#### Center for Advanced Non-Ferrous Structural Alloys

An Industry/University Cooperative Research Center

#### Project #33:In-situ Studies of Strain Rate Effects on Phase Transformations and Microstructural Evolution in β-Titanium and Multi-Principle Element Alloys

#### Spring 2018 Semi-Annual Meeting Colorado School of Mines, Golden, CO April 11-12, 2018

Student: Benjamin Ellyson (Mines) Faculty: Amy Clarke (Mines) Industrial Mentor(s): TBD Other Participants: Yaofeng Guo (Mines)







#### Project 33: In-Situ Studies of Strain Rate Effects on Phase Transformations and Microstructural Evolution in β-Titanium

| <ul> <li>Student: Benjamin Ellyson (Mines)</li> <li>Advisor(s): Amy Clarke (Mines)</li> </ul>  | Project Duration<br>PhD: September 2017 to May 2021   |
|--|---|
| <ul> <li><u>Problem:</u> Uniform elongation and work hardening of titanium alloys restricts applications.</li> <li><u>Objective:</u> Fundamentally understand microstructural evolution in metastable β titanium alloys to develop an alloy design methodology and tailor microstructures and properties.</li> <li><u>Benefit</u>: Novel titanium alloys for blast and crash resistant applications</li> </ul> | <ul> <li><u>Recent Progress</u></li> <li>Heat treatment performed to obtain β phase microstructures that exhibit TRIP/TWIP</li> <li>Compressive testing of solution treated samples partially completed</li> <li>Investigation of low-temperature, short soak time treatments is under way</li> <li>Initial thermo-mechanical testing completed in the Gleeble</li> </ul> |

| Metrics  |            |        |  |  |
|--|------------|--------|--|--|
| Description  | % Complete | Status |  |  |
| 1. β solution treatments   | 95%        | •      |  |  |
| 2. Literature review   | 50%        | •      |  |  |
| 3. High-throughput quasi-static compression testing to $\beta$ solution heat treatment | 90%        | •      |  |  |
| 4. Optical microstructural characterization of pre and post compression conditions     |            | •      |  |  |
| 5. EBSD/TEM microstructural characterization of pre and post compression conditions    | 10%        | •      |  |  |



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#### Industrial Relevance: Development of Blast Resistant Materials for the Navy

- Cellular Materials Program
  - Multifunctional structures
  - Blast resistance
  - Thermal management



https://www.onr.navy.mil/Science-Technology/Departments/Code-33

- Propulsion
   Materials Program
  - Aircraft and marine engines





# Multi-scale Studies of TRIP/TWIP during High Rate Deformation



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#### Ti-25Nb-3Zr-3Mo-2Sn (wt.%) Alloy Microstructure After Deformation at 10<sup>-3</sup> s<sup>-1</sup> and 0.18 True Strain



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<sup>6</sup> The Effect of Strain Rate (10<sup>-3</sup>, 10<sup>-1</sup>, 10<sup>1</sup>, 10<sup>2</sup> s<sup>-1</sup>) on Deformation Mechanisms during Compression of a Ti-10V-3Fe-3AI (wt.%) Alloy

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- As strain rate increases:
  - Stress-induced α" martensite (dominant) + {332}<113> β twinning + stressinduced ω phase + slip
  - Stress-induced α"
     martensite +
     {332}<113> β twinning
     + stress-induced ω
     phase + slip
  - Stress-induced α" martensite + {332}<113> β twinning (dominant) + stressinduced ω phase + slip





Ahmed, M., et al. 104 Acta Materialia (2016): 190-200

# Work Hardening and Evidence of TRIP/TWIP



Brozek, C., et al. Scripta Materialia 114 (2016): 60-64



# **Ti-1023 Heat Treatments to Obtain Fully β Microstructures**

To promote TRIP/TWIP:

- Single phase β microstructure
- Fully homogenized
- Small grain size promotes TRIP
- Large grain size promotes TWIP

Li, C., et al. *Materials Science and Engineering: A* 528.18 (2011): 5854-5860 Bhattacharjee, A., et al. *Scripta materialia* 53.2 (2005): 195-200





## **Solution Heat Treatment Matrix**

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- Hold temperature and quench rate effect on martensite fraction
- Response surface for martensite phase fraction dependence
- Water and helium to vary quench rate



| Temp (°C) | Time (h) | Quench<br>medium |
|-----------|----------|------------------|
| 900       | 2        | Water or He      |
| 1000      | 2        | Water or He      |
| 1100      | 2        | Water or He      |
| 1200      | 2        | Water or He      |

- Sample denomination will be as follows:
- Temperature-time-quench-condition
- 900-2h-WQ-pre
- 900-2h-WQ-post
- 900-2h-WQ-10<sup>-2</sup>





#### **Preliminary Water Quench Results**







#### **Representative of 1000°C and 1100°C**



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# <sup>13</sup> Challenges in Obtaining Fully β Microstructures in Ti-1023

 Obtaining a fully-retained β structure in Ti-1023 requires severe quench rates and thin sections

Bhattacharjee, A., et al. Scripta materialia 53.2 (2005): 195-200
Duerig, T. W., et al. Acta Metallurgica30.12 (1982): 2161-2172
Neelakantan, S., et al. Materials Science and Technology 25.11 (2009): 1351-1358





# <sup>14</sup> 1200-2h-WQ Exhibits Larger Grain Size and Inhomogeneous Response



#### Less nucleation sites for martensite





Factors controlling the ability to produce fully β microstructures:

- Sample size
- Quench delay
- Quench rate
- Grain size



### **Sample Geometry - Compression**



# 900-2h-HeQ-pre Exhibits Equiaxed β







### 1000C-2h-WQ-pre equiaxed β







### 1100C-2h-HeQ-pre equiaxed β

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#### Traces of α" in the 1200-2h-HeQ-pre



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# <sup>21</sup> Only a Single Grain Boundary in the 1200-2h-HeQ-pre cross-section



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# <sup>22</sup> Optical Microstructural Characterization Summary

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| Condition   | Martensite<br>Fraction | # of Grains in Φ4<br>mm Cross Section |
|-------------|------------------------|---------------------------------------|
| 900-2h-WQ   | ~ 15%                  | ~50                                   |
| 900-2h-HeQ  | ~ 2%                   | ~ 60                                  |
| 1000-2h-WQ  | < 1%                   | ~ 17                                  |
| 1000-2h-HeQ | ~ 0%                   | ~ 12                                  |
| 1100-2h-HeQ | ~ 2%                   | ~ 3                                   |
| 1200-2h-HeQ | ~ 6%<br>(only @ GB)    | ~ 2                                   |



## Compression of 1000-2h-WQ at 10<sup>-4</sup>/s



## Compression of 1000-2h-WQ at 10<sup>-4</sup>/s



## Comparison of As-received and 1000-2h-WQ-10<sup>-4</sup>



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# Instantaneous Work Hardening Rate comparison



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#### Comparison of Pre- and Post-Compression Microstructure of 1000-2h-WQ-10<sup>-4</sup>





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# Stress-Strain Behavior does not Suggest TRIP/TWIP ...



#### Comparison of Pre- and Post-Compression Microstructure of 1000-2h-HeQ-10<sup>-2</sup>





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#### Comparison of Pre- and Post-Compression Microstructure of 900-2h-WQ-10<sup>-2</sup>





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#### Comparison of Pre- and Post-Compression Microstructure of 900-2h-WQ-10<sup>-2</sup>





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#### Comparison of Pre- and Post-Compression Microstructure of 1200-2h-HeQ-10<sup>-2</sup>





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### **Compression Study Summary**

#### Every heat treatment investigated shows TRIP/TWIP in post-compression microstructure





# Orientation of Product Similar Within a Single Grain





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# <sup>35</sup> Multiple Variants Can Be Present in a Single Grain







### **Hierarchy of Deformation Product**







# <sup>37</sup> Work Hardening Rate and TRIP/TWIP Effect



# Deformation Modes in β-Ti Alloys at Room Temperature

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Twinning

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- {112}<111> twinning
- {332}<113> twinning
- Stress induced martensite
- Stress induced ω phase

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Slip





Ahmed, M., et al. 104 Acta Materialia (2016): 190-200

## **Two Twinning Systems**

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| {112}<111> twinning                                      | {332}<113> twinning |
|--|---------------------|
| (112)[111]   | (332)[113]          |
| $(121)[\overline{1}1\overline{1}]$                       | (323)[13 1]         |
| (211)[111]   | (233)[311]          |
| $(\bar{1}12)[1\bar{1}1]$                                 | (332)[113]          |
| $(\overline{1}21)[11\overline{1}]$                       | (3223)[131]         |
| $(\overline{2}11)[\overline{1}\overline{1}\overline{1}]$ | (233)[311]          |
| $(1\overline{1}2)[\overline{1}11]$                       | (332)[113]          |
| $(1\overline{2}1)[\overline{1}\overline{1}\overline{1}]$ | (323)[131]          |
| $(2\overline{1}1)[11\overline{1}]$                       | (233)[311]          |
| $(11\overline{2})[\overline{1}\overline{1}\overline{1}]$ | (332)[113]          |
| (121)[111]   | (323)[131]          |
| $(21\overline{1})[1\overline{1}1]$                       | (233)[311]          |
|  |                     |

Polarization of twinning and operative twinning



Center Proprietary – Terms of CANFSA Membership Agreement Apply

MINES

# <sup>40</sup> Schmid Factor of Two Twinning Systems



# <sup>41</sup> Coupled {332} Twinning and Stress Induced Martensitic Transformation

b

#### **Misorientation**

- {112} twinning: **∑**3, **60° <111>**
- {332} twinning: **∑11**, **50.57° <110>**



Lai, M.J., et al. 111 Acta Materialia (2016): 173-186

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4 um

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4 µm

a"\_

**B-twin** 

a"-

B-twin-

# **Ongoing EBSD Characterization**

- Post-mortem EBSD of deformed samples
- In situ EBSD during deformation
- Understanding the coupling of mechanisms in Ti-1023 will inform future Ti-alloy experiments





#### Summary

- Compression study nearly complete:
  - Fully equiaxed β microstructure with little/no martensite
  - Evidence of TRIP/TWIP behavior
- EBSD and TEM microstructural characterization is underway
- Tensile testing of Ti-1023 based upon compression testing results
- Ti-15Mo from ATI available





#### **Gantt Chart for Project 33**



Progress



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[8] Lai, M.J., et al. "On the mechanism of {332} twinning in metastable  $\beta$  titanium alloys." 111 Acta Materialia (2016): 173-186.



