

Project 26: Deformation Mechanisms in Refractory-Based Complex, Concentrated Alloys

***Spring 2018 Semi-Annual Meeting
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Faculty: Drs. Michael Kaufman and Amy Clarke (CSM)

Industrial Mentor: Drs. Kevin Chaput and Todd Butler (AFRL)

Other Participants : John Foltz (ATI), Paul Mason (Thermo-Calc)



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Project 26: Deformation Mechanisms in Refractory-Based Complex, Concentrated Alloys

- Student: Francisco Coury (Mines)
- Advisor(s): Michael Kaufman, Amy Clarke (Mines)

Project Duration
PhD: August 2015 to July 2018

Problem: Main factors that control strength and ductility of refractory complex, concentrated alloys (RCCAs) are not fully understood

Objective: Describe the mechanical behavior of RCCAs by means of conventional strengthening theories

Benefit: Improved understanding of strength and ductility will lead to more efficient alloy design.

Recent Progress

- Finished alloy characterization on as-cast and heat-treated conditions
- Started compression tests at different temperatures in different single phase alloys
- Developed modelling framework to interpret thermally activated deformation
- Modified athermal solid solution strengthening model for body centered cubic alloys

Metrics

Description	% Complete	Status
1. Literature review	100%	●
2. Production and characterization of as-cast alloys	100%	●
3. Heat-treating, processing and characterization of the heat-treated/processed material	100%	●
4. Mechanical testing the different alloys at different temperatures	90%	●
5. Develop methodology for interpreting strength of the RCCAs	50%	●



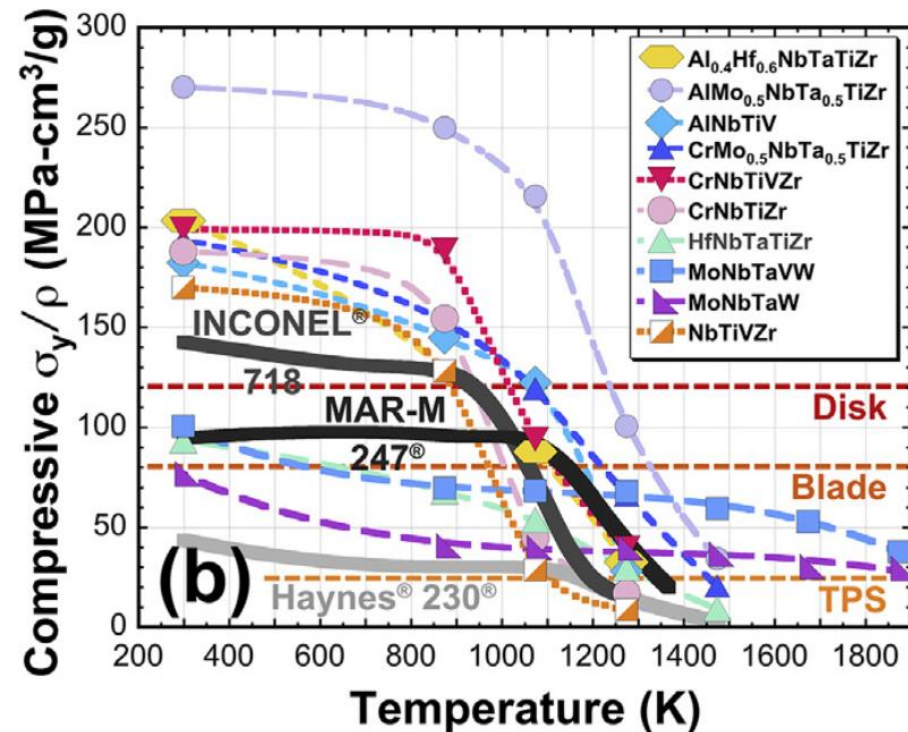
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Industrial Relevance

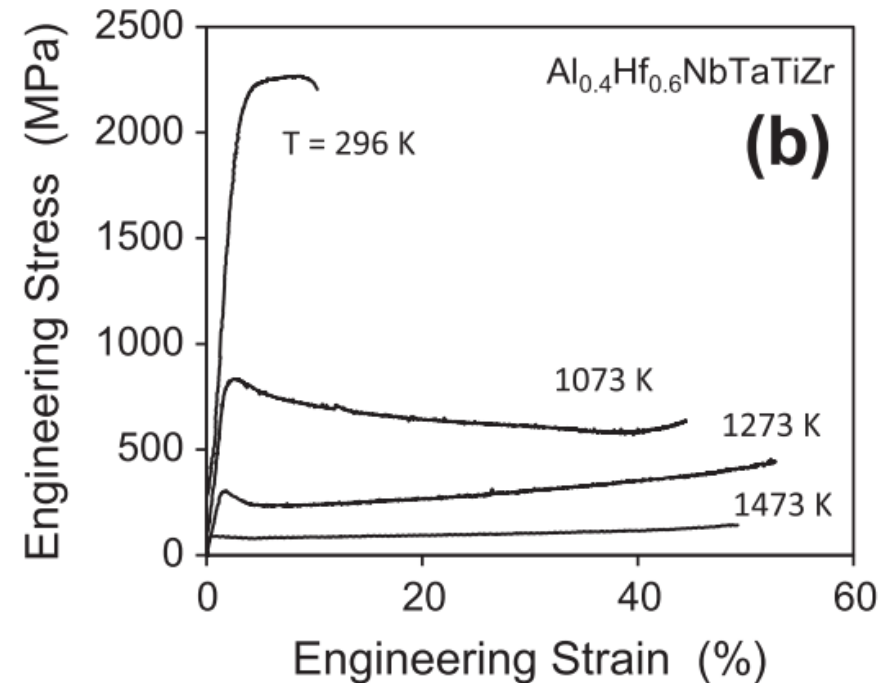
- New class of materials – early work by Senkov et al. (2011)
- Goal of expanding the applicability of refractory metals
 - High temperature strength
 - Low density
 - Easy to process
 - Better oxidation resistance



D.B. Miracle and O.N. Senkov, Acta Mater. **122**, 448 (2017).

Challenges in RCCA Development

- Typical drawbacks with refractory alloys
 - Poor room temperature ductility and toughness
 - Poor corrosion and oxidation resistance
- Specific challenges with RCCA approach
 - Broad composition space
 - Several possible compositions
 - Experimentally challenging



Senkov, O. N., Senkova, S. V. & Woodward, *Acta Mater.* **68**, 214–228 (2014).

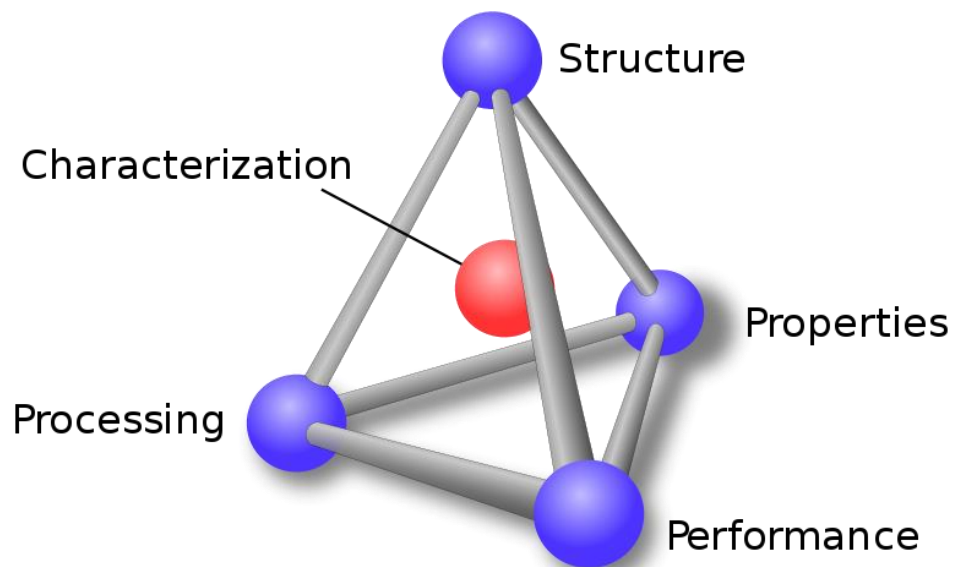
Butler, T. M., Chaput, K. J., Dietrich, J. R. & Senkov, O. N.. *J. Alloys Compd.* **729**, 1004–1019 (2017).

Where Do We Start?

- Need composition dependent models to predict properties
- For RCCAs:
 - Phase equilibria
 - Strength
 - Ductility
 - Oxidation

Motivation and Methodology

- Can we understand the strength and ductility?
 - Industrially-relevant compositions
- Approach
 - Phase equilibria
 - Microstructure
 - Processing
 - Mechanical properties



Alloy Selection

- 13 alloys using the following criteria:
 - BCC crystal structure
 - Density < 13 g/cm³
 - Cost < \$500/kg
 - No noble or rare elements
 - Fraction of binaries in thermodynamic database > 0.5
 - Small solidification range
 - No volatile elements
 - Low content of σ phase
- Cast and heat-treated at 1400 °C for 35 h

AlCrMoNb

AlHfTaTi

AlHfNbTi

AlMoNbTi

AlNbTaTi

WNbTaTi

HfNbTaTi

MoNbTaTi

CrNbTaTi

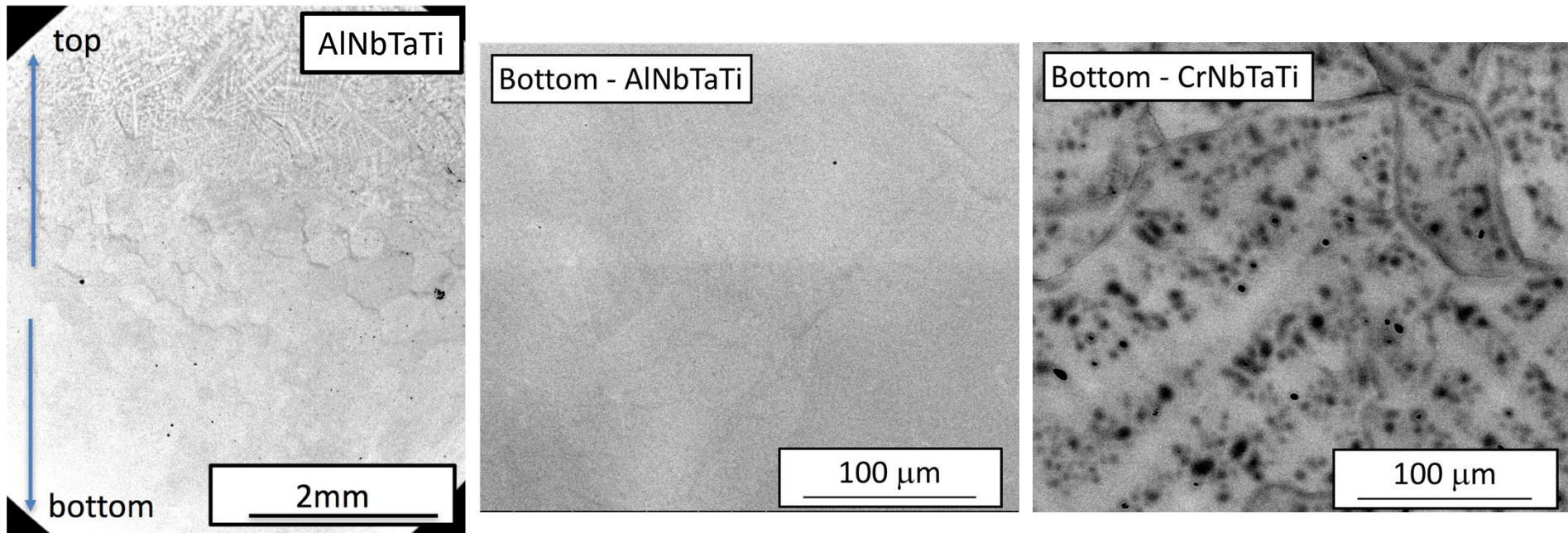
CrMoTaTi

CrMoNbTi

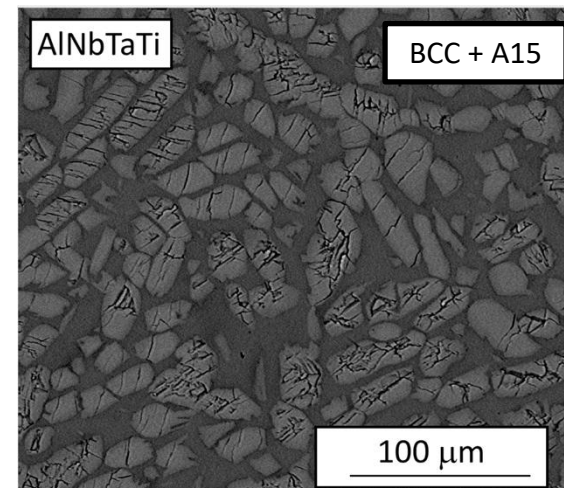
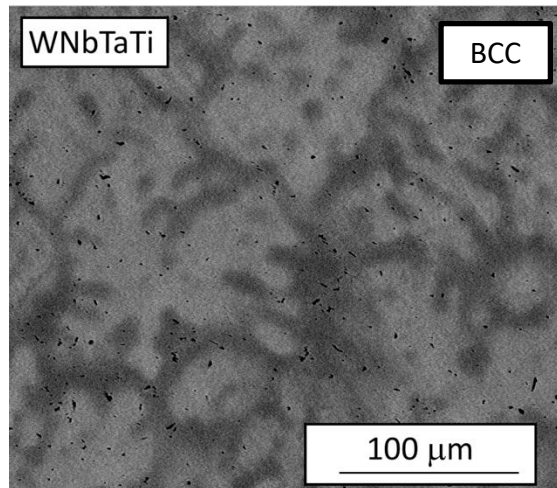
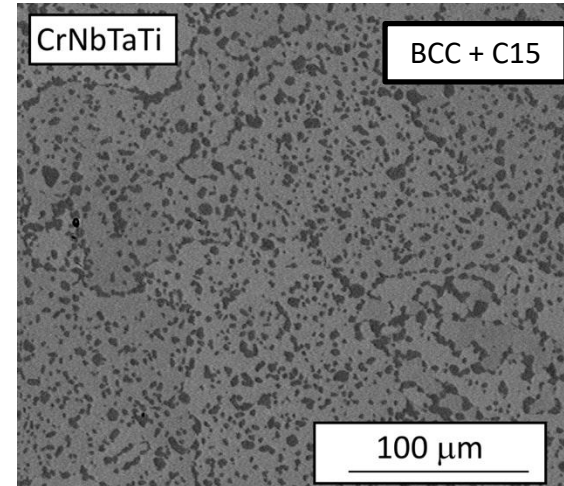
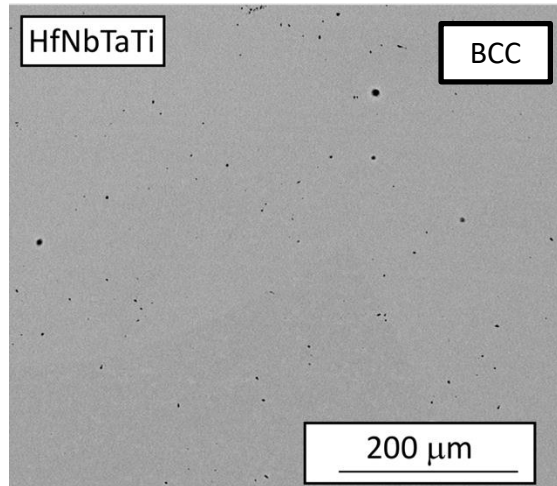
CrNbTiW

CrTaTiW

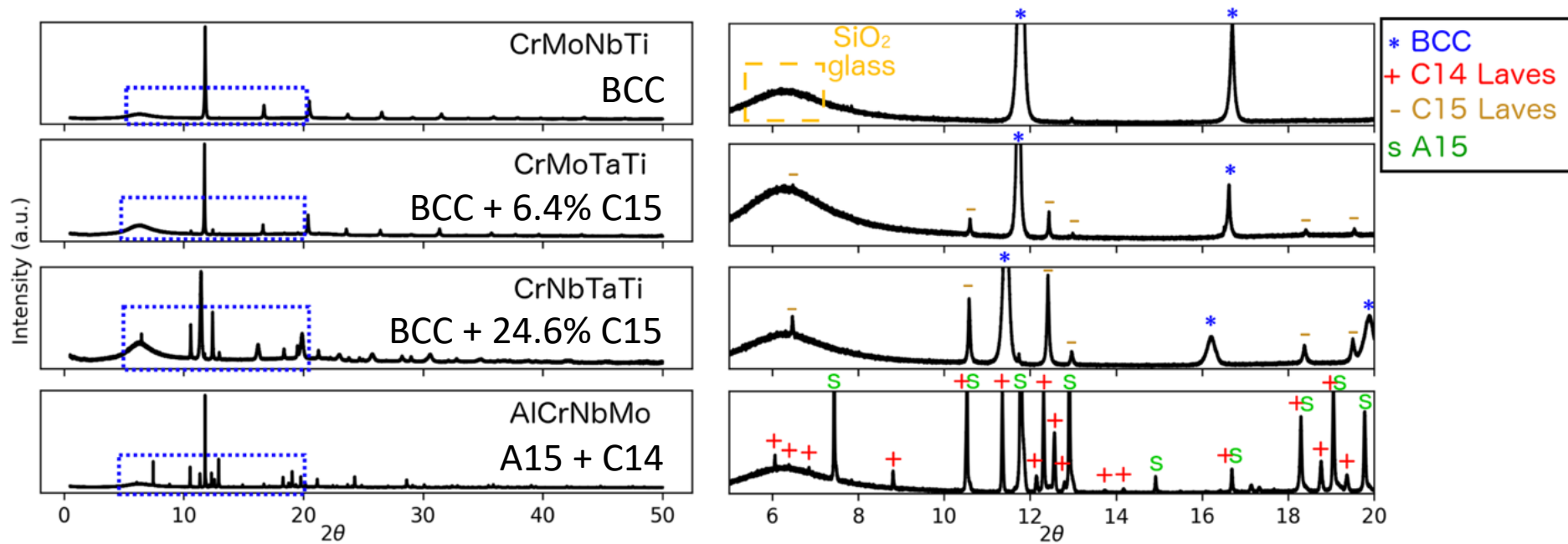
Microstructure of As-Cast Alloys



Microstructure of Heat-Treated Alloys



Synchrotron XRD Analysis of Cr-Containing Alloys



Models for Phase Prediction

- Empirical models based on Hume-Rothery rules

- Delta (δ): atomic radii differences

$$\delta = \sqrt{\sum_{i=1}^N x_i \left(1 - x_i / \sum_{j=1}^N x_j r_j\right)^2}$$

- Omega (Ω): differences in enthalpies, entropies of mixing and melting temperature

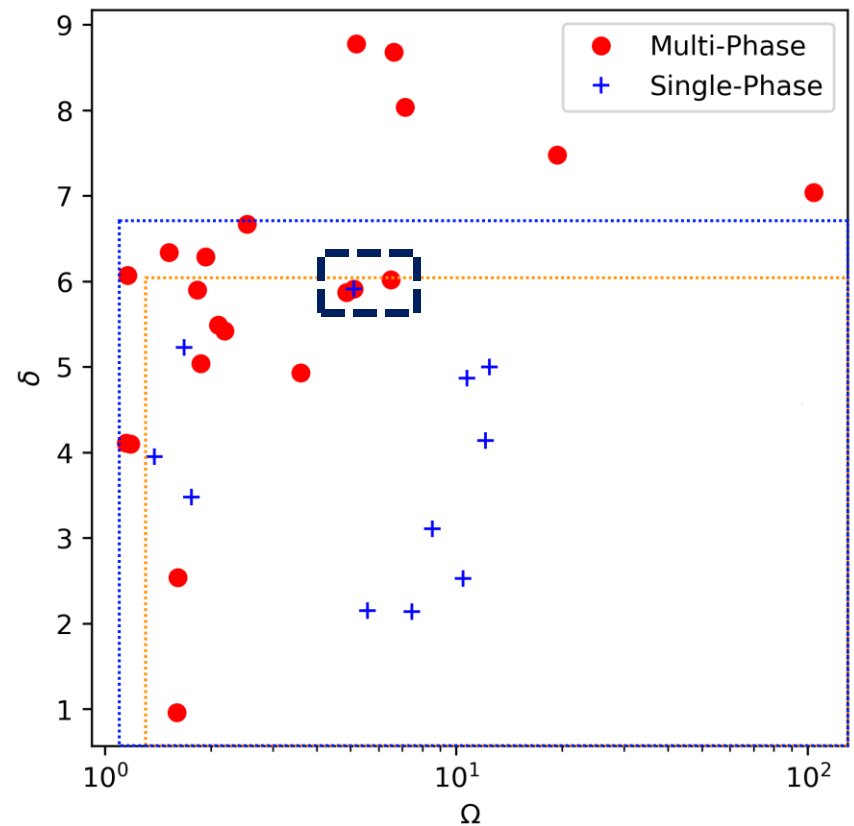
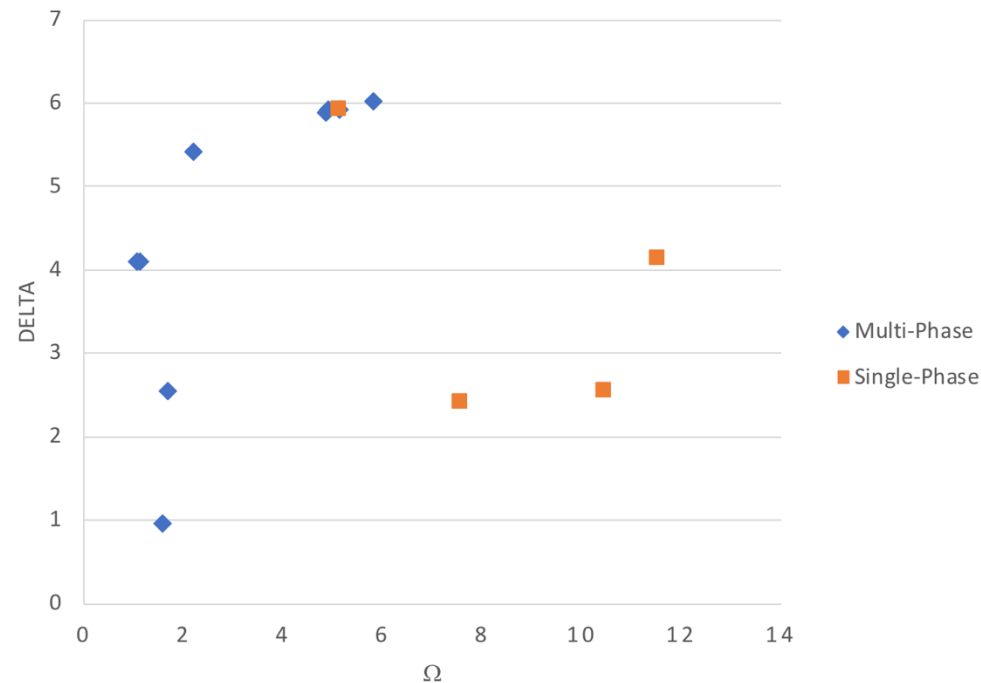
$$\Omega = \frac{T_m \Delta S_{\text{mix}}}{|\Delta H_{\text{mix}}|}$$

- Delta chi ($\Delta\chi$): electronegativity

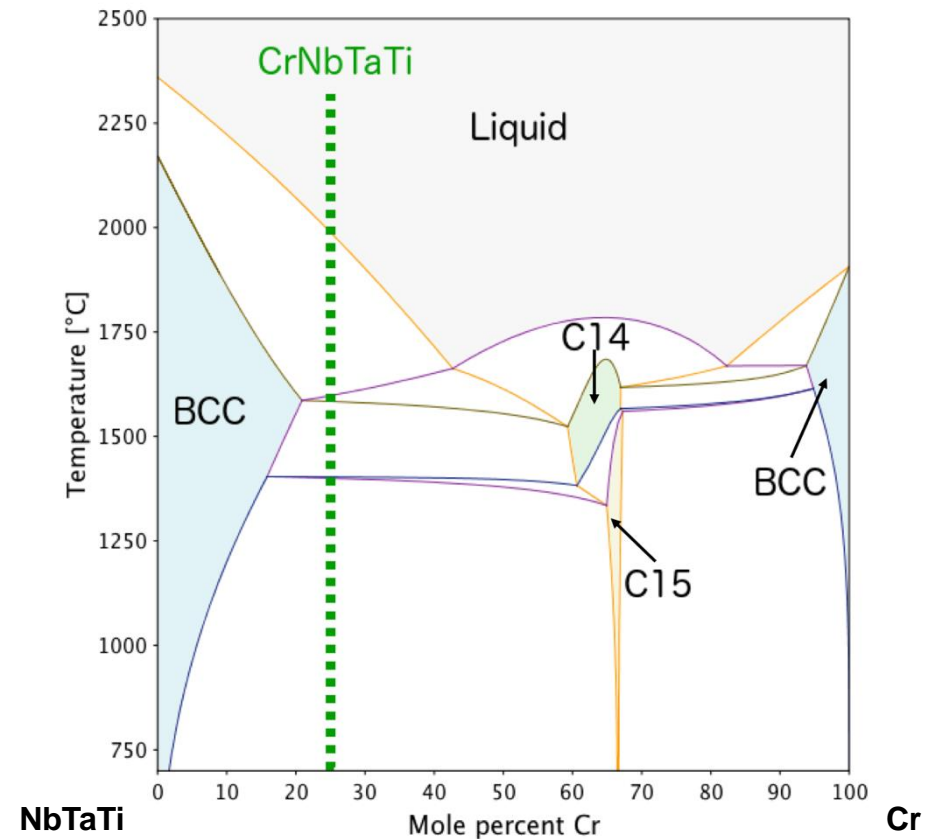
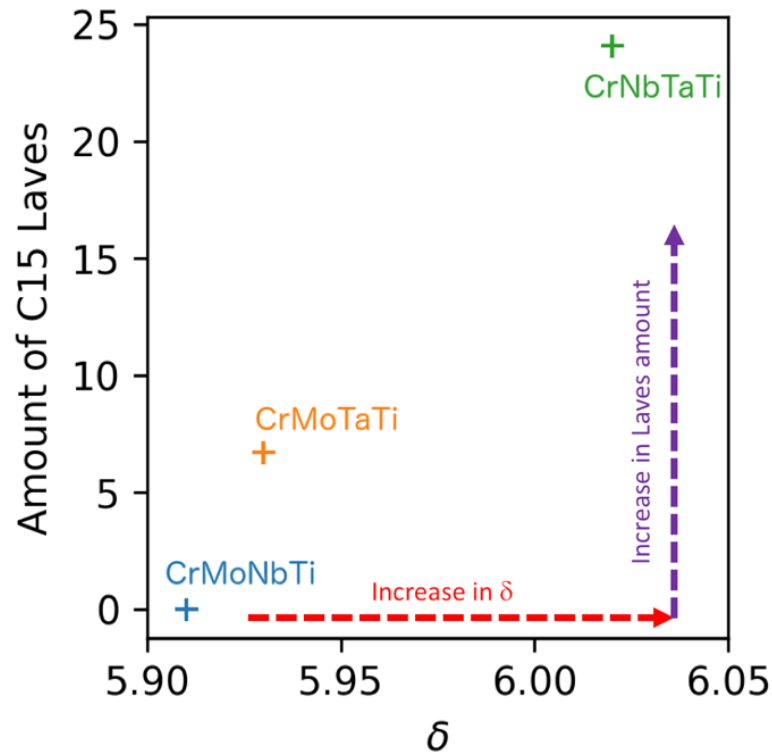
$$\Delta\chi = \sqrt{\sum_{i=1}^N x_i \left(\chi_i - \sum_{j=1}^N x_j \chi_j\right)^2}$$

- CALPHAD: Thermo-Calc[®], Pandat[™]
 - Minimize free energy in a given system

Empirical Phase Predictions



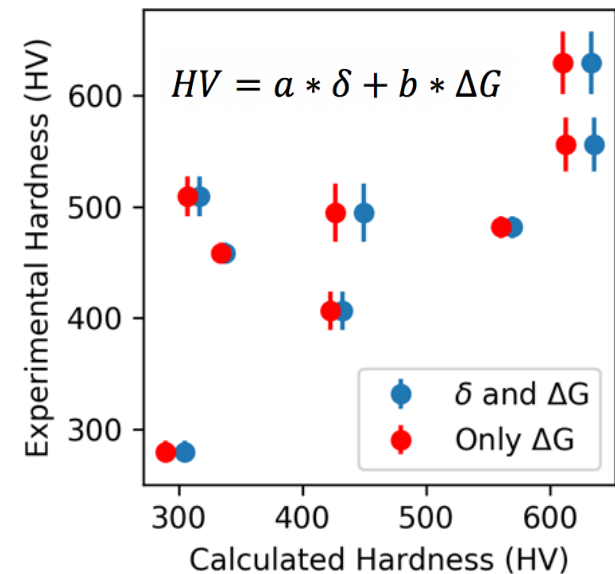
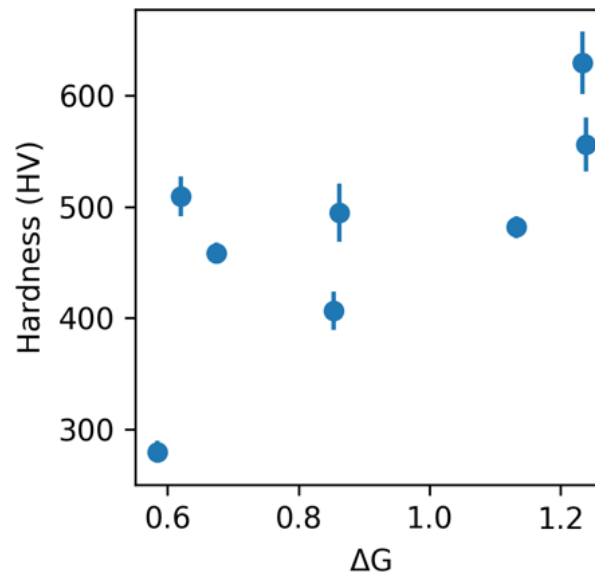
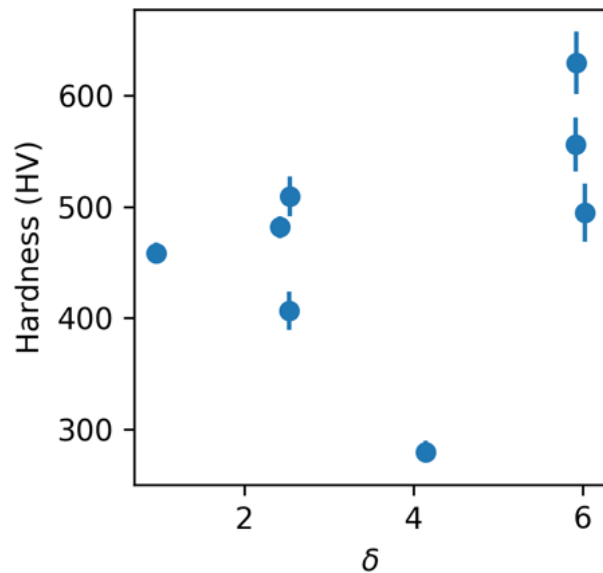
C15 Laves Phase Scales With δ



CALPHAD Predictions

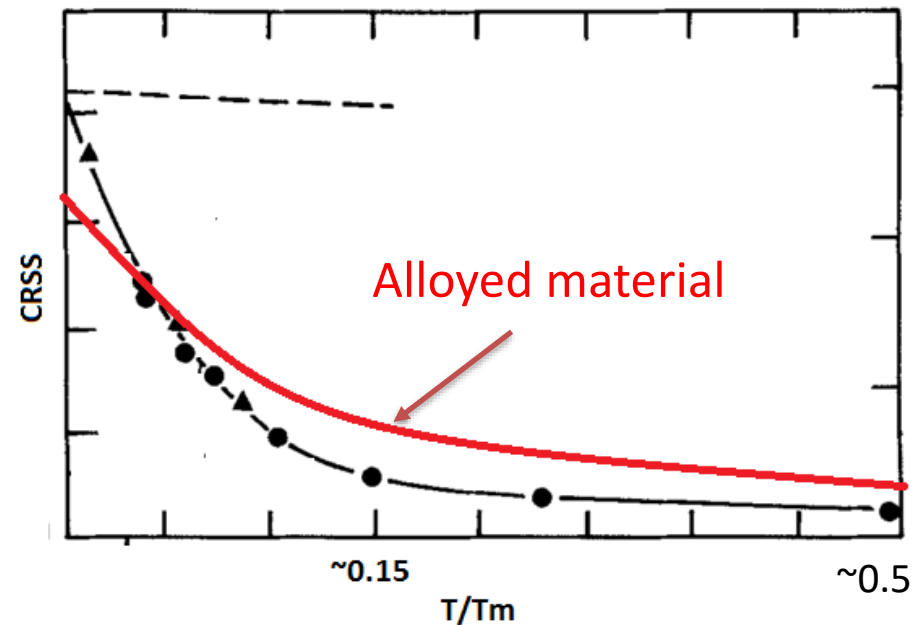
- TCHEA2 predicts correct phases in 9 of 12 alloys
 - Except B2 phase in AlHfNbTi and AlHfTaTi
 - AlMoNbTi is not single-phase
- Temperatures and volume fractions need further refinement
- Significant improvement over TCHEA1
 - C14, C15 and A15

Single-Phase RCCA Hardness

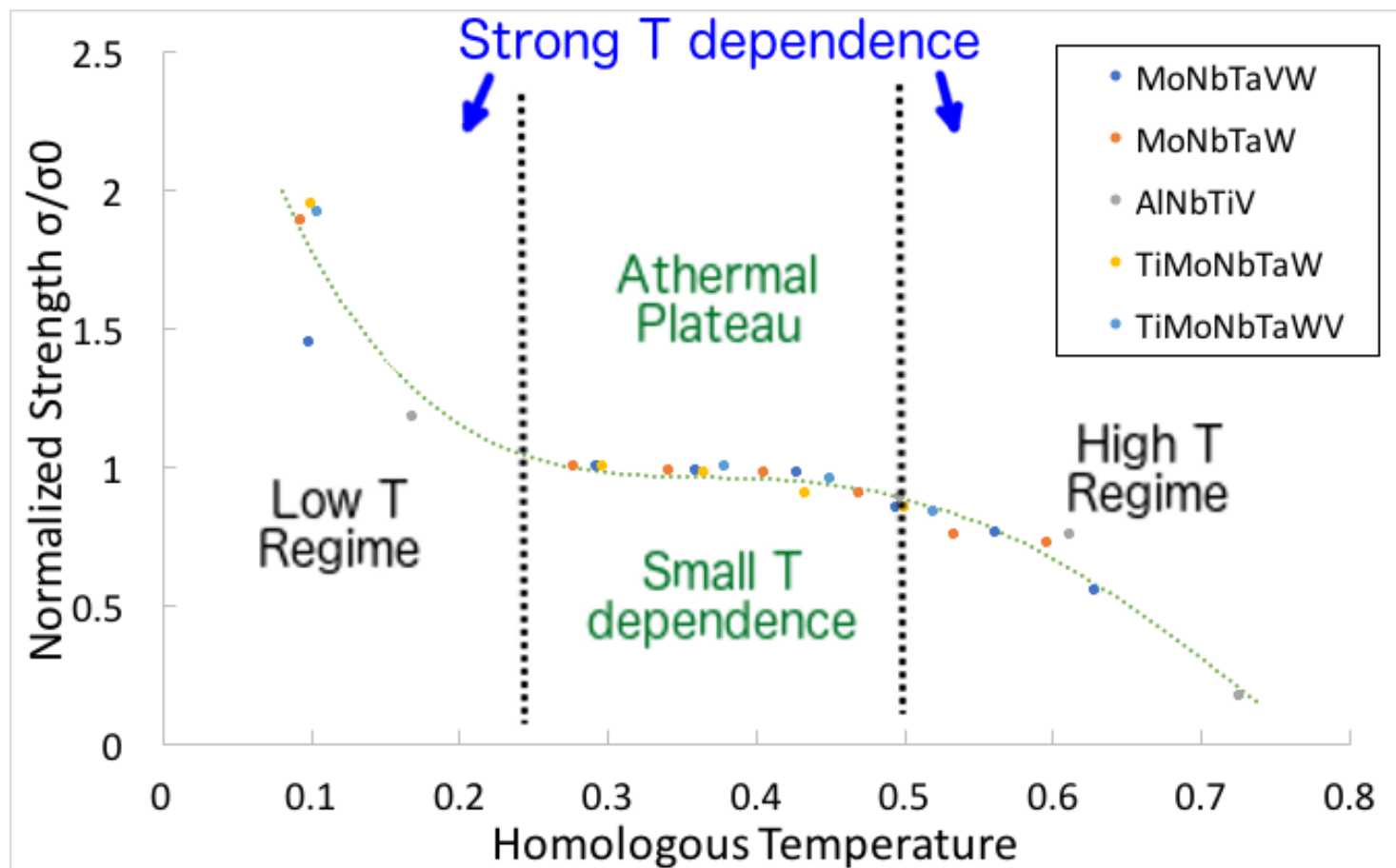


BCC Metals Deformation

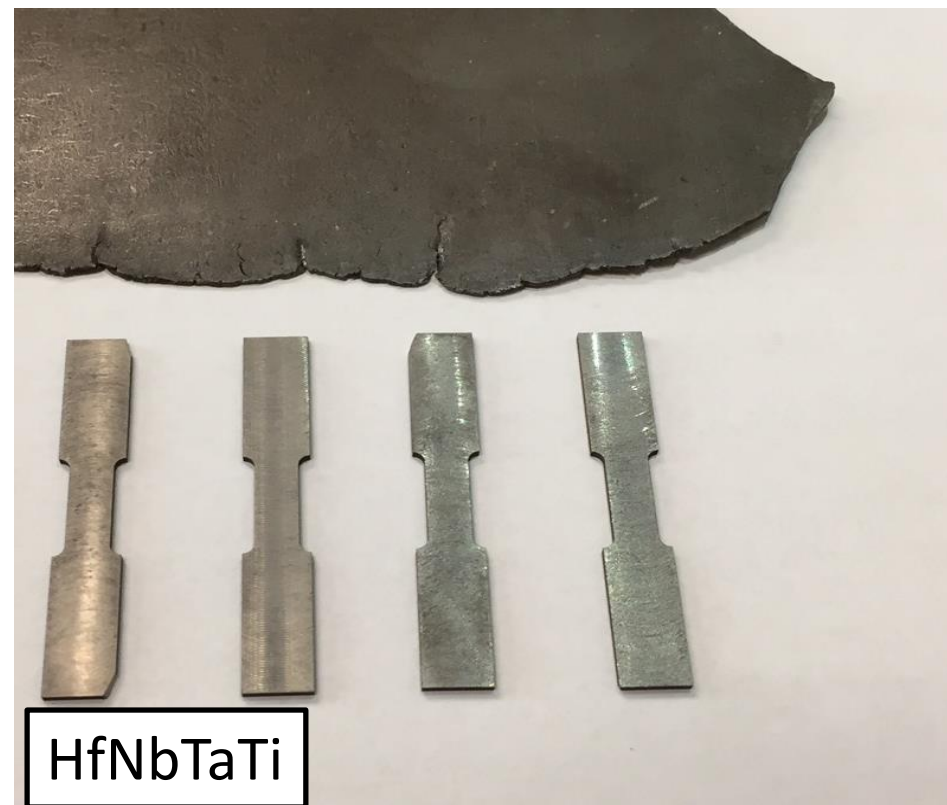
- Regimes II and III
 - High temperature dependence
 - Low mobility of screw dislocations
 - Brittle
- Regime I: athermal
 - Behavior closer to FCC metals
- Alloying changes the shape of the curve
 - Increases the plateau stress
 - Decreased temperature dependence in regime II
 - Softening in regime I



BCC RCCA Deformation



RCCA Cold Rolling

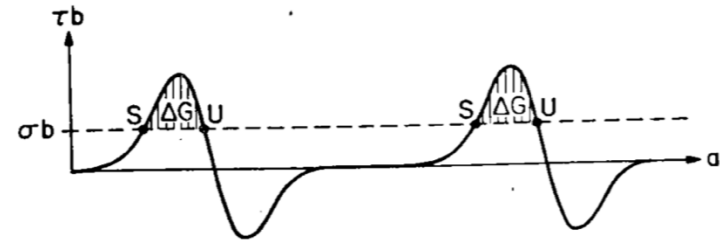


Thermally Activated Deformation Modelling

Thermal and athermal contributions to strength:

$$\tau = \tau^* + \tau^a$$

Thermally activated barriers:

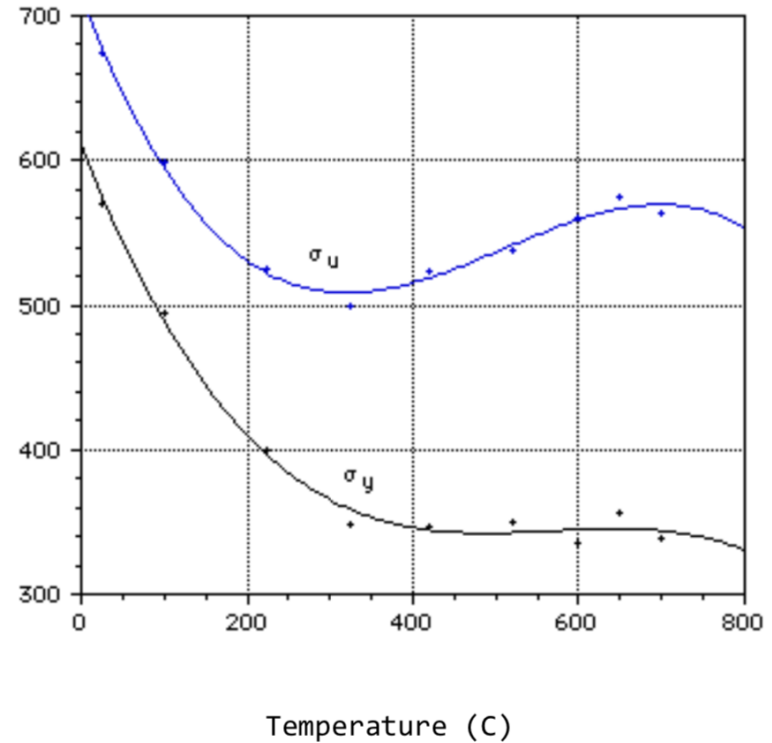
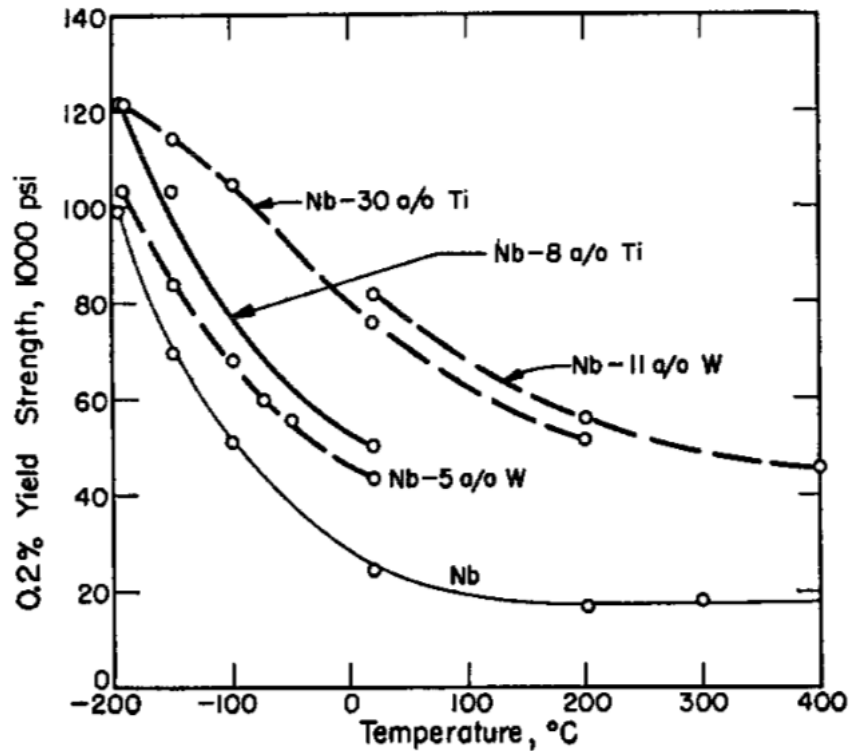


Activation barrier:
$$\Delta G = F_0 \left[1 - \left(\frac{\tau - \tau_i}{\tau_0 - \tau_i} \right)^p \right]^q = F_0 \left[1 - \left(\frac{\tau^*}{\tau_0^*} \right)^p \right]^q$$

Elastic modulus softening correction:
$$\frac{\mu(T)}{\mu_0} = f(T)$$

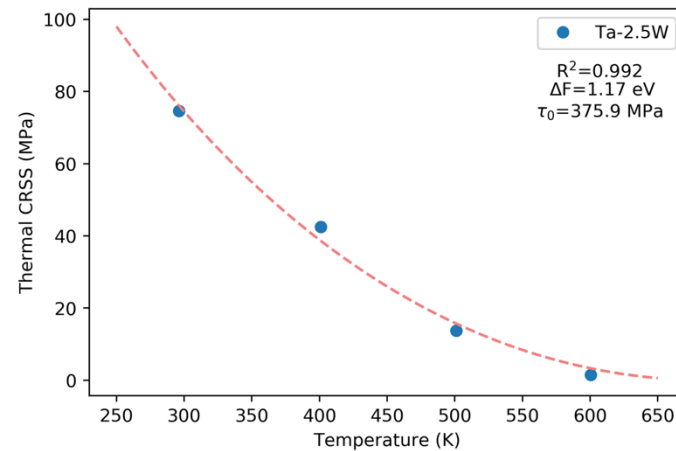
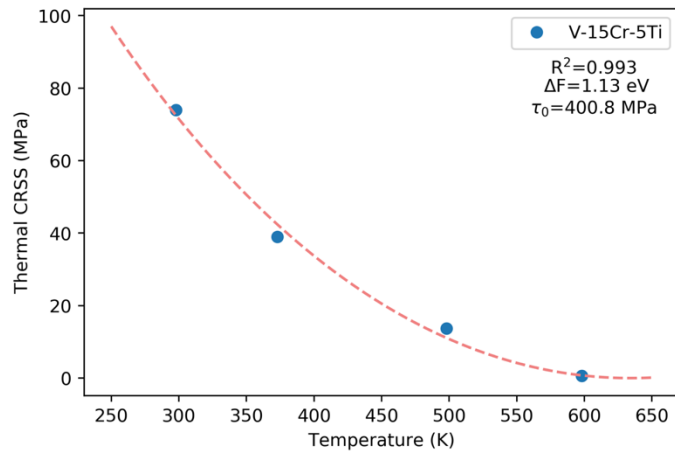
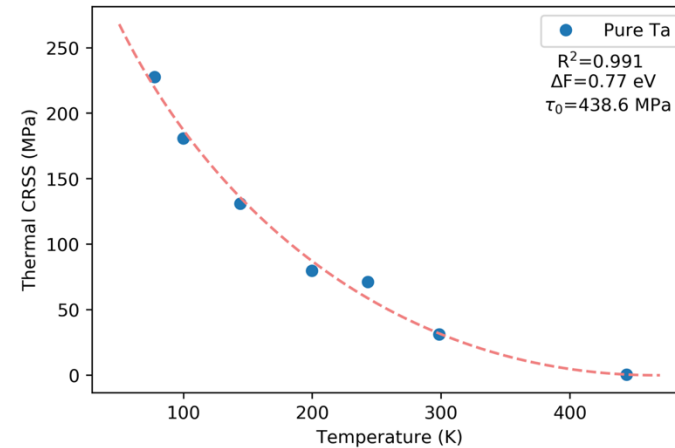
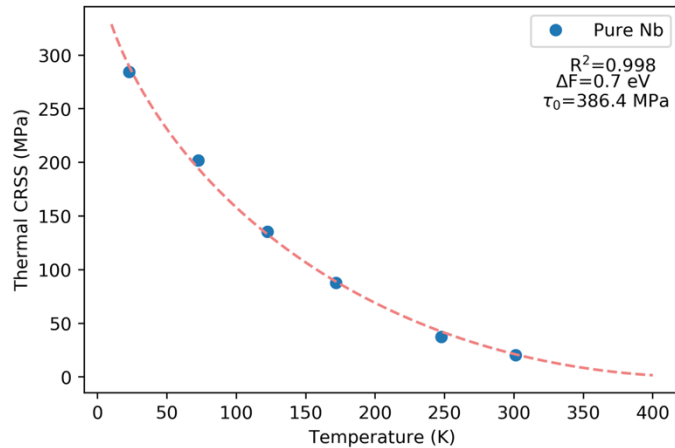
The p and q values:
Shape of the barrier

Application to Conventional Refractory Alloys

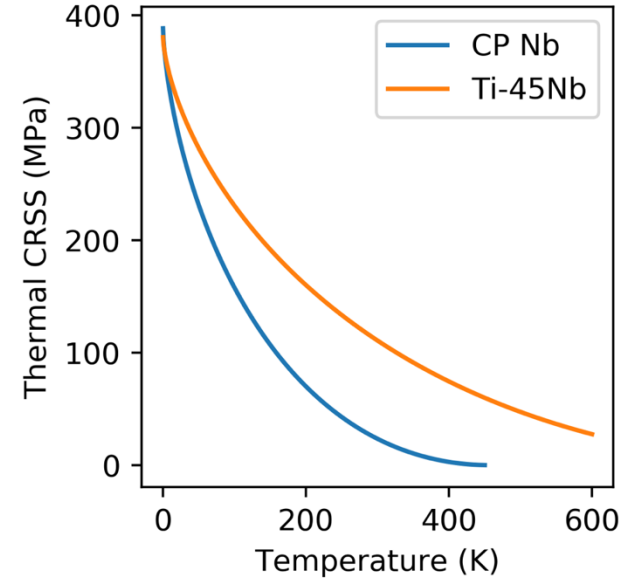
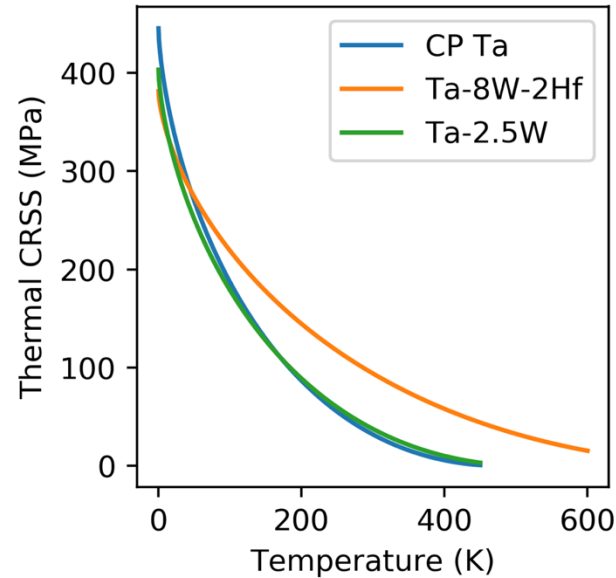
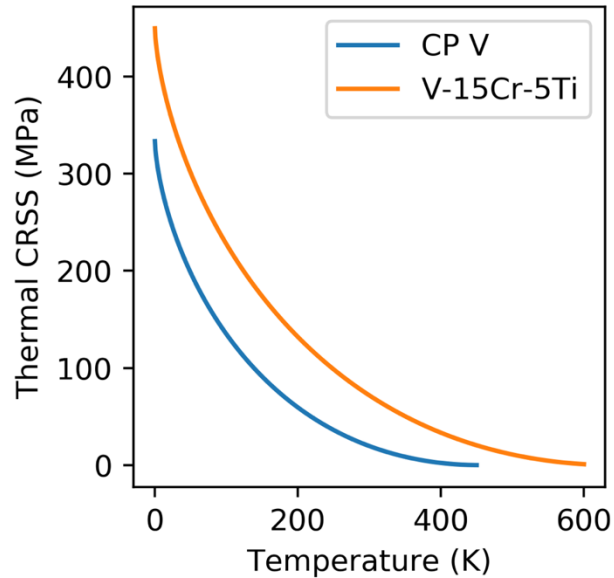


J.H. Bechtold, B. Road, J. Less-Common Met. 3 (1961) 1-12.
 S. Stud, VANADIUM ALLOY (V-15Cr-5Ti), 2018.

Conventional Refractory Alloy Thermal Activation

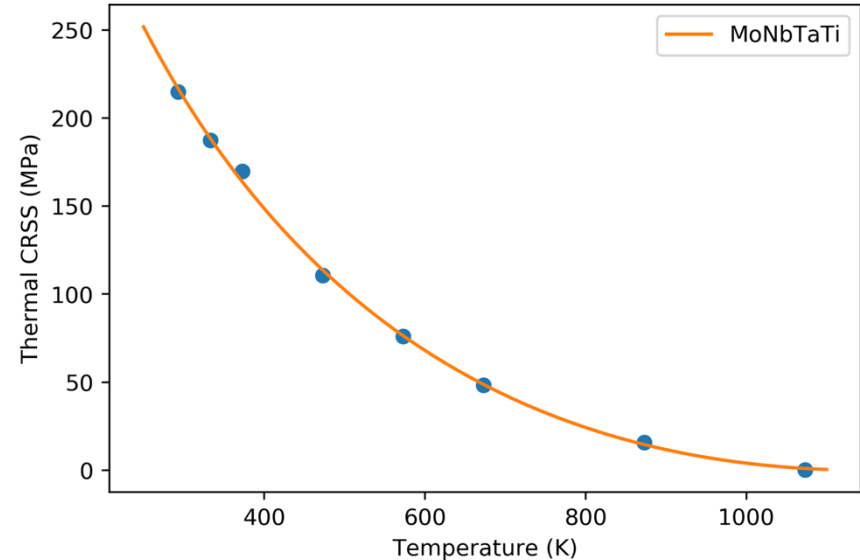


Conventional Refractory Alloy Comparison

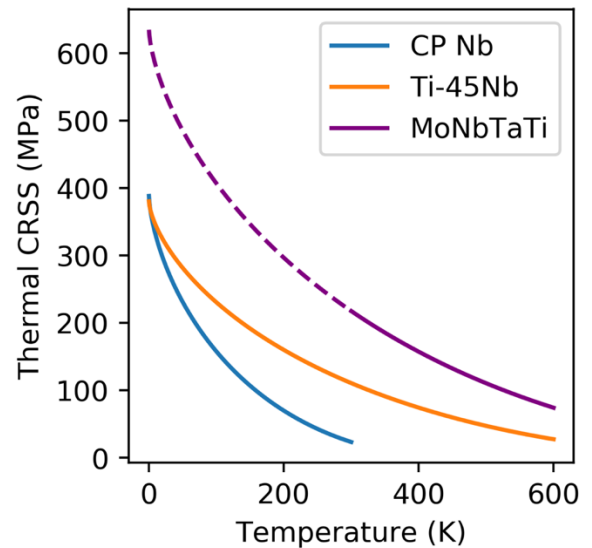
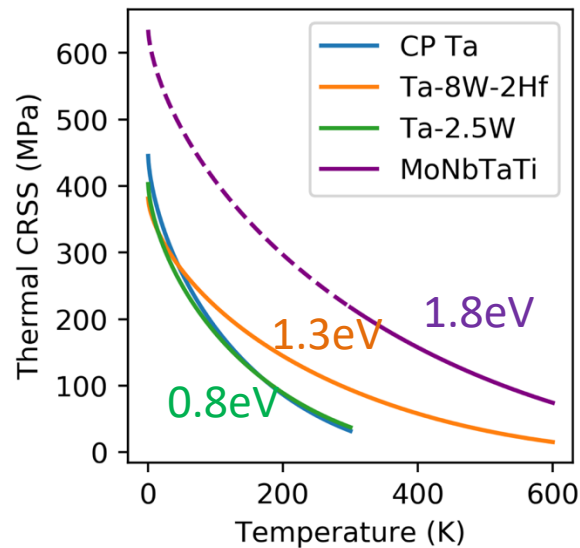
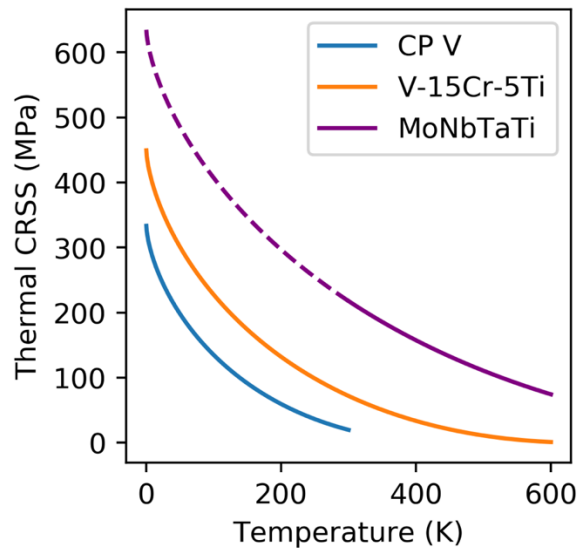


BCC Deformation at Low Temperatures

- Adapt σ -T models
 - Extract activation energies for double kink mechanism
 - Extrapolate the Peierls stress at 0K



Thermal Activation of RCCAs



Athermal Deformation Component

- Toda-Caraballo model (semi-empirical):

Original formulation:

Does not consider elastic modulus mismatch

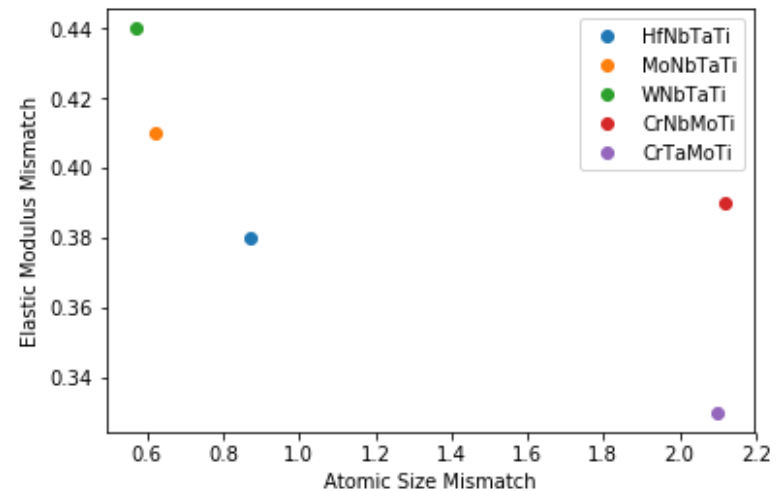
$$B = 3\mu Z \left[\xi(\eta'^2 + \alpha^2 \delta^2)^{1/2} \right]^{4/3}$$

Elastic Mismatch Size Mismatch

$$\Delta\sigma_{ss}^m = 3Z\mu \left(\frac{\xi\alpha}{a} \right)^{4/3} (x_1, x_2, \dots, x_n)$$

$$\begin{pmatrix} 0 & \left| \frac{da}{x_1^2} \right|^{4/3} & \dots & \left| \frac{da}{x_1^n} \right|^{4/3} \\ \left| \frac{da}{x_2} \right|^{4/3} & 0 & \dots & \left| \frac{da}{x_2^n} \right|^{4/3} \\ \vdots & \dots & \ddots & \vdots \\ \left| \frac{da}{x_1} \right|^{4/3} & \left| \frac{da}{x_n} \right|^{4/3} & \dots & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix}$$

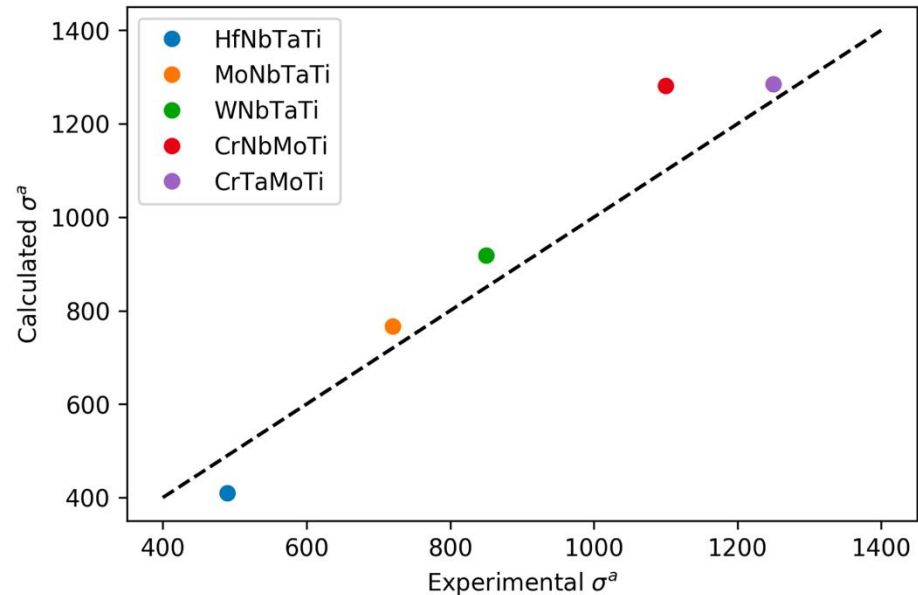
Alloy	Experimental σ^a (MPa)	Calculated σ^a (MPa)
HfNbTaTi	490	448
MoNbTaTi	720	580
WNbTaTi	850	608
CrMoNbTi	1000	2248
CrMoTaTi	1250	2475



Athermal Deformation Component

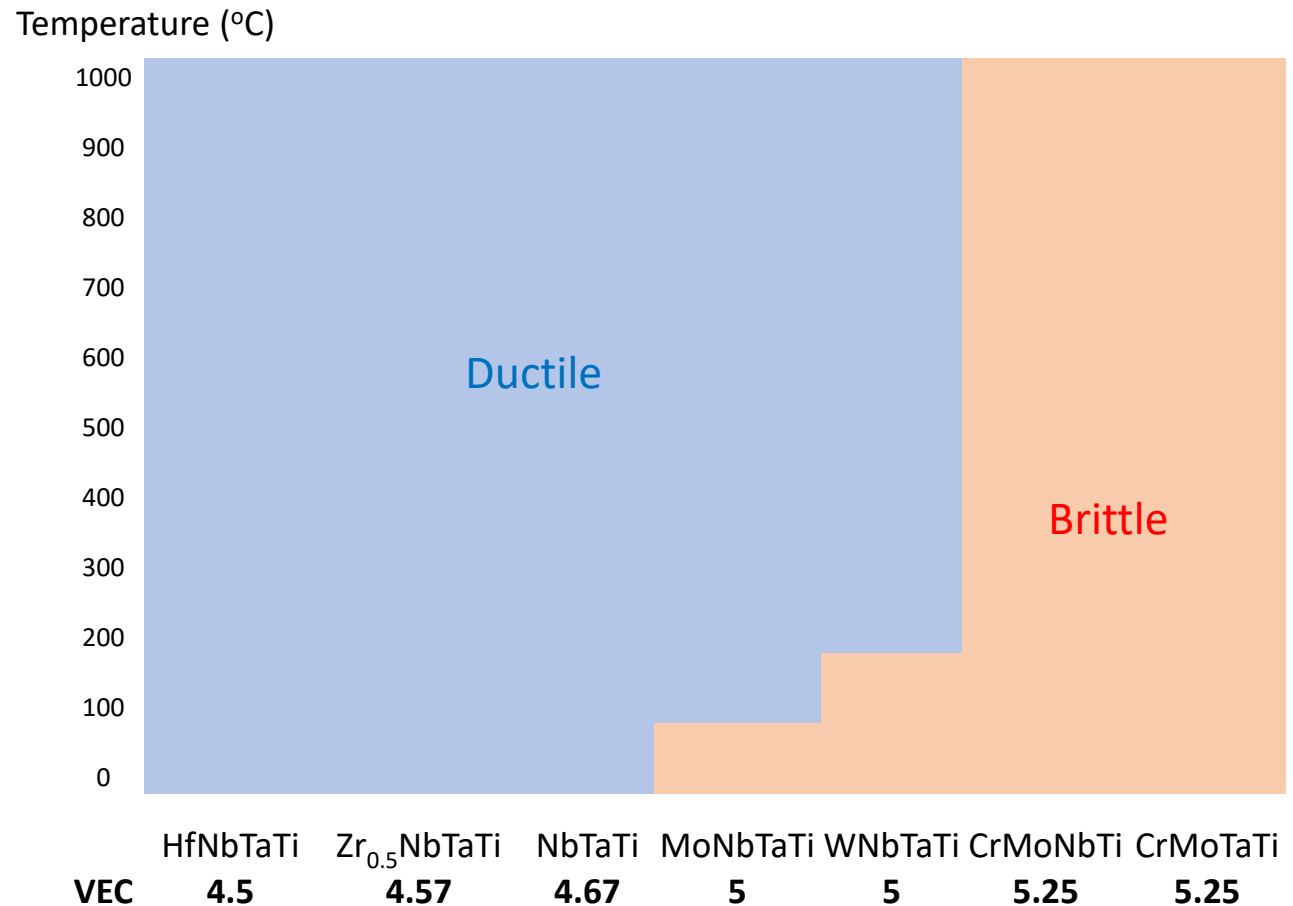
- Incorporate elastic mismatch
- Stronger alloys are outliers

Alloy	Experimental σ^a (MPa)	Calculated σ^a (MPa)
HfNbTaTi	490	410
MoNbTaTi	720	767
WNbTaTi	850	919
CrMoNbTi	1100	1282
CrMoTaTi	1290	1285



Ductility of RCCAs

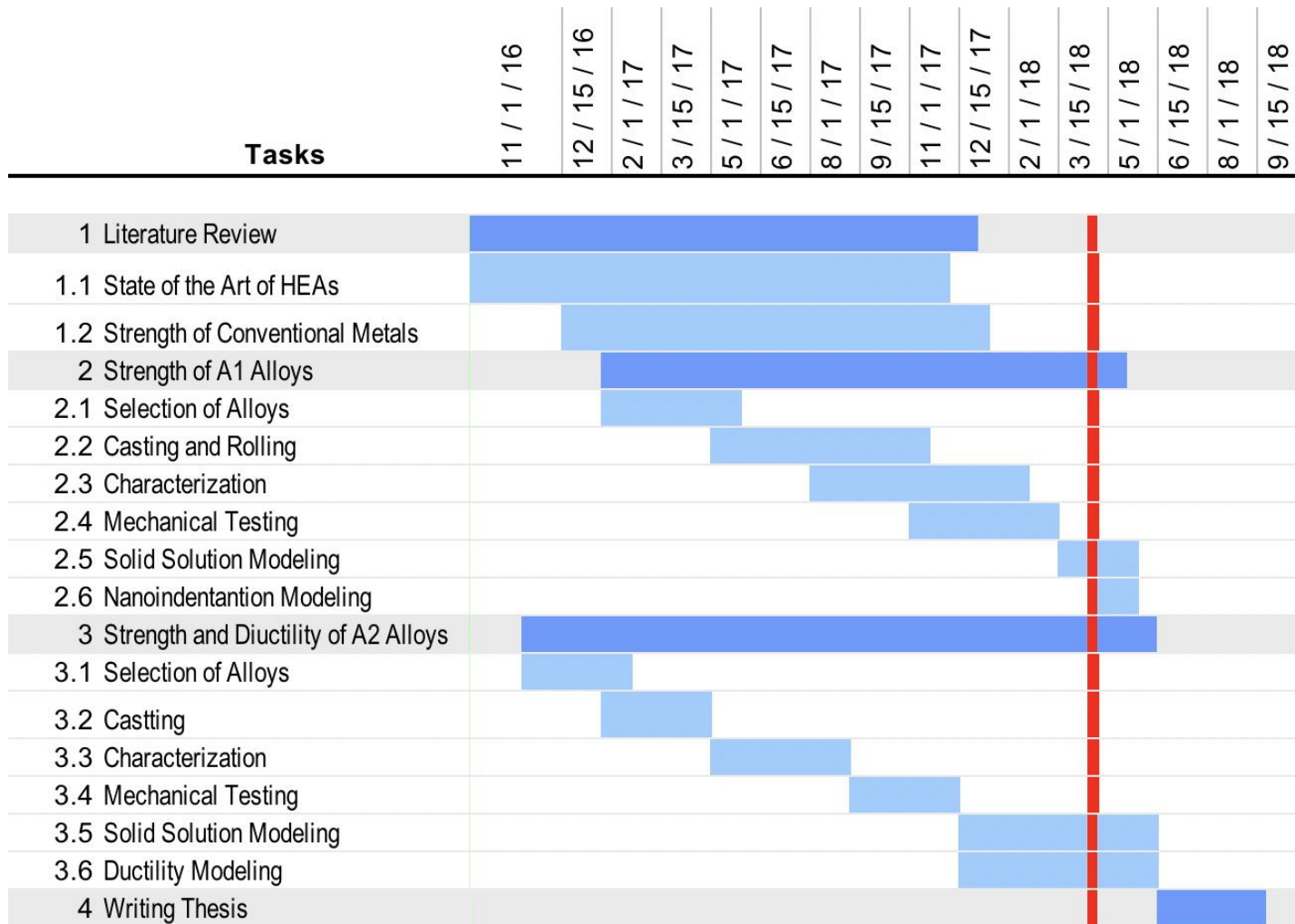
- Ductility criteria
 - 30% compression without fracture
- Ductility increases with VEC



Summary

- TCHEA2 provides improved predictions
- Narrower δ and Ω window for RCCAs
- Athermal and thermal components needed for RCCAs
- The activation energy of RCCAs is larger than conventional refractory alloys
- Current models do not describe the athermal component
- Incorporating elastic modulus mismatch improves predictions

Gantt Chart



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Thank you very much!

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