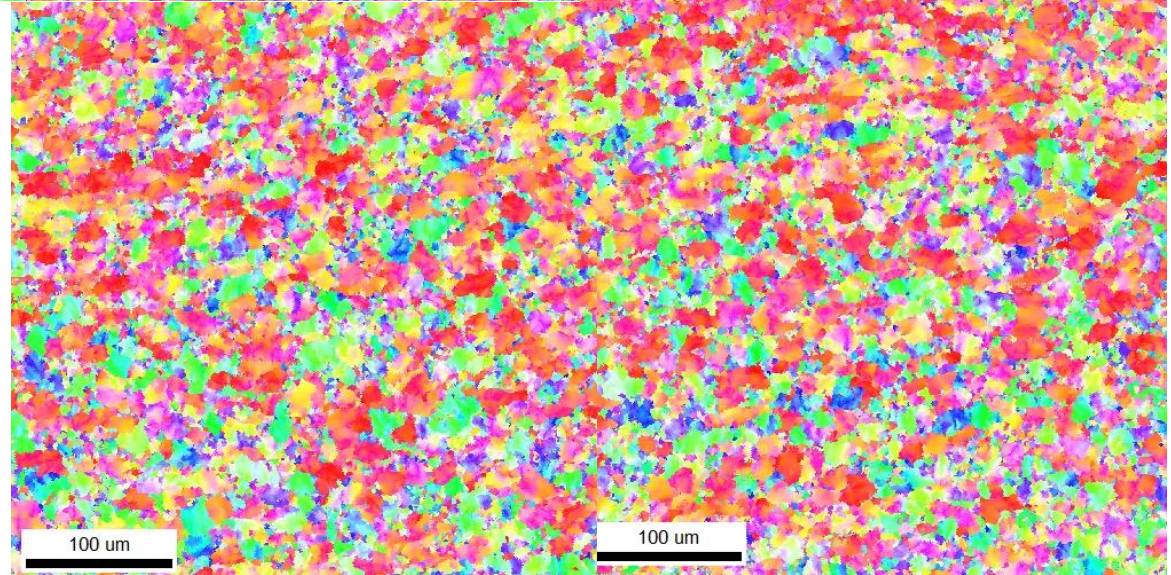


“Stitched” EBSD Maps

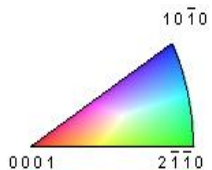


For a bigger picture view...

“I can’t do it in TSL/OIM, but I can do it in PowerPoint!”



— Connor Campbell



Recent Progress



- Removal of regions of interest via wire EDM
 - Samples were β -forged, β -annealed, and $(\alpha+\beta)$ -forged
 - Were not $(\alpha+\beta)$ annealed
- Bulk texture measurement via x-ray diffraction
 - Bulk texture was very weak (1.2x random for pyramidal planes)
- Scanning electron microscopy of samples
 - From regions with high ultrasonic signal, took images of:
 - α colony remnants
 - Elongated and coarse α
 - Preferred orientation

Summary of Recent Progress



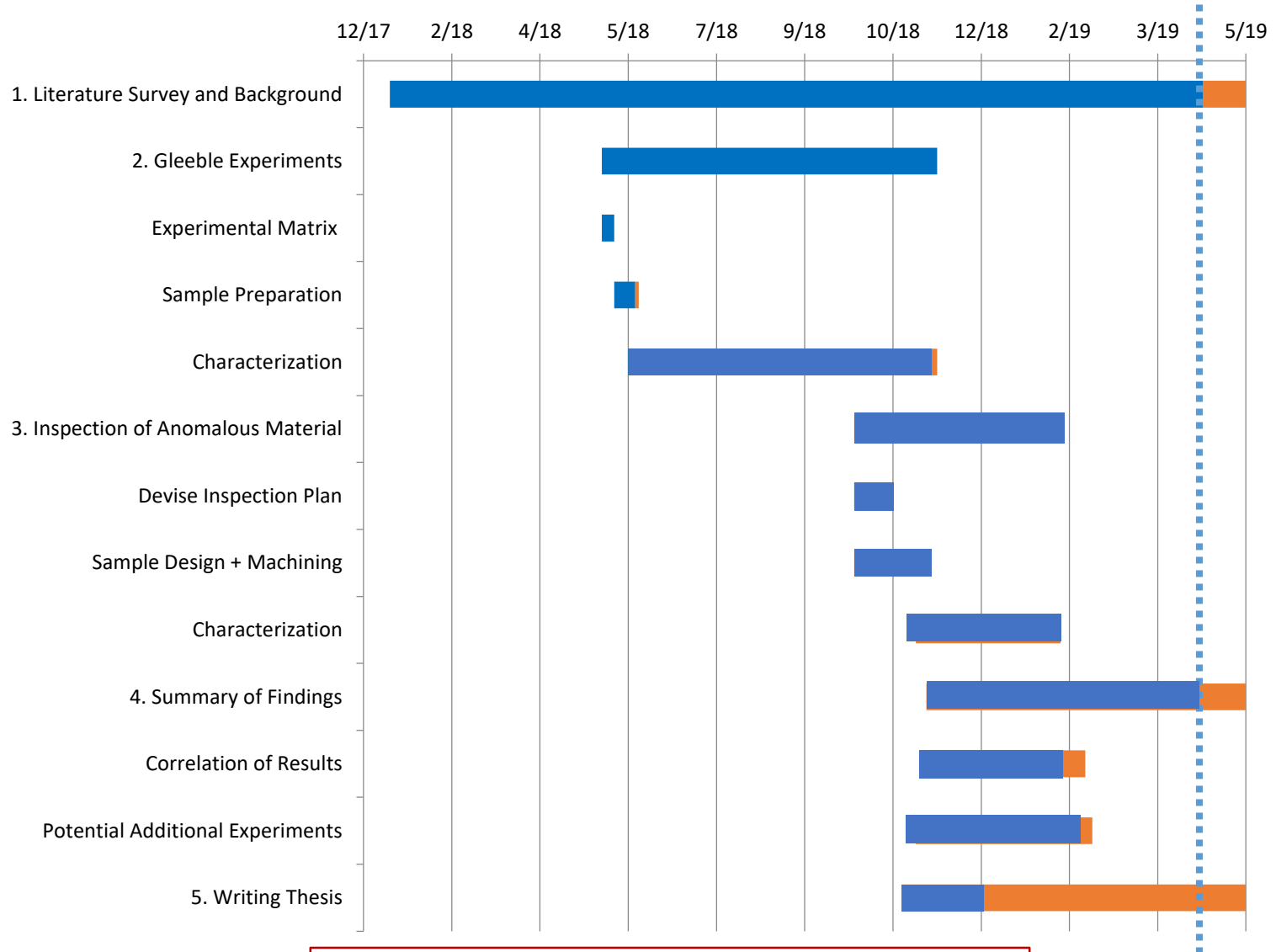
- Weak bulk texture detected via XRD
- Stronger local texture detected via EBSD
- Microstructural heterogeneity observed via SEM-BEI
 - α colony remnants
 - Elongated and coarse α (up to $100\mu\text{m}$)
 - If UT wavelength was selected for a uniform, fine microstructure, plausible that these features would scatter incident acoustics
- Microstructure appears to have not recrystallized
 - Plausible, given location near surface
 - Thermal losses and friction at dies may have a role in decreasing strain at observed locations

Future Work



- Quantify SEM images by measuring:
 - Size of equiaxed α
 - Volume fraction of equiaxed α
 - Volume fraction of total α
 - Thickness of α laths
- Obtain EBSD maps of control regions for comparison and analysis
 - Regions of low noise and symmetrically equivalent sites
 - i.e. similar depth, but near the top surface
- Finish thesis

Gantt Chart



Thank you very much!

Connor R. Campbell
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Special thanks to B. Terry at Colorado School of Mines for his tireless FESEM work!



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Membership Agreement Apply