

Project 38-L: On-Demand Casting of Net-Shape Titanium Components for Improved Weapon System Reliability

***Spring 2019 Semi-Annual Meeting
Iowa State University, Ames IA
April 3-5, 2019***

Students: Undergraduate students TBD (Mines)

Faculty: Steve Midson (Mines)

Industrial Mentor: Paul Brancaleon (NADCA)



COLORADO SCHOOL OF
MINES

**IOWA STATE
UNIVERSITY**

**Center Proprietary – Terms of CANFSA
Membership Agreement Apply**

Project 38-L: On-Demand Casting of Net-Shape Titanium Components for Improved Weapon System Reliability



- Undergraduate student: TBD
- Advisor: S. Midson (Mines)

Project Details
 UG August 2018 to July 2023
 Funded by DLA

- **Problem:** The supply chain for low-cost, lightweight net-shape titanium components needs to be expanded.
- **Objective:** Extend the die casting process for the casting of titanium alloys. Identify a permanent die + coating system for titanium die casting.
- **Benefit:** Die casting is a low-cost approach for producing components, and so the extension of die casting to Ti-alloys could have a significant impact on the titanium marketplace.

- Recent Progress
- Reviewed published information on die materials for high melting temperature alloys
 - Identified a study where refractory metals were successfully used as die materials for steel die casting
 - Looking at three approaches to fabricate a die that will meet project targets

Metrics		
Description	% Complete	Status
1. Identification of titanium alloy with improved castability (if necessary)	5%	●
2. Identification of candidate high temperature resistant die casting die materials & coatings for titanium die casting	15%	●
3. Casting trials to evaluate die materials	0%	●
4. Provide a coated tool for the demonstration of on-demand melting	0%	●

Industrial Relevance



Needs

- The supply chain for net-shape titanium components can be expanded by the development of high volume die casting methods

Benefits

- Expanded supply chain for net-shape titanium components
- Production of lower cost titanium components
- Replace heavier components with lightweight titanium castings



Project Outline



- **Three Universities**

- CSM, Purdue, University of Alabama at Birmingham

- **Technology:**

- Develop an on-demand die casting system for titanium alloys

- Develop advanced die materials for casting titanium

- Ensure castability through modifications of titanium alloy composition

- Optimize metal quality

Project Tasks - CSM



1. Die casting dies

- Identify high temperature resistant die materials and coatings for titanium die casting
- Test die concepts in the laboratory
- Provide a coated tool for the demonstration of on-demand die casting of titanium

Potential Tooling Issues

- Heat checking
 - Cracking of die surface due to cyclical thermal fatigue
- Gross cracking
 - From high levels of thermal and mechanical stresses
- Oxidation of die
 - Due to high melting temperature of the titanium
- Reaction between liquid titanium and mold material



Heat checking of an H13 steel die

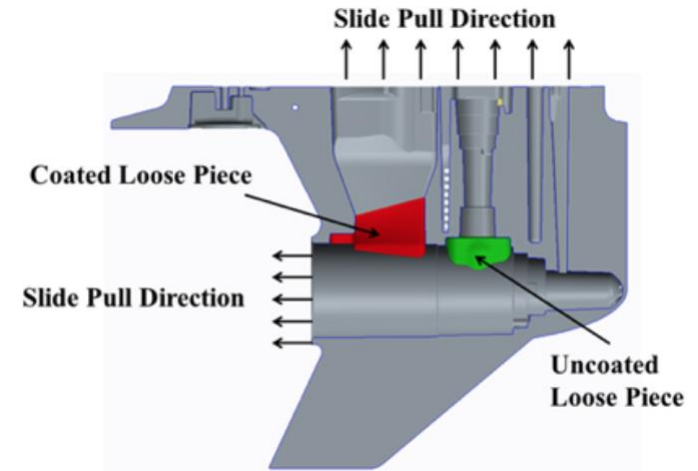
Tooling Concepts



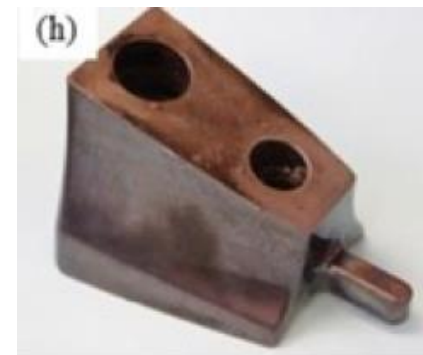
- Examining three approaches
 1. Metallic tool with graphite liners
 2. Metallic tool with ceramic coatings
 3. Refractory metal tools

Graphite Liners

- Would a relatively soft graphite liner survive aggressive die casting process?
 - High injection speeds
 - 25 m/sec
 - High injection pressures
 - 6,000 psi
- Fabricate an insert from graphite
 - For an aluminum die casting die
- Perform a test at Mercury Castings



- Gearcase die casting at Mercury Castings
- Colored die inserts are ejected with casting



- Insert shown in red
- Insert is about 4-inches in size

Grade of Graphite	Compressive Strength (ksi)	Tensile Strength (ksi)
IPG24	24	7

Metallic Tool with Ceramic Coating



- Metallic tool would support loads from die casting process
 - Ceramic coating would protect the metallic tool from the high temperatures associated with titanium die casting
- Utilize similar ceramics as thermal barrier coatings
 - Partially or fully stabilized zirconia
 - Yttria
 - Coating would need to be fully dense
- Current deposition process of EB-PVD would provide poor adhesion to the metallic substrate
- Alternative deposition processes
 - Sputtering
 - Pulsed laser deposition
 - Thermal spray + post-deposition grinding

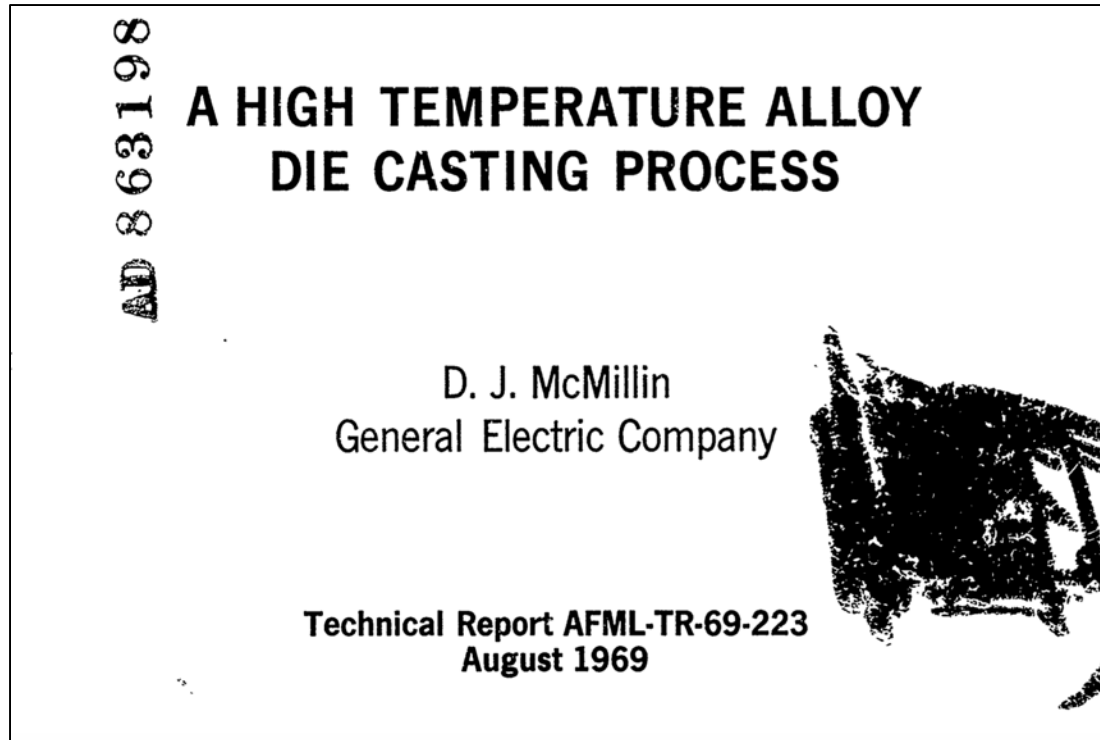
Metallic Tool with Ceramic Coating



- What are the potential failure modes?
 - Spalling of coating
 - Thermal shock of coating
- Test by fabricating simple coated tool for evaluation in CSM foundry
- Pour liquid metals into the mold
 - Liquid aluminum
 - Liquid copper
 - Liquid steels
- Evaluate integrity of ceramic coatings after testing

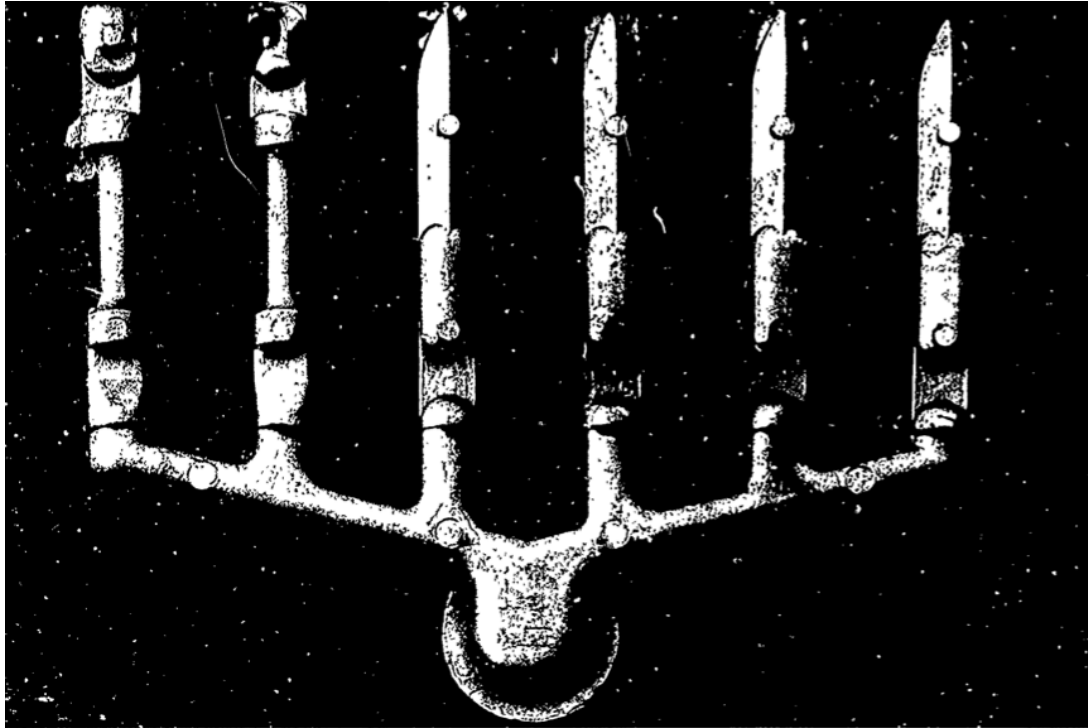
Refractory Metal Dies

- GE examined ferrous die casting in the 1960s



- Produced an extensive 450 page report in 1969
 - 80 pages involves a die material study

GE's Die Life Study



- Used a 6-cavity die
- Examined 23 different die materials
 - Molybdenum based
 - Tungsten based

Summary of Die Life



<u>Material</u>	<u>Number of Cycles Experienced</u>	<u>Condition</u>	<u>Mode of Deterioration</u>
Cu-infiltrated W	2	Failed	Brittle failure (mechanical-- not in cavity)
H-13	728	Failed	Plastic deformation (cavity)
Cu-infiltrated Mo (2% Be-Cu)*	2,745	Failed	Heat checking/erosion
Anviloy 1150	2,585	Failed	Heat checking/erosion
Cb-752	4,017	Failed	Gross cracking
GE-474*	7,017	Failed	Erosion/heat checking
P&S W-2% ThO ₂ +	3,470	Poor	Random brittle failure/erosion
Anviloy 1150	8,992	Failed	Heat checking/erosion
P&S W+	6,055	Fair/Poor	Random brittle failure/erosion
80-20*	8,992	Failed	Random brittle failure/ heat checking
Wrought Mo	8,990	Failed	Brittle failure (delamination)
Cb-25% Zr+	8,285	Fair	Heat checking
Hi-density, P&S Mo (insert retainer plates)	8,992	Failed	Gross cracking/plastic deformation
Wrought Mo (insert retainer plates)+	6,055	Good/Fair	Gross cracking/brittle failure (delamination)
Silicided wrought Mo+	6,055	Very good	Plastic deformation (gap formation) brittle failure (delamination)
Wrought Mo+	15,047	Fair/Poor	Brittle failure (delamination)
Hi-density, P&S Mo+	8,285	Very good	Plastic deformation
Hi-density, P&S Mo	15,047	Fair/Poor	Plastic deformation (gaps and dents)/gross cracking
HOT SHOT 2920X**	14,792	Fair	Heat checking
HOT SHOT 2920X** (solution annealed)	14,319	Good	Heat checking
Hi-density, P&S Mo+	15,047	Good	Plastic deformation (dents)
TZM+	15,047	Good	Brittle failure (delamination)
Mo-3**	15,047	Good	Pitting/heat checking

- 23 different die materials

Summary of Die Life



<u>Material</u>	<u>Number of Cycles Experienced</u>	<u>Condition</u>	<u>Mode of Deterioration</u>
Cu-infiltrated W	2	Failed	Brittle failure (mechanical-- not in cavity)
H-13	728	Failed	Plastic deformation (cavity)
Cu-infiltrated Mo (2% Be-Cu)*	2,745	Failed	Heat checking/erosion
Anviloy 1150	2,585	Failed	Heat checking/erosion
Cb-752	4,017	Failed	Gross cracking
GE-474*	7,017	Failed	Erosion/heat checking
P&S W-2% ThO ₂ +	3,470	Poor	Random brittle failure/erosion
Anviloy 1150	8,992	Failed	Heat checking/erosion
P&S W+	6,055	Fair/Poor	Random brittle failure/erosion
80-20*	8,992	Failed	Random brittle failure/ heat checking
Wrought Mo	8,990	Failed	Brittle failure (delamination)
Cb-25% Zr+	8,285	Fair	Heat checking
Hi-density, P&S Mo (insert retainer plates)	8,992	Failed	Gross cracking/plastic deformation
Wrought Mo (insert retainer plates)+	6,055	Good/Fair	Gross cracking/brittle failure (delamination)
Silicided wrought Mo+	6,055	Very good	Plastic deformation (gap formation) brittle failure (delamination)
Wrought Mo+	15,047	Fair/Poor	Brittle failure (delamination)
Hi-density, P&S Mo+	8,285	Very good	Plastic deformation
Hi-density, P&S Mo	15,047	Fair/Poor	Plastic deformation (gaps and dents)/gross cracking
HOT SHOT 2920X**	14,792	Fair	Heat checking
HOT SHOT 2920X** (solution annealed)	14,319	Good	Heat checking
Hi-density, P&S Mo+	15,047	Good	Plastic deformation (dents)
TZM+	15,047	Good	Brittle failure (delamination)
Mo-3**	15,047	Good	Pitting/heat checking

- 23 different die materials

Summary of Die Life



<u>Material</u>	<u>Number of Cycles Experienced</u>	<u>Condition</u>	<u>Mode of Deterioration</u>
Cu-infiltrated W	2	Failed	Brittle failure (mechanical-- not in cavity)
H-13	728	Failed	Plastic deformation (cavity)
Cu-infiltrated Mo (2% Be-Cu)*	2,745	Failed	Heat checking/erosion
Anviloy 1150	2,585	Failed	Heat checking/erosion
Cb-752	4,017	Failed	Gross cracking
GE-474*	7,017	Failed	Erosion/heat checking
P&S W-2% ThO ₂ +	3,470	Poor	Random brittle failure/erosion
Anviloy 1150	8,992	Failed	Heat checking/erosion
P&S W+	6,055	Fair/Poor	Random brittle failure/erosion
80-20*	8,992	Failed	Random brittle failure/heat checking
Wrought Mo	8,990	Failed	Brittle failure (delamination)
Cb-25% Zr+	8,285	Fair	Heat checking
Hi-density, P&S Mo (insert retainer plates)	8,992	Failed	Gross cracking/plastic deformation
Wrought Mo (insert retainer plates)+	6,055	Good/Fair	Gross cracking/brittle failure (delamination)
Silicided wrought Mo+	6,055	Very good	Plastic deformation (gap formation) brittle failure (delamination)
Wrought Mo+	15,047	Fair/Poor	Brittle failure (delamination)
Hi-density, P&S Mo+	8,285	Very good	Plastic deformation
Hi-density, P&S Mo	15,047	Fair/Poor	Plastic deformation (gaps and dents)/gross cracking
HOT SHOT 2920X**	14,792	Fair	Heat checking
HOT SHOT 2920X** (solution annealed)	14,319	Good	Heat checking
Hi-density, P&S Mo+	15,047	Good	Plastic deformation (dents)
TZM+	15,047	Good	Brittle failure (delamination)
Mo-3**	15,047	Good	Pitting/heat checking

- 23 different die materials

Summary of Die Life



<u>Material</u>	<u>Number of Cycles Experienced</u>	<u>Condition</u>	<u>Mode of Deterioration</u>
Cu-infiltrated W	2	Failed	Brittle failure (mechanical-- not in cavity)
H-13	728	Failed	Plastic deformation (cavity)
Cu-infiltrated Mo (2% Be-Cu)*	2,745	Failed	Heat checking/erosion
Anviloy 1150	2,585	Failed	Heat checking/erosion
Cb-752	4,017	Failed	Gross cracking
GE-474*	7,017	Failed	Erosion/heat checking
P&S W-2% ThO ₂ +	3,470	Poor	Random brittle failure/erosion
Anviloy 1150	8,992	Failed	Heat checking/erosion
P&S W+	6,055	Fair/Poor	Random brittle failure/erosion
80-20*	8,992	Failed	Random brittle failure/ heat checking
Wrought Mo	8,990	Failed	Brittle failure (delamination)
Cb-25% Zr+	8,285	Fair	Heat checking
Hi-density, P&S Mo (insert retainer plates)	8,992	Failed	Gross cracking/plastic deformation
Wrought Mo (insert retainer plates)+	6,055	Good/Fair	Gross cracking/brittle failure (delamination)
Silicided wrought Mo+	6,055	Very good	Plastic deformation (gap formation) brittle failure (delamination)
Wrought Mo+	15,047	Fair/Poor	Brittle failure (delamination)
Hi-density, P&S Mo+	8,285	Very good	Plastic deformation
Hi-density, P&S Mo	15,047	Fair/Poor	Plastic deformation (gaps and dents)/gross cracking
HOT SHOT 2920X**+	14,792	Fair	Heat checking
HOT SHOT 2920X**+ (solution annealed)	14,319	Good	Heat checking
Hi-density, P&S Mo+	15,047	Good	Plastic deformation (dents)
TZM+	15,047	Good	Brittle failure (delamination)
Mo-3**+	15,047	Good	Pitting/heat checking

- 23 different die materials

Summary of Die Life

<u>Material</u>	<u>Number of Cycles Experienced</u>	<u>Condition</u>	<u>Mode of Deterioration</u>
Wrought Mo+	15,047	Fair/Poor	Brittle failure (delamination)
Hi-density, P&S Mo+	8,285	Very good	Plastic deformation
Hi-density, P&S Mo	15,047	Fair/Poor	Plastic deformation (gaps and dents)/gross cracking
HOT SHOT 2920X*+	14,792	Fair	Heat checking
HOT SHOT 2920X*+ (solution annealed)	14,319	Good	Heat checking
Hi-density, P&S Mo+	15,047	Good	Plastic deformation (dents)
TZM+	15,047	Good	Brittle failure (delamination)
Mo-3*+	15,047	Good	Pitting/heat checking

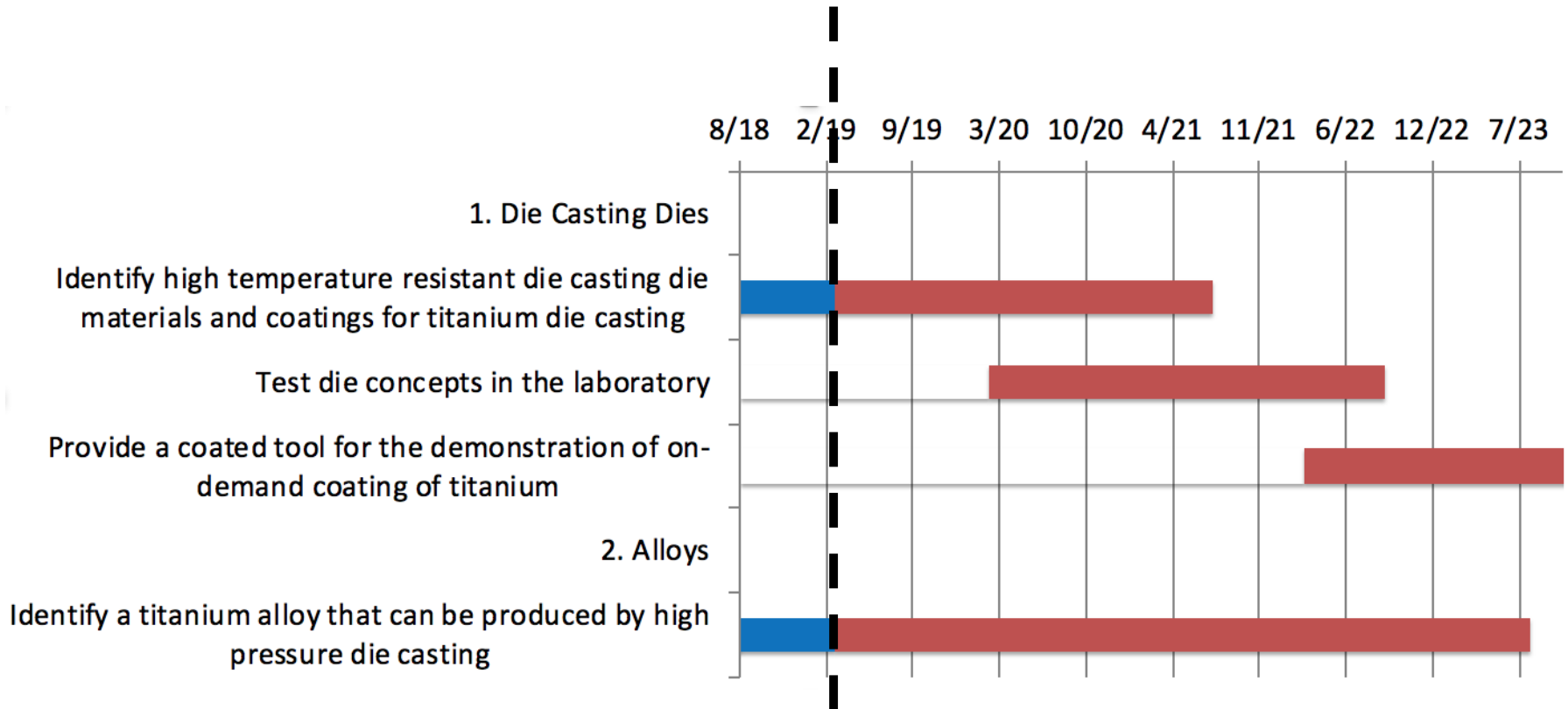
Source: GE Ferrous Die Casting Report, 1969

Future Work - Die Materials for Titanium Die Casting



- Continue to evaluate three approaches
 - Graphite liners
 - Coated metallic tools
 - Refractory metals
- Refractory metal dies
 - Use modeling to evaluate optimum configuration of die and cooling
 - Does conformal cooling extend or reduce die life
 - Cast steel alloys for testing of die materials in foundry at the Colorado School of Mines

Gantt Chart



Acknowledgement

This research is sponsored by the DLA – Troop Support, Philadelphia, PA and the Defense Logistics Agency Information Operations, J62LB, Research & Development, Ft. Belvoir, VA



**Center Proprietary – Terms of CANFSA
Membership Agreement Apply**

Thank you!

Steve Midson

smidson@mines.edu